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NRL Memorandum Report 2425

# Short Range Air-to Air Weapon Control Requirements [Unclassified Title]

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April 1972





NAVAL RESEARCH LABORATORY Washington, D.C.

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#### MEMORANDUM

#### 1. Background

(C) The Southeast Asia conflict has demonstrated the need for a short range air-to-air weapon. As a result, several dogfight missiles are being developed, namely, AGILE, AIM-7E-2/F and a dogfight AIM-9. The need therefore arises for a definition of the dogfight environment in terms of design requirements (so that system components can be made) for weapon control systems capable of operating in this dogfight environment.

#### 2. Findings

(C) This study defines the dogfight environment in terms of a tracking weapon control system. It is shown that the present airborne intercept (AI) radars, and in particular their range and angle tracking circuits, are not capable of handling the dogfight weapon control problem. More importantly, however, the tracking requirements for a weapon control system are defined in terms of cumulative probability distributions.

#### 3. R & D Implications

(C) This study shows that full-sphere tracking capability is desired for the dogfight environment. Coupled with this feature, an extremely rapid automatic lock-up and very wide-bandwidth tracking loops are required. Full-sphere tracking may require the development of a completely new type of tracking system.

#### 4. Recommended Action

(C) It is recommended that models of the present AI radars be utilized to evaluate the recommended tracking parameters. It is further recommended that a study be undertaken to design the  $360^{\circ}$  tracking loops required for full-sphere tracking capability.

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#### ABSTRACT

- (U) The primary objective of this study is to define the dogfight environment in terms of a tracking system. The secondary objective is to apply this dogfight definition to present AI radars.
- (U) This study is divided into two efforts, a determination of the primary weapon control requirements and a parameter interaction study. The purpose of the primary weapon control requirements study is to define the dogfight environment and to investigate the relationship of aircraft, tactics, weapons, and the available data base. The purpose of the parameter interaction study is to define the dogfight environment more precisely in terms of tracking loop requirements, clutter problems, and glint.

#### PROBLEM STATUS

- (U) The two studies, the primary weapon control requirement study and the parameter interaction study, have been completed. Work, however, continues on interpretation of the data developed during the parameter interaction study.
- (U) Tracking models for AI radar are being developed to determine the effects of the recommended tracking parameters on these radars.

#### **AUTHORIZATION**

Short Range Weapon Control Compatibility with AWG-10/AWG-14 NRL Problem 53D01-03.308 A510-5108/652-4/1510-00-31

F-14/AWG-9 Weapon Systems Analysis NRL Problem 53D01-03.308 A510-5108/652-F/1W16-08-0000

Airborne Intercept Weapon Control NRL Problem 53D01-03.323 A360-5333/652B/1F17-342-603

Guided Missile AIM-7F Simulation Studies NRL Problem 53D01-03.311 A510-5108/652-F/1W16-14-0000

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Short Range Air-to-Air Weapons Control Requirements

#### I. INTRODUCTION

#### A. Background

- (C) In the past, Naval airborne intercept (AI) radars were designed to intercept non-maneuvering bomber targets. Since these radars were designed to detect and track such targets at long range, they required a high power but relatively little angular coverage. Further, since these bomber targets have low maneuvering capabilities, the radars were designed with low tracking rates and accelerations. With these restrictions these radars were severely limited in their short-range air-to-air capability.
- (C) The Southeast Asian conflict has shown that superiority in the short-range air-to-air (dogfight) engagement is a critical requirement for today's Naval aircraft. Many reports attest to this fact, the best known being the "Red Baron" (1) reports.
- (C) A short-range weapon is required in a dogfight engagement. To fulfill this need, a dogfight missile (AGILE) is currently being developed by The Naval Weapons Center (NWC), China Lake (Refs. 2,3,4,5,6,7,8). In addition, modifications are being made to the AIM-7 Sparrow-TII and the AIM-9 Sidewinder missiles to provide a dogfight capability.
- (C) With the development of dogfight missiles, the need for a short range air-to-air weapon control system (WCS) becomes evident. The nature of the dogfight environment requires that this WCS be quite different from those of the present Al radars. The target, instead of being a slowly maneuvering bomber at long range, is now a highly maneuverable fighter at close range.

#### B. Program Objectives

- (U) The primary objective of this study is to accurately define the dogfight environment in terms of the tracking requirements for a variety of WCS. Many flight tests, computer simulations, and manned simulations have been performed by many people to gather data on the dogfight environment. For the purpose of this report, one of the manned simulations and one of the flight tests were used to determine the tracking requirements. The influence of specific weapons and their associated kill probabilities are important but fortunately not critical to this study.
- (U) The generic types of tracking systems investigated in this study are listed below.

- 1. A typical AI radar  $\pm 60^{\circ}$  off the nose in azimuth and elevation.
- 2. A tail warning/tracking system having a coverage ±60° off the tail in azimuth and elevation.
- 3. A full sphere coverage system.
- (U) Further objectives of this study pertain directly to problems associated with clutter and glint.

#### C. Analytical Approach

- 1. (U) This study made use of existing dogfight data from the NADC manned simulation and from VX-4 flight tests.
- a. The NADC simulation consisted of two cockpits in which two pilots simulated a dogfight while computers provided the aircraft dynamics. Pertinent details of the simulation are given below. Full details may be found in Refs. 9 and 10.
  - Each aircraft was moduled with 6 by 4 degrees of freedom.
  - ii. Each dogfight originated at 15,000 feet altitude with the aircraft abeam of each other and separated by 2 nm.
  - iii. Three friendly and two enemy type aircraft were simulated.
    - iv. Two weapon mixes were simulated for the friendly aircraft.
      - (A) A short range missile with an all-aspect and a 45° off-boresight capability.
      - (B) Guns and Sidewinder
    - v. 72 dogfights with a given aircraft and weapon mix made up one situation for study.
    - vi. Pilot presentation was a 16" CRT providing a forward hemisphere field of view with the presentation slewable to allow full cockpit visibility. Pilot blackout was simulated by dimming the display.
  - vii. The trained pilots were selected from tactics instructors on the F-4 and F-8 aircraft.

- viii. Pilots were rotated every 6 encounters.
- b. The VX-4 flight test data were obtained from a simulated combat of two F-4 aircraft. Pertinent characteristics of the VX-4 data are:
  - i. All aircraft position data were obtained by beacon tracking of the aircraft with two FPS-16 ground-based radars.
  - ii. For safety, a minimum altitude of 5,000 feet was required.
  - iii. Approximately 800 seconds of useful data were obtained.
  - iv. The pilots were flying gun/Sidewinder tactics.
- 2. To achieve a precise definition of the dogfight environment, the study was divided into phases so that the results of each phase could be thoroughly understood and applied in the following phases. This study is divided into three phases, with the results of the first two phases being the subject of this report.
- (U) The first phase, the primary weapon control requirement study, is designed to assess the effects of the various aircraft, the tactics, and the two simulations upon the short-range WCS requirement. The specific areas of interest for the first phase are the coverage requirement, the maximum range requirement, and the tracking requirements as a function of target angular position.
- (U) The second phase is the parameter interaction study. Based upon results of the first phase, data were selected for this detailed study of tracking loop requirements, clutter, and glint. The areas of investigation were a forward tracker, a rearward tracker, and a full sphere tracker.

### II. PRIMARY WEAPONS CONTROL REQUIREMENTS

#### A. Program Description

- (U) Approximately 157,000 seconds of data are available from the two sources. A description of the basic computer program to reduce these data is contained in Appendix A. This basic program required extensive modification before use on the VX-4 data.
- (C) Table 1 lists the simulation, the aircraft type, and the tactics by data tape number. As will be seen by the data presented later in this Section, the results, for the parameters of interest, are relatively independent of aircraft type. For this reason, and at the request of NADC, the aircraft are designated by letters. Specifically, three friendly aircraft types, designated A, B or C were used in the NADC simulations. The F-4 aircraft used in the VX-4 flight tests are designated by F.

TABLE 1.

Tape Number	Simulation	Fighter l (Friendly)	Fighter 2 (Enemy)	Fighter 1 Tactics	Fighter 2 Tactics
1	NADC	C	E	SRAAM*	G/S
2	NADC	С	D	G/ <b>S**</b>	G/S
3	NADC	A	E	G/S	G/S
4	NADC	A	D	SRAAM	G/S
5	NADC	В	D	SRAAM	G/S
6	NADC	В	E	G/S	G/S
101	VX-4	F	F	G/S	G/S

<sup>\*</sup> Short Range Air-To-Air Missile

#### 1. Azimuth vs Elevation of the Target vs Frequency of Occurrence

(U) The results of this study are shown in Figs. A-2 to A-15, Appendix A. The purpose of these plots is to determine the most

<sup>\*\*</sup> Guns/Sidewinder

<sup>(</sup>U) The data reduction for this phase of the study was carried out in three parts, (1) azimuth vs elevation of the target vs frequency of occurrence, (2) angle off boresight vs range of the target vs frequency of occurrence, and (3) tracking rates and accelerations as a function of relative target position.



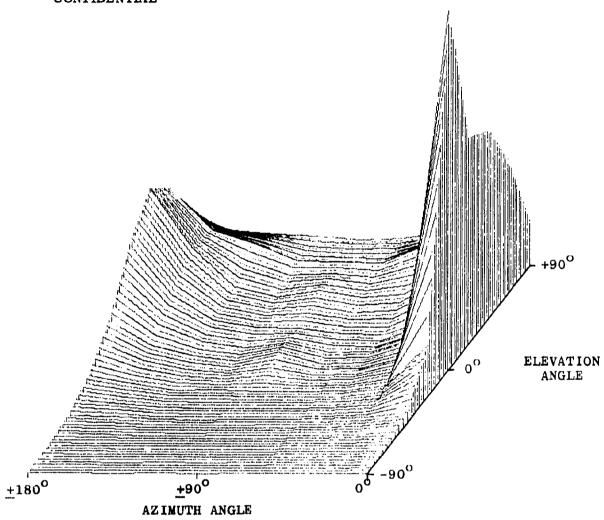


FIG. 1 - TAPE 1 - FIGHTER 1 - ELEVATION ANGLE VERSUS AZIMUTH ANGLE VERSUS FREQUENCY OF OCCURRENCE.

likely positions of the target with respect to the fighter in aircraft coordinates. Figure 1, an example of these plots, was computer generated from tabulated data with a linear interpolation between the azimuth elevation points. Because of this interpolation, these plots are qualitative and are presented only for visualization purposes. Quantitative data are given later in this report.

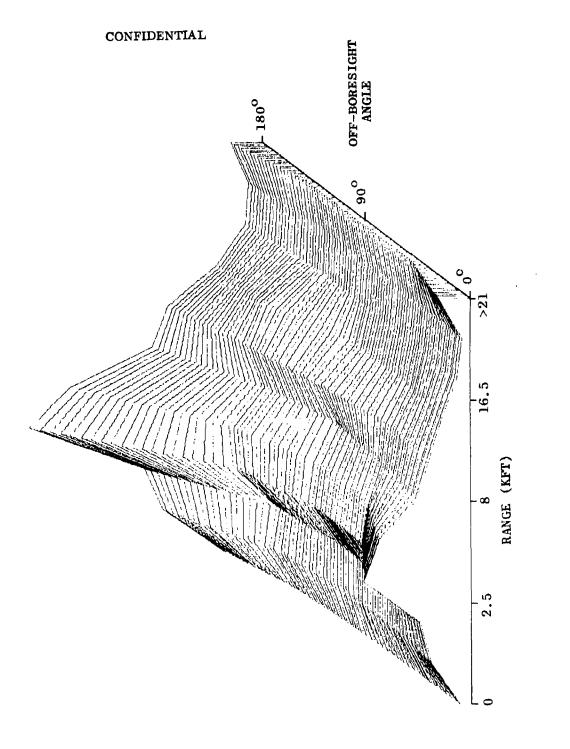
(C) Figure 1 is a three-dimensional plot of target position with respect to the fighter (Fighter 1 in this case as experienced in 72 three-minute encounters. The azimuth position of the target with respect to the fighter is plotted along the X-axis (180° is the tail-on position and 0° is head-on). The corresponding position of the target in elevation with respect to the fighter is plotted along the Y-axis. Directly underneath the fighter is designated -90° and directly overhead is +90°. The frequency of occurrence during the 72 three minute encounters is plotted along the Z-axis. It can be seen that the target is below the fighter a very small portion of the time. Further, the target is within approximately 30° in azimuth off the nose and/or tail of the fighter a majority of the time. The plots for all the aircraft show the same general trend with wide variation in the amplitude of forward and rearward peaks.

#### Angle Off Boresight vs Range to the Target vs Frequency of Occurrence.

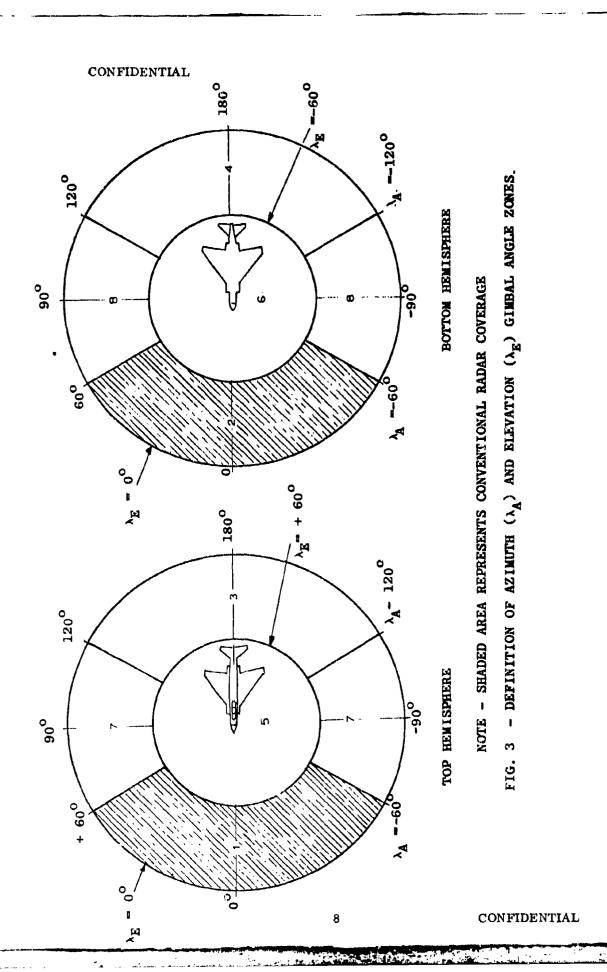
- (U) The results of this study are shown in Fig. A-16 to A-29, Appendix A. These plots portray the dependence of range on angle off boresight. In the collection of the data, the cell sizes (segment of range at a segment of angle off boresight) were not chosen to be equal, which makes the interpretation of these plots difficult.
- (C) Referring to Fig. 2, which is an example, it can be noted that the distribution of range is independent of angle off boresight. This feature, noted in all the data, can be seen by the ridges and valleys which are constant in range, regardless of angle.

# 3. Tracking Rates and Accelerations as a Function of Relative Target Position.

(U) The purpose of this portion of the study was to obtain an estimate of the tracking requirements as a function of target position with respect to the fighter. Figure 3 depicts the various gimbal angle zones which were investigated. The total sphere around the fighter aircraft is divided into a top and a bottom hemisphere. Each hemisphere is divided into forward, rearward, side, and top (bottom) zones of coverage. The zones are grouped in the following manner:



TAPE 1 - FIGHTER 1 - RANGE VERSUS OFF-BORESIGHT ANGLE VERSUS FREQUENCY OF OCCURRENCE. N



- a. Conventional AI radar coverage zones 1 and 2.
- b. Rearward coverage zones 3 and 4.
- c. Top and bottom coverage zones 5 and 6.
- d. Side coverage zones 7 and 8.
- (U) The results of the data reductions are presented in Figs. A-30 to A-125, Appendix A, as bar graphs, with fourteen bars depicting the various aircraft, weapons, and simulations as shown in Table 1. The parameters listed below are of specific interest in the design of the tracking loops for a weapon control system.
  - a. The percent of time that the target was in a particular gimbal angle zone. This assesses the importance of the various zones.
  - b. The statistics of range, Figures A-38 to A-45 (11).
  - c. Range rate, Figures A-46 to A-53.
  - d. Range acceleration, Figures A-54 to A-61.
  - e. Azimuth line-of-sight rate, Figures A-62 to A-69.
  - f. Azimuth line-of-sight acceleration, Figures A-70 to A-77.
  - g. Elevation line-of-sight rate, Figures A-78 to A-85.
  - h. Elevation line-of-sight acceleration, Figures A-86 to A-93.
  - 1. Azimuth gimbal rate, Figures A-94 to A-101.
  - j. Azimuth gimbal acceleration, Figures A-102 to A-109.
  - k. Elevation gimbal rate, Figures A-110 to A-117.
  - 1. Elevation gimbal acceleration, Figures A-118 to A-125.
- (U) Using Fig. 4 as an example, the average value of all range rate values experienced during 72 three minute encounters is shown as a line through the shaded area of each bar. The  $2\sigma$  values (95%) are shown as the shaded area in each bar and the minimum and maximum values are shown as the full extent of each bar. In order to accurately portray these values, a log scale is used on the ordinate axis. The use of the log scale expanded the data about zero to show the average and  $2\sigma$  values, and contracted the data to show minimum and maximum values.

#### B. Data Verification

- (C) In general, the VX-4 and the NADC data are in close agreement. This can be seen in Figs. A-30 to A-125. Points of disagreement are listed below.
- 1. In the range plots, shown in Figs. A-46 to A-53, the minimum range in the VX-4 data is greater than in the NADC data. In the manned NADC simulation, the fear of aircraft collision does not exist, and therefore, for range, the VX-4 data are more accurate. Consequently,

4 - SUMMARY OF RANGE R

- U N

Ö.

CASE

AIRCRAFT WEAPONS

800

-400

-1600

-3200

RANGE RATE (R) (FT/SEC)

1600

800

400

3200

conclusions drawn from this entire study will neglect some of the short-range NADC data.

- 2. The accelerations (range, line-of-sight, and angular) shown in Figs. A-70 to A-125 are greater in the VX-4 data. The VX-4 data, based on ground-based radar tracking information, are very noisy, and differentiations amplify the noise and render the accelerations suspect. For this reason the VX-4 data were not used for analyzing accelerations.
- 3. The amount of VX-4 data is small compared to the amount of NADC data. At times, there were insufficient VX-4 data from which to develop meaningful statistics.

For the above reasons, further analyses in this program will use NADC data with limits being imposed by the VX-4 data.

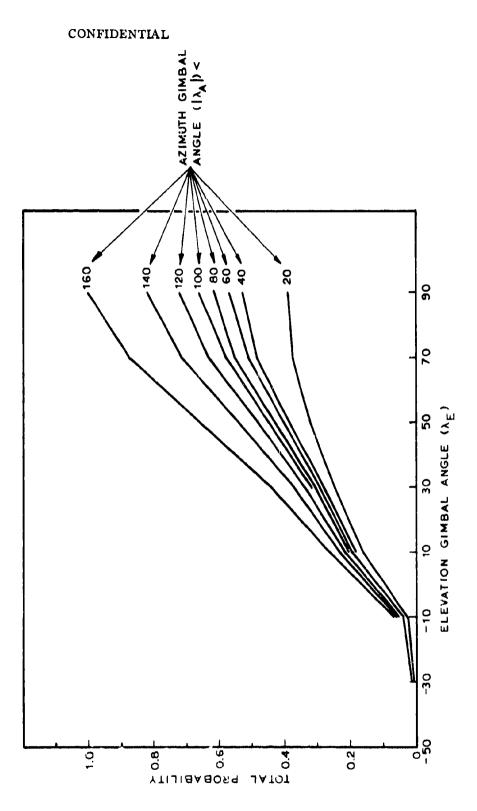
- (C) A direct analysis of the differences in WCS requirements brought about by aircraft type was a goal. However, of the combinations possible from 3 friendly and 2 enemy aircraft, and 2 weapon mixes, only six were available for analysis. But, in general, the data reflect little direct change with the aircraft type with the exception of the relative importance of tail and forward coverage. For this reason, the 2  $\sigma$  values for the worst case are cited in the conclusions of this phase of the report.
- (U) In Figs. A-2, A-6, and A-12, it can be seen that the friendly aircraft have an advantage over the same enemy aircraft, fighter E. This was the only discernible effect of influence by aircraft type.

#### C. Coverage Requirement

(C) The WCS coverage requirements are shown graphically in Section A-2 of Appendix A. As might be expected, the upper hemisphere is extremely important, as is the forward zone of approximately  $\pm 30^{\circ}$  azimuth. Also, it is important to be able to track the target in the off tail zone. This indicates a need for the upper hemisphere, nose, and tail coverage for the weapon control system. A trade off based on probability of occurrence for azimuth and elevation coverage can be made with the use of Fig. 5. Although the relative weights on the tail and nose vary among aircraft types, the general distribution is independent of aircraft type.

#### D. Tracking Parameter Variations as a Function of Coverage Areas

(U) For the reporting of the results of this section, the area around the fighter aircraft is broken into five zones:



CUMULATIVE PROBABILITY DISTRIBUTION OF ELEVATION GINBAL ANGLE FOR SEVERAL VALUES OF AZIMUTH GIMBAL ANGLE. S

- 1. The forward  $160^{\circ}$  in azimuth and elevation nose sector.
- 2. The rear  $\pm 60^{\circ}$  in azimuth and elevation tail sector.
- 3. The top and bottom  $\pm 30$  cones top and bottom cones.
- 4. The side sectors  $\pm 60^{\circ}$  in elevation and between  $\pm 60^{\circ}$  and  $\pm 120^{\circ}$  azimuth side sectors.
- 5. Total sphere coverage.
- (U) The values quoted in Table 2 are maxima of the  $2\sigma$  values (95% based upon normal distribution assumption) except for the total sphere coverage case, for which maximum and minimum are quoted. The bottom side sector and the bottom tail sector were not used in the determination of rates and accelerations for the table because of their low frequency of occurrence. Their small sample size makes the normal distribution assumption less valid; therefore, confidence is reduced in the  $2\sigma$  value containing 95% for the data. It is also important to note that the data in Section A-4 of Appendix A is divided into 8 sectors, which differs from the division of data shown in Table 2.

TABLE 2 - TRACKING PARAMETER VARIATIONS AS A FUNCTION OF COVERAGE AREA.

		31	COVERAGE AREA		
PARAMETER	NOSE SECTOR TAIL SECTOR (2 \sigma) (2 \sigma)		TOP & BOTTOM CONE (2 \sigma)	SIDE SECTORS FULL SPHERE (2 \sigma) (maximums)	FULL SPHERE (maximums)
% OF TIME IN COVERAGE AREA	44	28	23	ro	100
RANGE (FT)	30,000	37,000	28,000	32,000	50,000
RANGE RATE (FT/SEC)	- 2,100	- 1,000	- 1,300	- 1,300	± 2,400
	+ 1,000	+ 2,100	+ 1,600	+ 1,500	
RANGE ACCELERATION (FT/SEC <sup>2</sup> )	400	360	670	800	3,000
AZINUTH LINE OF SIGHT RATE (DEG/SEC)	40	99	28	85	1,300
AZIMUTH LINE OF SIGHT ACCELERATION (DEG/ SEC <sup>2</sup> )	36	89	38	102	1,300
ELEVATION LINE OF SIGHT RATE (DEG/SEC)	41	45	31	38	1,140
ELEVATION LINE OF SIGHT ACCELERATION (DEG/SEC <sup>2</sup> )	37	51	40	45	1,130
AZIMUTH GIMBAL RATE (DEG/SEC)	ij	82	450	95	12,000
AZIMUTH GIMBAL ACCELERA- TION (SEG/SEC <sup>2</sup> )	47	88	580	140	12,000
ELEVATION GIMBAL RATE (DEG/SEC)	47	46	37	89	12,000
ELEVATION GIMBAL ACCELERA- TION (DEG/SEC <sup>2</sup> )	51	55	49	76	930

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#### III. PARAMETER INTERACTION STUDY

#### A. Program Description

- (U) In Section II of this report, the mean plus or minus  $2\sigma$  values for the tracking parameters were given. In order to assign a probability to these numbers, a distribution must be assumed. If a normal distribution is assumed, then the average plus  $2\sigma$  yields a 95% probability. In this section of the report, the actual distributions of the parameters were determined and the actual probabilities found. In addition, the actual distribution of two related parameters were determined thus enabling the determination of a single probability for two related parameters, such as the range rate and range acceleration.
- (C) The basic computer program description is contained in Appendix B. This program has the capability of computing a two-variable cumulative distribution with average and  $1\,\sigma$  of the dwell time for any parameters of interest. The program has the further capability of calculating a frequency distribution in the third dimension and/or collecting the data by gimbal angle off nose and off tail of the fighter aircraft. Further restrictions such as minimum range, maximum range, etc., can be applied to the data.
- (U) Tape 1 was used for this atudy because by the primary weapon control study it was shown to be a good representative of the dogfight engagement. For the parameters of interest, the 2 \u03c4 values do vary somewhat for the various tapes (Appendix A). As an example of the continuing verification of the results of the parameter interaction study, tape 3 in addition to tape 1 was used in analysis of the tracking parameters. A comparison of the results from these two tapes showed that for the primary area of interest (the 90% to 99% probability of track), the results were the same. In the lower probability of track region, tape 3 showed a higher rate and acceleration requirement than tape 1.
- (U) A conclusion to be drawn by the comparison of the two tapes is that for the 90% to 99% probability of track the results of tape 1 are valid for all the data tapes. The differences in the 2  $\sigma$  values between tapes arises because of the assumption of a normal distribution made for the primary weapon control requirements study.
- (U) The following is an explanation of three basic types of parameter interactions completed under this study. It should be noted that the basic reduction method is not restricted to the interactions accomplished. An example of the flexibility of this program was a study to analyze the altitude clutter as a function of range and altitude while in the vertical scan lock-up mode of the AWG-9 radar.

#### 1. Tracking Parameter Interactions

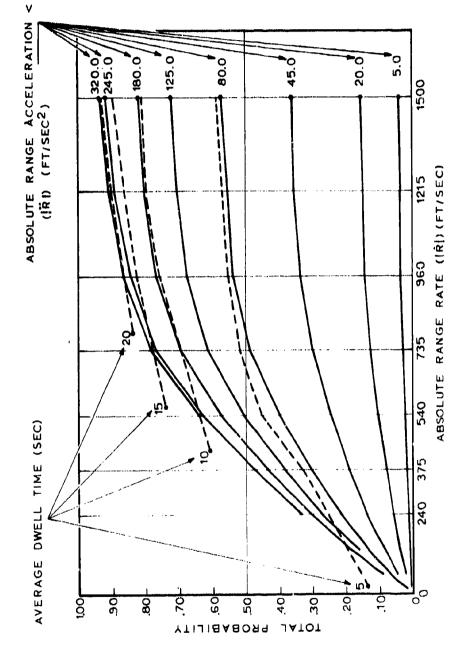
- (U) The tracking parameter interactions were accomplished using a minimum range restriction of 225 feet in order to elimate unrealistic rates and accelerations (inside minimum range of most tracking systems) and in order to reflect the minimum ranges experienced in the VX-4 flight test. Furthermore, the data were collected for three cases ±60° off nose, ±60° off tail, and the full sphere coverage case.
- (U) Figure 6 is representative of the plots for the tracking parameters contained in Appendix B. Referring to Fig. 6, the absolute value of range rate is plotted versus the total probability of occurrence. In cases where the coverage is not full-sphere, a probability normalized to the area of coverage is shown alongside of the total probability. The various solid lines on the graph represent the variations in maximum range accelerations. The average dwell times for the conditions of range rate and accelerations are shown by the dotted lines.
- (U) Referring to Fig. 6, and taking a range rate capability of 960 ft/sec, it can be seen that the probability of occurrence of range acceleration less than 180 ft/sec<sup>2</sup> is .77. In other words, with a 360° tracker with a range rate capability of 960 ft/sec and a range acceleration capability of 180 ft/sec<sup>2</sup>, tracking can be accomplished 77% of the total combat time. Referring to the dotted lines on the same graphs, the average duration of the track under these conditions is approximately 11 seconds. Further details on the tracking performance under these specific conditions can be extracted from the tables in Appendix B.

The parameter interactions studied in the aforementioned manner are:

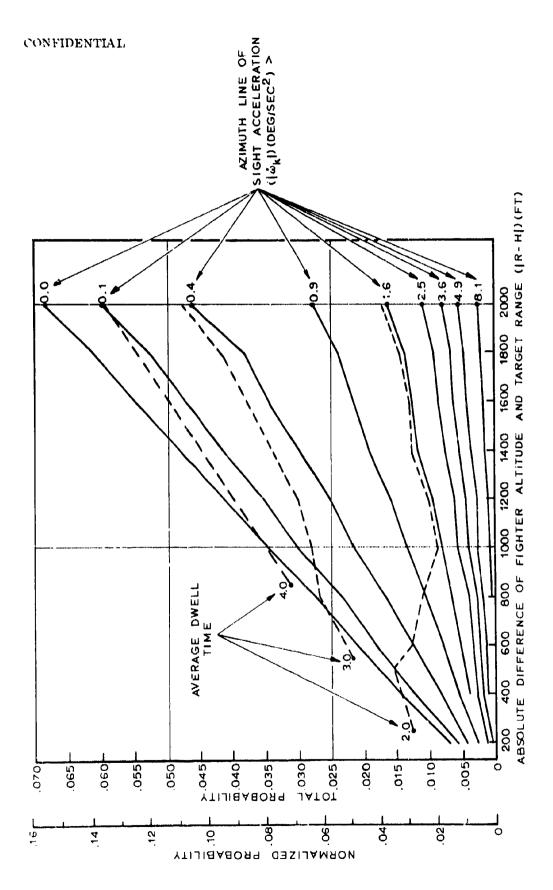
- i. Range rate versus range acceleration
- Azimuth line-of-sight rate versus azimuth line-ofsight acceleration
- iii. Elevation line-of-sight rate versus elevation line-of-sight acceleration.

#### 2. Clutter Interactions

- (U) The clutter interactions, like the tracking parameter interactions, were subject to a minimum range of 225 ft. and for three cases:  $^{1}60^{\circ}$  off nose,  $^{1}60^{\circ}$  off tail, and the full sphere coverage case.
- (U) Figure 7 is representative of the plots for the clutter interactions contained in Appendix B. Referring to Fig. 7, the



DISTRIBUTION OF ABSOLUTE COVERAGE RANGE SPHERE ABSOLUTE FOR TOTAL = 225 FT. FOR SEVERAL PROBABILITY RANGE RATE FOR SEV ACCELERATION LIMITS AND MINIMUM RANGE CUMULATIVE ω FIG



CUMULATIVE PROBABILITY DISTRIBUTION OF ABSOLUTE DIFFERENCE OF FIGHTER ALTITUDE AND TARGET RANGE FOR SEVERAL VALUES OF AZIMUTH LINE OF SIGHT ACCELERATION FOR AI RADAR COVERAGE AND MINIMUM RANGE = 225 FT.

difference in the range to the target and the altitude of the fighter is plotted versus the total probability of occurrence and the normalized probability (normalized to the area coverage, in this case  $\pm 60$  off nose) of occurrence. The solid lines represent the probability that the azimuth line-of-sight rate is greater than the value indicated. The dotted lines represent the average dwell time in clutter. Using Fig. 7 as an example and assuming the altitude clutter return has a spread of  $\pm 1000$  ft, the target is within that region 4.3% of the total combat time and 7.8% of the time when the target is within  $\pm 60^{\circ}$  of the nose of the fighter. Using the same clutter width, the azimuth line-of-sight rate exceeds  $\pm .9^{\circ}/\sec^2$  3.5% of the normalized time for an average duration of 2.3 seconds.

(U) Four types of clutter were investigated as a function of range acceleration, azimuth line-of-sight acceleration, and elevation line-of-sight acceleration. These three parameters, with their time duration, were chosen because they present the severest problem in tracking through a clutter "blind" zone. The servo or memory systems are dependent upon the extrapolation of old information to coast through the clutter. The rate of change of the old information and the associated blind time are vital in order to be able to assess the probability of a track through clutter. For example, assuming a "blin' time" of 2.3 seconds and an azimuth line-of-sight acceleration during this time of .90/sec2, the azimuth angle error of the tracking loop is 2.380. The four types of clutter parameterized are listed below:

#### a. Pulse Doppler Main Beam Clutter (see Fig. 8)

(U) The main beam return of a pulse doppler radar has a frequency shift and a finite width dependent upon the main beam ground return, the antenna beamwidth, and the look-down angle from the velocity vector. Because of this clutter, the area around the mainbeam return is notched out. The data presented in this report can be evaluated for various notch widths.

The equation used to position the main beam clutter notch is given below:

 $VCBT = V_{T} \cos \lambda_{AT} \cos \lambda_{ET}$ 

 $V_{\rm T}$  = target velocity

VCBT = target contribution to the range rate

 $^{\lambda}$ AT = target azimuth angle

λET = target elevation angle

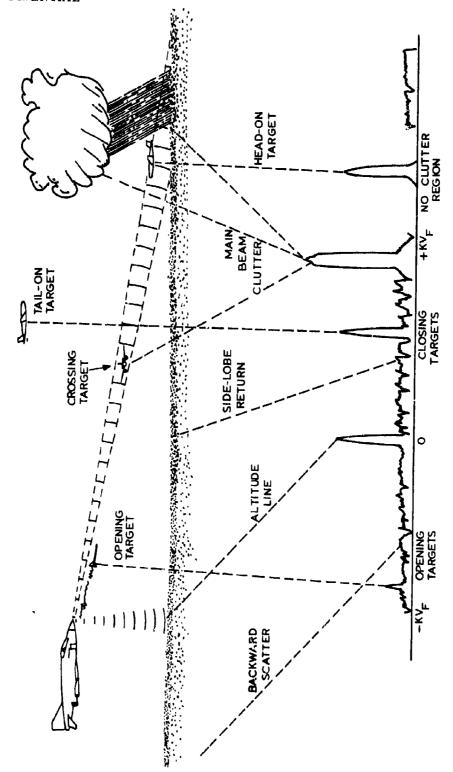


FIG. 8 - DOPPLER CLUTTER SPECTRUM.

- b. Pulse Doppler Altitude Line,  $f_0$  (see Fig. 8)
- (U) The altitude line return in a pulse doppler system is the return from the ground directly below the aircraft which has a doppler shift equal to the velocity of the fighter times the sine of the climb angle. With the fighter flying straight and level, the doppler shift is zero, i.e., the return from the ground is at the transmitted frequency fo. This ground return has, like the main beam clutter, a frequency spread. For this reason and because of the fo notch mechanization of the current AI radars, this study used various notch widths about the transmitted frequency. Therefore, when the range rate to the target is zero, within the tolerance of the notch, the target is said to be in the notch.
  - c. Pulse Mainbeam Clutter (see Fig. 9)
- (U) The pulse mainbeam clutter is the return of the mainbeam from ground. The equation used for this analysis is given below:

DELTA-R = 
$$\frac{HF}{\sin (B + 2.5^{\circ})} - R$$

DELTA-R = range difference between target return and leading edge of mainbeam clutter - ft.

HF = fighter altitude - ft.

B = angle the center of mainbeam makes with the ground - degrees.

2.5° = the first null on the antenna pattern degrees.

R = range to the target - ft.

Various widths of DELTA-R were used in order to approximate the effect of the various size range gates used in the AI radars of today.

- d. Pulse Altitude Line (see Fig. 9)
- (U) The pulse altitude line is the ground return directly below the aircraft. When the range to the target and the altitude of the fighter are close to each other, the target is said to be in altitude line clutter. As before, this clutter is investigated for various widths.

#### 3. Miscellaneous Interactions

(U) The primary interaction conducted in this portion of the study consisted of a preliminary study of radar glint. The objec-

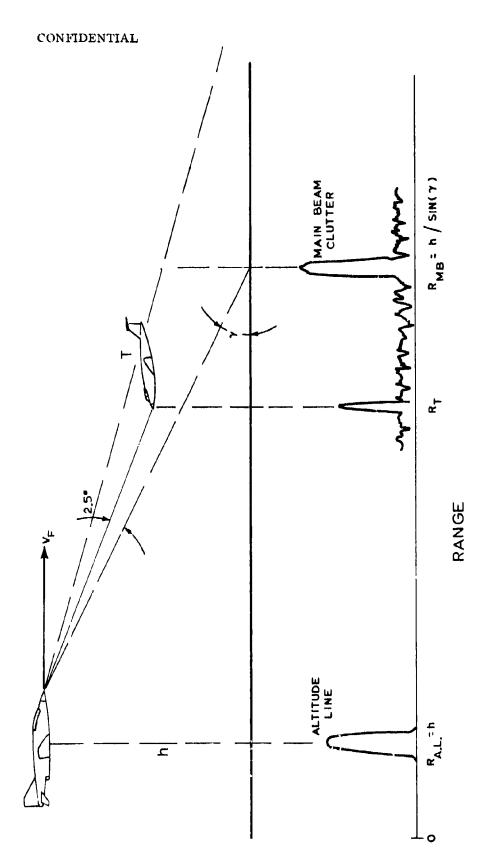


FIG. 9 - PULSE CLUTTER SPECTRUM.

**"我们的一个,我们不是我们的,我们就是我们的,我们就是我们的,我们就是我们的,我们就是我们的,我们就是我们的,我们就是我们的,我们就是我们的,我们就是我们的,** 

tive was to determine whether or not glint is a problem and, if so, to ascertain the magnitude of the problem. To accomplish this, the range to the target versus the rate of change of the target aspect was investigated for various target aspects.

- (U) Another study undertaken in this section was one to determine the minimum range distribution. In the previous study, primary weapon control requirements, it can be noted that the distributions given for range were with regard to maximum range only. This study shows the distribution of the other end of the total range distribution.
- (U) Also given in this section is the distribution of the fighter "g" loading.

#### B. Results

#### 1. Tracking Parameter Interaction

- (U) Table 3 is a summary of weapon system tracking requirement for a dogfight environment. The parameter values given are the tracking loop requirements in terms of rates and accelerations for 90, 95, and 99% probability of each loop retaining lock. Appendix B contains the curves and data tables from which these numbers were extracted. Through use of Appendix B. values for different probabilities may be obtained and average track times may be determined.
- (U) The probability of track in Table 3 is expressed for each track loop independent of the other two track loops. The rates and accelerations given for each loop are dependent and thus various combinations of the two parameters can yield the same probability of track. For a description of this dependence, refer to Appendix B.

#### 2. Clutter Interactions

- (U) Appendix B contains the figures and data used to determine the probabilities of being in clutter and the average duration in the clutter. In addition, track errors at time of emergence from clutter may also be calculated.
- (U) Table 4, in addition to summarizing the pulse and pulse doppler clutters, shows the clutter for a coherent pulse radar. A coherent pulse radar as used herein is basically a short pulse, low PRF radar with doppler filters in the range bins. The coherent pulse radar has the same altitude clutter as a pulse radar but has pulse doppler type main beam clutter. The blind velocity for the main beam clutter notch filter is smaller than in a conventional high PRF pulse

SUMMARY OF WEAPON CONTROL SYSTEM TRACKING REQUIREMENTS. TABLE 3

	AI RA	RADAR COVERAGE	ERAGE	+60 T	+60 TAIL COVERAGE	RAGE	FULL SI	FULL SPHERE COVERAGE	VERAGE
	90%	95%	99%	306	95%	%66	%06	95%	%66
RANGE TRACK LOOP									
RATE (ft/sec)	1700	1700	1800	1700	1700	2000	1400	1700	2200
ACCELERATION $(ft/sec^2)$	210	280	460	210	290	200	310	390	1000
AVERAGE TRACK TIME (sec)	6	10	<b>o</b>	9	<b>r</b>	<b>∞</b>	20	30	100
ELEVATION TRACK LOOP									
RATE (deg/sec)	25	25	50	15	20	35	25	35	72
$ACCELEKATION (deg/sec^2)$	7	15	32	6	15	39	10	19	81
AVERAGE TRACK TIME (sec)	10	11	12	2	80	<b>∞</b>	23	38	143
AZ IKUTH TRACK LOOP									
RATE (deg/sec)	20	25	45	10	15	30	20	30	72
$ACCELERATION$ ( $deg/sec^2$ )	လ	10	34	6	13	44	6	20	81
AVERAGE TRACK TIME (sec)	6	11	12	ţ-	œ	∞.	24	38	165

TABLE 4 - CLUTTER SUMMARY FOR AI RADAR.

	<u>na</u>	PULSE	PULSE DOPPLER	OPPLER	COHERENT PULSE	PULSE
	MBC	AL	MBC	$f_{ m O}$	ивс	AL
SIZE NOTCH USED	300 (FT)	+1000 -(FT)	+200 (FT/SEC)	+150 +40 (FT/SEC) (FT/SEC)	+40 (FT/SEC)	+1000 -(FT)
PROBABILITY OF OCCURENCE	.005	870.	060.	. 083	.0001	.078
AVERAGE DWELL TIME (SEC)	1.1	3.9	1.8	2.4	1.0	3.9
.05 PROBABILITY OF BREAK LOCK ERROR						
a) RANGE (FT)	*	115			*	115
RANGE RAGE (FT/SEC)			75	61		
b) ELEVATION ANGLE (DEGREES)	*	1.7	. 22	.34	*	1.7
c) AZIMUTH ANGLE (DEGREES)	*	1.01	. 15	. 43	*	1.01

NOT MEASURABLE BY . 05 CRITERIA

doppler radar. A typical value for this notch filter is ±40 ft/sec.

- (U) The 0.05 probability of break lock error contained in Table 4 is the average error in the tracking loop that is seen when the target comes out of the clutter. This error or greater than this error is experienced 5% of the time the target is within AI radar coverage.
- (C) As can be seen in Table 4, the pulse doppler system has the severest problem with clutter. 17% of the time in AI radar coverage, the PD radar is in clutter. It can also be seen that in order to effectively use a short pulse radar, the altitude clutter problem must be overcome. A signal strength analysis will provide better insight into the severity of this problem.

#### 3. Miscellaneous Interactions

- (U) For a complete description of the interactions performed in this section, refer to Appendix B.
- (C) In looking at the minimum range of a dogfight, it was shown that 2.5% of the engagement time the two aircraft were within 765 ft. Of the time the target was within the fighters AI radar coverage, 2.5% of the time the target was within 1200 ft.
- (C) In the investigation of the aircraft "g" loading, it was shown that the fighter aircraft pulled 6 "g" or better, 5% of the time.
- (C) In a preliminary investigation of glint, it was suggested that it is possible to increase the tracking loops' bandwidth at short ranges without worsening the glint problems. A notable exception to this is the head on case where the target is nonmaneuvering prior to a flyby. In this case, an increase in bandwidth will probably cause an earlier break-lock.

#### IV. CONCLUSIONS

- A. (C) In Section II of this report, the verification of the NADC manned air combat simulation by VX-4 flight tests was shown.
- B. (C) In Section II of this report, the weapon control parameter requirements, with the exception of coverage requirements, were shown to be independent of aircraft and weapons.
- C. (C) In the comparison of Tables 2 and 3, it can be seen that distribution of the weapon control parameters is not normal. The impact of this conclusion is that the actual distribution, as shown in Section III, is required in order to arrive at valid weapon control parameters.
- D. (C) It was shown in Section III that the rates and accelerations for each tracking loop are dependent and that they must be considered jointly when deriving realistic tracking requirements. To look at the parameters independently, one could erroneously derive tracking requirements too severe.
- E. (C) Due to the length of time in clutter notches (Table 4), it is concluded that high PRF pulse doppler radar should not be used in the dogfight engagement.
- F. (C) The altitude line presents the severest clutter problem for the short pulse mode. The occurrences of main beam clutter for pulse and coherent pulse radar modes are small enough to be ignored.
- G. (C) Table 5 presents the probability of track for the AERO-1A, AWG-9, and AWG-10 AI radars operating in the short pulse mode. This table is useful in determining the areas in which improvements could be made in order to improve overall capability.
- (C) This table, although specifying track loop probabilities, gives the independent probabilities for the parameters listed with the exception of gimbal angle by which the rest of the parameters were limited. The "worst case" total track probabilities assume the independence of the parameters. The "best case" total track probabilities assume total dependence. The actual track probability for each radar is between these two extremes and in order to ascertain this actual probability, the correlation of all these parameters must be considered. This is best accomplished in a tracking model of each radar with special emphasis on the treatment of altitude line clutter.
- H. (C) It is apparent throughout this report that the expansion of the coverage area would yield the most gain in track time. However,

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TABLE 5 - PROBABILITY OF TRACK FOR PRESENT AI RADARS.

	AER	<u> 1A</u>	AW	G-9	AWC	<u>i-10</u>
	%	AVG. DURATION (sec.)	%	AVG. DURATION (sec.)	%	AVG. DURATION (sec.)
PROBABILITY OF BEING IN						
GIMBAL ANGLE	44.8	12	39.8	12	44.8	12
RANGE*	99	125	99	125	99	125
RANGE TRACK*	70.8	6	90.1	9	95.4	10.5
ELEVATION TRACK*	89.1	9.7	95.6	11	89.1	9.7
AZIMUTH TRACK*	93.2	10.2	97.5	11	93.2	10.2
PROBABILITY OF BEING FREE OF ALTITUDE LINE CLUTTER* MAIN BEAM CLUTTER*	<b>92.2</b> <b>99.</b> 5	112 220	92.2 99.5	11 <b>2</b> 220	92.2 99.5	112 220
"WORST CASE," TOTAL TRACK PROABILITY	23.	. 9%	3	0.4%	32	2 . 2%
"BEST CASE," TOTAL TRACK PROBABILITY	31	. 7%	3	5.9%	39	9.9%

<sup>\*</sup>VALUES GIVEN ARE WHILE IN GIMBAL ANGLE

it is also shown that the size and shape of the coverage area greatly influences the remainder of the parameters. Furthermore, with expansion of the coverage area towards a hemisphere, the present type of tracking loops would be inadequate to handle the situation.

### V. RECOMMENDATIONS

- A. (C) It is recommended that radar tracking models (currently under development) be utilized to more precisely define the dogfight capabilities of present radars. These tracking models would be further utilized for the final determination of the modifications to be made to the AI radars to improve their dogfight capabilities.
- B. (C) It is recommended that adaptive bandwidth tracking loops be investigated as a means of coordinating the AI and the dogfight requirements.
- C. (C) It is recommended that a pulse clutter model, including antenna patterns and terrain reflectivity, be incorporated into the tracking model. This is necessary in order to properly size the clutter notches and to optimize the track-through requirements presented in this report.
- D. (C) This study shows that glint should be incorporated into the tracking model.
- E. (C) As explained in this report, no single data source is totally descriptive of the dogfight environment. It is recommended that an additional data source, NMC-ACM free combat flight test data, be utilized to forther verify and strengthen the conclusions of this report.
- F. (C) The desirability of a total coverage tracker is evident. It can be noted that the present range-angle tracking system presents extremely high rates and accelerations around the beam of the aircraft. It is recommended that an investigation of alternative tracking methods be made. Candidate systems would be adaptive bandwidth tracking and a new tracker based on inertial coordinates.
- G. (C) Although electro-optical trackers could be utilized to provide angle information, range information would still be required for the development of launch criteria. It is recommended that an investigation of alternative ranging systems be made for use with electro-optical trackers.

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## VII. ACKNOWLEDGEMENTS

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### IX. APPENDIX

### A. Primary Weapon Control Requirements

### 1. Data Reduction Program

The data reduction program for this phase of the study was originally written to provide the desired data from the data collected by NADC on their manned simulator. The data provided by the NADC simulation are shown in Table A-1. With much modification of the data reduction program, the VX-4 data were used to obtain the same data output. The VX-4 tape output (as supplied by NWC) is shown in Table A-2.

The flow diagram of the data reduction program used in this phase of the study is shown in Figure A-1.

The following paragraphs are a description and derivation of the equations used in this data reduction program.

### TABLE A-1

### QUANTITIES PRINTED OUT BY JOHNSVILLE SIMULATION

- X relative position in earth coordinates
- Y relative position in earth coordinates
- H altitude of each aircraft in earth coordinates

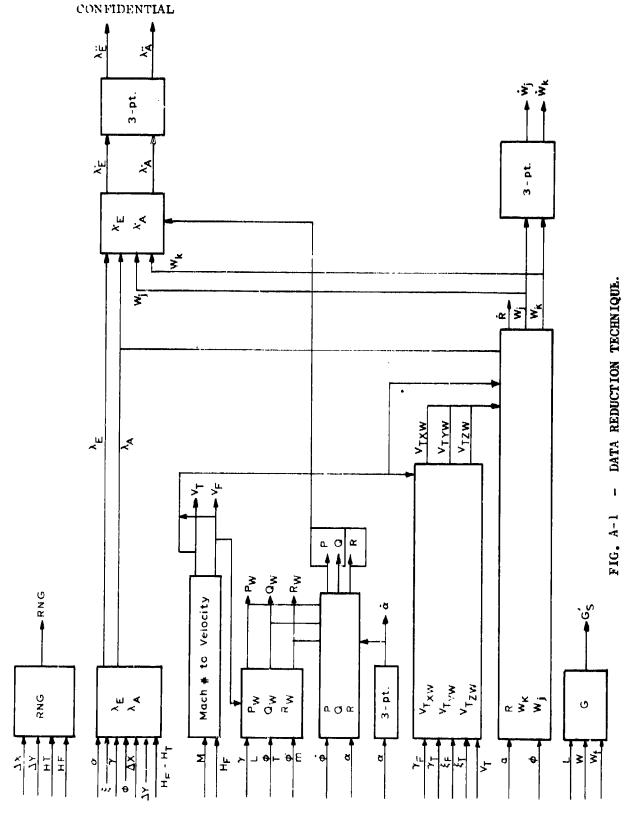
The following quantities are given for both aircraft.

- $\psi$  course angle in degrees
- O climb angle in degrees
- Ø roll angle of velocity vector
- Ø roll rate
- & angle of attack
- L lift
- T thrust
- $W_{\mathbf{F}}$  weight of fuei
- M mach number
  - W weight of fighter
  - t time

### TABLE A-2

# QUANTITIES PRINTED OUT BY NWC REDUCED VX-4 FLIGHT TESTS

- X X position
- Y Y position
- Z Z position
- $\lambda$  angle off boresight
- $\boldsymbol{A}_{\boldsymbol{n}}$  acceleration perpendicular to the velocity vector
- $\mathbf{A}_{\mathbf{L}}$  acceleration along the velocity vector
  - t time



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#### a. Matrix Notation

The following are expansions of matrices which will hereafter be expressed in their shorthand forms.

$$\begin{bmatrix} \cos \xi & \sin \xi & 0 \\ -\sin \xi & \cos \xi & 0 \\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} \xi \end{bmatrix}$$

$$\begin{bmatrix} \cos \gamma & 0 & -\sin \gamma \\ 0 & 1 & 0 \\ \sin \gamma & 0 & \cos \gamma \end{bmatrix} = \begin{bmatrix} \gamma \end{bmatrix}$$

$$\begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \beta & \sin \beta \\ 0 & -\sin \beta & \cos \beta \end{bmatrix} = \begin{bmatrix} \phi \end{bmatrix}$$

$$\begin{bmatrix} \cos \alpha & 0 & -\sin \alpha \\ 0 & 1 & 0 \\ \sin \alpha & 0 & \cos \alpha \end{bmatrix} = \begin{bmatrix} \alpha \end{bmatrix}$$

$$\begin{bmatrix} \cos \lambda_A & \sin \lambda_A & 0 \\ -\sin \lambda_A & \cos \lambda_A & 0 \\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} \lambda_A \end{bmatrix}$$

$$\begin{bmatrix} \cos \lambda_E & 0 & -\sin \lambda_E \\ 0 & 1 & 0 \\ \sin \lambda_E & 0 & \cos \lambda_E \end{bmatrix} = \begin{bmatrix} \lambda_E \end{bmatrix}$$

The inverses of these matrices are the following:

$$\begin{bmatrix} \cos \xi & -\sin \xi & 0 \\ \sin \xi & \cos \xi & 0 \\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} \xi \end{bmatrix}^{-1}$$

$$\begin{bmatrix} \cos \gamma & 0 & \sin \gamma \\ 0 & 1 & 0 \\ -\sin \gamma & 0 & \cos \gamma \end{bmatrix} = \begin{bmatrix} \gamma \end{bmatrix}^{-1}$$

$$\begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \beta & -\sin \beta \\ 0 & \sin \beta & \cos \delta \end{bmatrix} = \begin{bmatrix} \phi \end{bmatrix}^{-1}$$

$$\begin{bmatrix} \cos \alpha & 0 & \sin \alpha \\ 0 & 1 & 0 \\ -\sin \alpha & 0 & \cos \alpha \end{bmatrix} = \begin{bmatrix} \alpha \end{bmatrix}^{-1}$$

$$\begin{bmatrix} \cos \gamma_A & -\sin \gamma_A & 0 \\ \sin \gamma_A & \cos \gamma_A & 0 \\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} \lambda_A \end{bmatrix}^{-1}$$

$$\begin{bmatrix} \cos \gamma_A & -\sin \gamma_A & 0 \\ \sin \gamma_A & \cos \gamma_A & 0 \\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} \lambda_A \end{bmatrix}^{-1}$$

$$\begin{bmatrix} \cos \lambda_E & 0 & \sin \lambda_E \\ 0 & 1 & 0 \\ -\sin \lambda_E & 0 & \cos \lambda_E \end{bmatrix} = \begin{bmatrix} \lambda_E \end{bmatrix}^{-1}$$

### b. Calculation of Gimbal Angles

Define an earth axis coordinate system such that R  $_{\rm XE}$  =  $\Delta$  X, R  $_{\rm YE}$  =  $\Delta$  Y, and R  $_{\rm ZE}$  =  $\Delta$  H where H corresponds to altitude. The range between the fighter and target is then given by

$$RNG = \sqrt{R_{XE}^2 + R_{YE}^2 + R_{ZE}^2}$$
 (A-1)

In the body axis system of an aircraft these become

$$\begin{bmatrix} R_{X} \\ R_{Y} \\ R_{Z} \end{bmatrix} = [\alpha] [\phi] [\gamma] [\xi] \begin{bmatrix} R_{XE} \\ R_{YE} \\ R_{ZE} \end{bmatrix}$$
(A-2)

Where the aircraft has an angle of attack  $\alpha$  and a sideslip angle assumed to be zero. In the antenna axis, the range lies along the line-of-sight or X-axis therefore

$$\begin{bmatrix} R_{X} \\ R_{Y} \\ R_{Z} \end{bmatrix} = \begin{bmatrix} \lambda_{A} \end{bmatrix} - 1 \begin{bmatrix} \lambda_{E} \end{bmatrix} - 1 \begin{bmatrix} RNG \\ 0 \\ 0 \end{bmatrix}$$
(A-3)

Expanding A-2 and A-3 and equating:

$$\begin{bmatrix} \cos \alpha \cos \gamma \cos \xi & -\sin \alpha & (\sin \theta \sin \xi + \cos \theta \sin \gamma \cos \xi) \end{bmatrix} R_{XE} + \\ \begin{bmatrix} -\cos \theta \sin \xi + \sin \theta \sin \gamma \cos \xi \end{bmatrix} R_{XE} + \\ \begin{bmatrix} \sin \alpha \cos \gamma \cos \xi + \cos \alpha & (\sin \theta \sin \xi + \cos \theta \sin \gamma \cos \xi) \end{bmatrix} R_{XE} \\ \begin{bmatrix} \cos \alpha \cos \gamma \sin \xi - \sin \alpha & (-\sin \theta \cos \xi + \cos \theta \sin \gamma \sin \xi) \end{bmatrix} R_{YE} + \\ \begin{bmatrix} \cos \theta \cos \xi + \sin \theta \sin \gamma \sin \xi \end{bmatrix} R_{YE} + \\ \begin{bmatrix} \sin \alpha \cos \gamma \sin \xi + \cos \alpha & (-\sin \theta \cos \xi + \cos \theta \sin \gamma \sin \xi) \end{bmatrix} R_{YE} + \\ \begin{bmatrix} -\cos \alpha \sin \gamma - \sin \alpha \cos \theta \cos \gamma \end{bmatrix} R_{ZE} \\ \begin{bmatrix} RNG \cos \lambda_E \cos \lambda_A \\ RNG \cos \lambda_E \sin \lambda_A \end{bmatrix} (A-4) + \\ \begin{bmatrix} -\sin \alpha \sin \gamma + \cos \alpha \cos \theta \cos \gamma \end{bmatrix} R_{ZE} \\ \begin{bmatrix} -RNG \sin \lambda_E & (-\cos \theta \sin \gamma + \cos \theta \cos \theta \cos \gamma) \end{bmatrix} R_{ZE} \\ \end{bmatrix}$$

Solving the three equations of the matrices for  $~\lambda_E$  and  $~\lambda_A$ 

$$\lambda_{E} = -\sin^{-1} \left( \begin{bmatrix} \sin \alpha \cos \gamma & \cos \xi + \cos \alpha (\sin \emptyset & \sin \xi + \cos \emptyset & \sin \gamma \cos \xi) \end{bmatrix} R_{XE} + \begin{bmatrix} \sin \alpha & \cos \gamma & \sin \xi + \cos \alpha (-\sin \emptyset & \cos \xi + \cos \emptyset & \sin \gamma & \sin \xi) \end{bmatrix} R_{YE} + \begin{bmatrix} -\sin \alpha & \sin \gamma + \cos \emptyset & \cos \alpha & \cos \gamma \end{bmatrix} R_{ZE} \right)$$

$$RNG \qquad (A-5)$$

$$\lambda_{A} = \tan^{-1} \left[ -\cos \theta \sin \xi + \sin \theta \sin \gamma \cos \xi \right] R_{XE} + \left[ \cos \theta \cos \xi + \frac{1}{2} + \sin \theta \sin \gamma \sin \xi \right] R_{YE} + \left[ \sin \theta \cos \gamma \right] R_{ZE} \right]$$

$$\left[ \cos \alpha \cos \gamma \cos \xi - \sin \alpha \left( \sin \theta \sin \xi + \cos \theta \sin \gamma \cos \xi \right) \right] R_{XE} + \left[ \cos \alpha \cos \gamma \sin \xi - \sin \alpha \left( \sin \theta \cos \xi + \cos \theta \sin \gamma \sin \xi \right) \right] R_{YE} + \left[ -\cos \alpha \sin \gamma - \sin \alpha \cos \theta \cos \gamma \right] R_{ZE}$$

$$\left[ -\cos \alpha \sin \gamma - \sin \alpha \cos \theta \cos \gamma \right] R_{ZE}$$

$$(A-6)$$

# c. Calculation of W and R

In the wind coordinate axis of the target, the velocity is entirely in the X-direction. Transforming this velocity vector to the wind axis of the fighter, the components of velocity become

$$\begin{bmatrix} v_{TXW} \\ v_{TYW} \\ v_{YZW} \end{bmatrix} = \begin{bmatrix} \gamma_F \end{bmatrix} \begin{bmatrix} \xi_F \end{bmatrix} \begin{bmatrix} \xi_T \end{bmatrix}^{-1} \begin{bmatrix} \gamma_T \end{bmatrix}^{-1} \begin{bmatrix} v_T \\ 0 \\ 0 \end{bmatrix}$$
(A-7)

Expanding the matrix equation:

These are the components of the target velocity in the modified wind axis of the fighter where the roll of the fighter has not yet been included. The components of velocity of the fighter can now be subtracted and the difference in the velocities transformed to the antenna axis of the fighter to give

$$\begin{bmatrix} \dot{R} \\ RW_{j} \\ RW_{K} \end{bmatrix} = \begin{bmatrix} \lambda_{E} \end{bmatrix} \begin{bmatrix} \lambda_{A} \end{bmatrix} \begin{bmatrix} \alpha \end{bmatrix} \begin{bmatrix} \emptyset \end{bmatrix} \begin{bmatrix} V_{TXW} - V_{F} \\ V_{TYW} - O \\ V_{TZW} - O \end{bmatrix}$$
(A-11)

Here the roll angle of the fighter has been included. Expanding A-11 and solving for  $W_1$ ,  $W_K$ , and  $\dot{R}$  results in

$$W_{K} = \begin{cases} [-\sin_{A} \cos \alpha] (V_{TXW} - V_{F}) - [\sin^{\lambda}_{A} \sin \alpha \sin \phi + \cos^{\lambda}_{A} \cos \phi] V_{TYW} \\ + [\sin_{\lambda_{A}} \sin \alpha \cos \theta + \cos^{\lambda}_{A} \sin \theta] V_{TZW} \end{cases} / RNG \qquad (A-12)$$

$$-W_{j} = \begin{cases} [\sin_{\lambda_{E}} \cos^{\lambda}_{A} \cos \alpha + \cos^{\lambda}_{E} \sin \alpha] (V_{TXW} - V_{F}) \\ + [\sin_{\lambda_{E}} (\cos^{\lambda}_{A} \sin \alpha \sin \theta + \sin^{\lambda}_{A} \cos \theta) - \cos^{\lambda}_{E} \end{cases}$$

$$\cos_{\alpha} \sin_{\theta} V_{TYW} - [\sin_{\lambda_{E}} \cos^{\lambda}_{A} \cos^{\theta} \cos_{\alpha} - \sin^{\lambda}_{E} \sin^{\lambda}_{A} \cos^{\theta} - \cos^{\theta} \cos^{\alpha} \cos^{\alpha}_{E}] V_{TZW} \end{cases} / RNG$$

$$\sin_{\theta} - \cos_{\theta} \cos_{\alpha} \cos^{\alpha}_{E} V_{TZW} \end{cases} / RNG$$

$$(A-13)$$

$$\dot{R} = [\cos_{\lambda_{E}} \cos_{\lambda_{A}} \cos_{\alpha} + \sin^{\lambda}_{E} \sin_{\alpha}] (V_{TXW} - V_{F})$$

$$+ [\cos_{\lambda_{E}} (\cos^{\lambda}_{A} \sin_{\alpha} \sin_{\theta} + \sin^{\lambda}_{A} \cos_{\theta}) + \sin^{\lambda}_{E} \cos_{\alpha} \sin_{\theta}] V_{TYW}$$

$$- [\cos_{\lambda_{E}} (\cos^{\lambda}_{A} \sin_{\alpha} \cos_{\theta} - \sin^{\lambda}_{A} \sin_{\theta}) + \sin^{\lambda}_{E} \cos_{\alpha} \cos_{\theta}] V_{TZW}$$

$$(A-14)$$

## d. Calculation of Gimbal Angle Rates

The aircraft is assumed to be acted upon by the forces of thrust, gravity, lift, and drag. Thrust is defined to be aligned with the body X-axis of the aircraft and an angle of attack  $\alpha$  is assumed. In the wind axis system of the aircraft, the acceleration is given by

$$\frac{1}{m} \begin{bmatrix} \mathbf{\Sigma} \mathbf{F}_{XW} \\ \mathbf{\Sigma} \mathbf{F}_{YW} \\ \mathbf{\Sigma} \mathbf{F}_{ZW} \end{bmatrix} = \begin{bmatrix} \dot{\mathbf{V}}_{\mathbf{F}} \\ \mathbf{R}_{\mathbf{W}} \mathbf{V}_{\mathbf{F}} \\ -\mathbf{Q}_{\mathbf{W}} \mathbf{V}_{\mathbf{F}} \end{bmatrix} \tag{A-15}$$

where  $\mathbf{R}_{\mathbf{W}}$  and  $\mathbf{Q}_{\mathbf{W}}$  are the aircraft angular rates about the wind axis.

$$\frac{1}{m} \begin{bmatrix} \mathbf{\Sigma} \mathbf{F}_{XW} \\ \mathbf{\Sigma} \mathbf{F}_{YW} \\ \mathbf{\Sigma} \mathbf{F}_{ZW} \end{bmatrix} = \begin{bmatrix} \frac{1}{m} \begin{bmatrix} -D \\ 0 \\ -L \end{bmatrix} + \begin{bmatrix} \alpha \end{bmatrix} \begin{bmatrix} T \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} \emptyset \end{bmatrix} \begin{bmatrix} \gamma \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ mg \end{bmatrix}$$
(A-16)

where gravitational force is changed from the earth axis system to wind axis system. Expanding (A-16) and substituting in (A-15) yields:

$$\dot{V}_{F} = \frac{T \cos \alpha - D}{m} - g \sin \gamma \qquad (A-17)$$

$$R_W = g \sin \theta \cos \gamma / V_F$$
 (A-18)

$$Q_{W} = (-g \cos \theta \cos \gamma + \frac{L - T \sin \alpha}{m})/V_{F} \qquad (A-19)$$

 $P_W$  is assumed to be equal to  $\rlap{/}{p}$  whose value is given.

The angular rates in the wind axis system are related to the angular rates in the body axis system by

$$\begin{bmatrix} P \\ Q \\ R \end{bmatrix} = \begin{bmatrix} 0 \\ \dot{\alpha} \\ 0 \end{bmatrix} + \begin{bmatrix} \alpha \end{bmatrix} \begin{bmatrix} P_W \\ Q_W \\ R_W \end{bmatrix}$$
(A-20)

The expanded matrix equation results in:

$$P = P_{W} \cos \alpha - R_{W} \sin \alpha \qquad (A-21)$$

$$Q = \dot{\alpha} + Q_{W} \tag{A-22}$$

$$R = P_{W} \sin \alpha + R_{W} \cos \alpha \qquad (A-23)$$

The gimbal angle rates are related to P, Q, and R in the following way

$$\begin{bmatrix} W_{i} \\ W_{j} \\ W_{K} \end{bmatrix} = \begin{bmatrix} \lambda_{E} \end{bmatrix} \begin{bmatrix} \lambda_{A} \end{bmatrix} \begin{bmatrix} P \\ Q \\ R \end{bmatrix} + \begin{bmatrix} \lambda_{E} \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ \lambda_{A} \end{bmatrix} + \begin{bmatrix} 0 \\ \lambda_{E} \\ 0 \end{bmatrix}$$
(A-24)

The equation in the expanded matrix equation are:

$$W_i = P \cos \lambda_E \cos \lambda_A + Q \cos \lambda_E \sin \lambda_A - R \sin \lambda_A - \dot{\lambda}_A \sin \lambda_E$$
(A-24)

$$W_{j} = -P \sin \lambda_{A} + Q \cos \lambda_{A} + \lambda_{E}$$
 (A-25)

$$W_{K} = P \sin_{\lambda_{E}} \cos_{\lambda_{A}} + Q \sin_{\lambda_{E}} \sin_{\lambda_{A}} + R \cos_{\lambda_{E}} + \lambda_{A} \cos_{\lambda_{E}}$$
(A-26)

Solving for  $\overset{\bullet}{\lambda_A}$  and  $\overset{\bullet}{\lambda_E}$  in terms of W  $_j$  and W  $_K$  yields:

$$\dot{\lambda}_{E} = W_{j} + P \sin \lambda_{A} - Q \cos \lambda_{A}$$

$$\dot{\lambda}_{A} = \left[W_{K} - P \sin \lambda_{E} \cos \lambda_{A} - Q \sin \lambda_{E} \sin \lambda_{A} - R \cos \lambda_{E}\right]/\cos \lambda_{E}$$

```
Glossary
```

 $\xi_n = yaw angle of fighter$ 

ξ<sub>m</sub> = yaw angle of target

 $\gamma_{\rm F}$  = pitch angle of fighter

 $\gamma_{\rm m}$  = pitch angle of target

Ø = roll angle of fighter

α = angle of attack of fighter

 $\lambda_{\Lambda}$  = gimbal angle in azimuth

 $\lambda_{p}$  = gimbal angle in elevation

R<sub>vv</sub> = X-coordinate

R<sub>vr</sub> = Y-coordinate

R<sub>7F</sub> = Z-coordinate

R<sub>v</sub> = X-coordinate

R, = Y-coordinate

 $R_7 = 2$ -coordinate

of Range between fighter

and target in earth axis system

of Range between fighter

and target in body axis system

RNG = Range from fighter to target

V<sub>m</sub> = Velocity of target

V<sub>TXW</sub> = X-coordinate

V<sub>TYW</sub> = Y-coordinate

V<sub>TZW</sub> = Z-coordinate

of velocity of target in modified

wind axis system of fighter

R = Closing velocity between fighter and target

W, - Space line of sight rate measured about line of sight X-axis

 $W_4$  = Space line-of-sight rate measured about line of sight Y-axis

 $W_{\nu}$  = Space line of sight rate measured about line of sight 2-axis

V<sub>n</sub> = Velocity of fighter  $\dot{v}_{\nu}$  = Acceleration of fighter X-axis Qw = Angular rate of fighter in wind Y-axis R<sub>L</sub> = Axis system measured about Z-axis F<sub>XW</sub> = X-component of forces on fighter Fyw = Y-component in wind axis system F<sub>ZW</sub> = Z-component T = thrust D = drag L = lift g = gravitational constant m = mass of fighter and fuel  $\dot{\alpha}$  = rate of change of angle of attack  $\dot{\lambda}_{A}$  = rate of change of gimbal azimuth angle  $\dot{\lambda}_{_{\rm F}}$  = rate of change of gimbal elevation angle

2. Azimuth versus elevation of the target versus frequency of occurrence data plots are contained in Fig. A-2 through Fig. A-15.

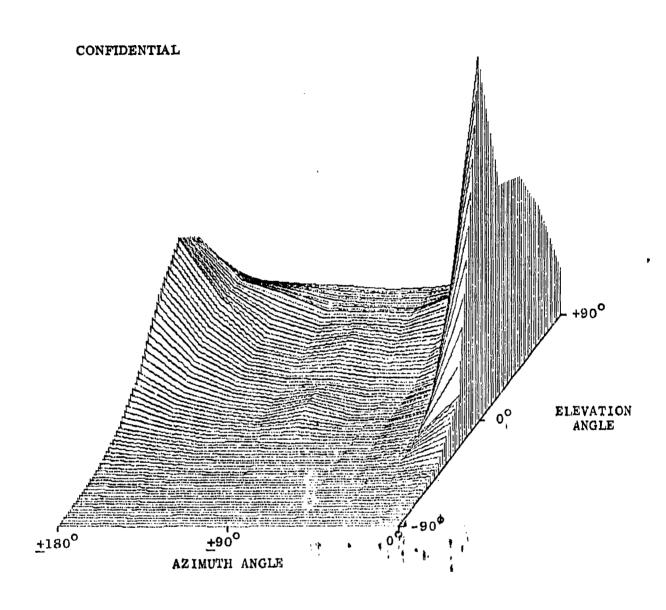


FIG. A-2 - TAPE 1 - FIGHTER 1 - ELEVATION ANGLE VERSUS AZIMUTH ANGLE VERSUS FREQUENCY OF OCCURRENCE.

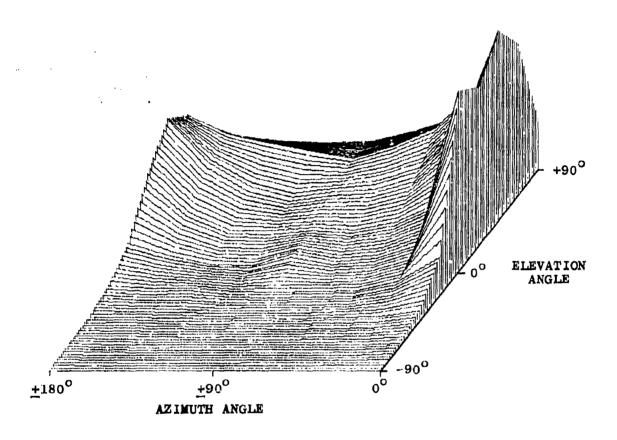


FIG. A-3 - TAPE 1 - FIGHTER 2 - ELEVATION ANGLE VERSUS AZIMUTH ANGLE VERSUS FREQUENCY OF OCCURRENCE.

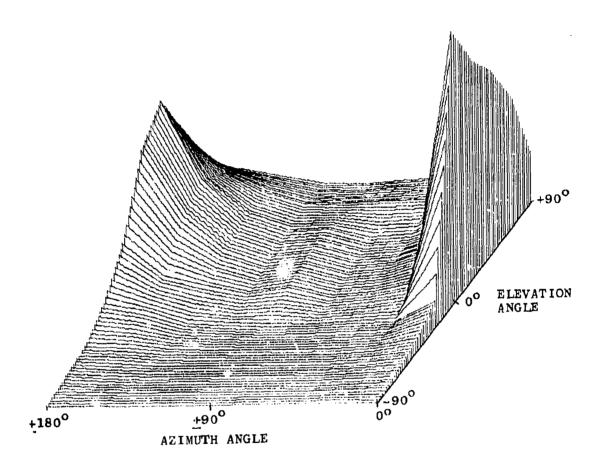


FIG. A-4 - TAPE 2 - FIGHTER 1 - ELEVATION ANGLE VERSUS AZIMUTH ANGLE VERSUS FREQUENCY OF OCCURRENCE.

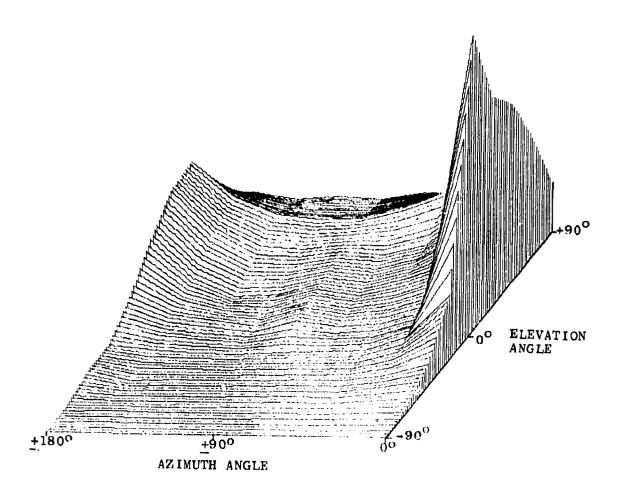


FIG. A-5 - TAPE 2 - FIGHTER 2 - ELEVATION ANGLE VERSUS AZIMUTH ANGLE VERSUS FREQUENCY OF OCCURRENCE.

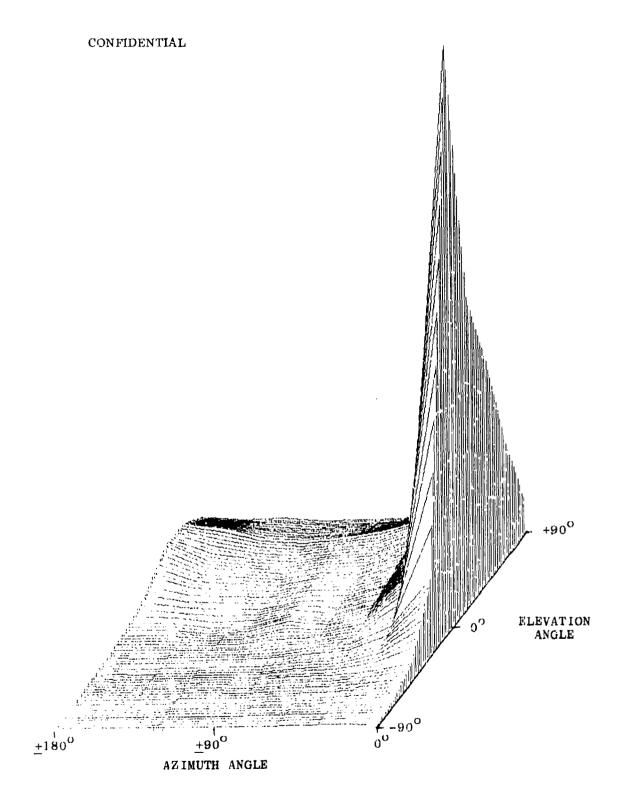


FIG. A-6 - TAPE 3 - FIGHTER 1 - ELEVATION ANGLE VERSUS AZIMUTH ANGLE VERSUS FREQUENCY OF OCCURRENCE.

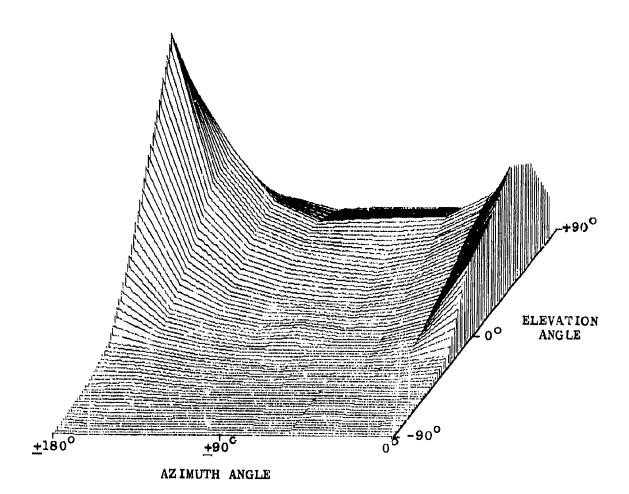


FIG. A-7 - TAPE 3 - FIGHTER 2 - ELEVATION ANGLE VERSUS AZIMUTH ANGLE VERSUS FREQUENCY OF OCCURRENCE.

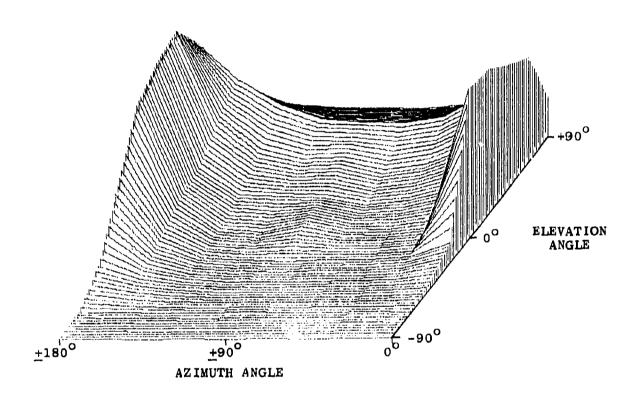
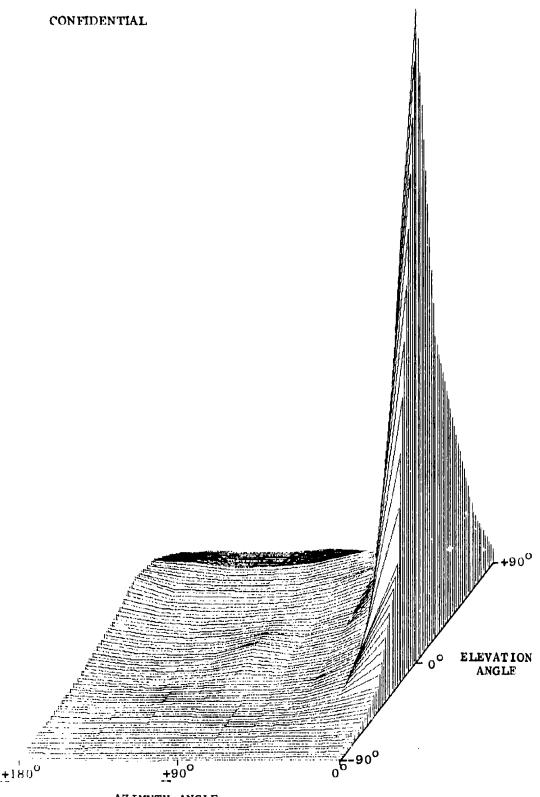


FIG. A-8 - TAPE 4 - FIGHTER 1 - ELEVATION ANGLE VERSUS AZIMUTH ANGLE VERSUS FREQUENCY OF OCCURRENCE.



AZIMUTH ANGLE

FIG. A-9 - TAPE 4 - FIGHTER 2 - ELEVATION ANGLE VERSUS AZIMUTH ANGLE VERSUS FREQUENCY OF OCCURRENCE.

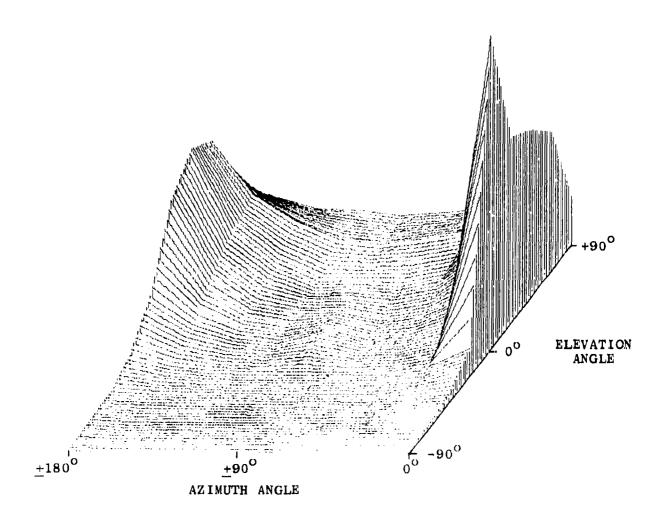


FIG. A-10 - TAPE 5 - FIGHTER 1 - ELEVATION ANGLE VERSUS AZIMUTH ANGLE VERSUS FREQUENCY OF OCCURRENCE.

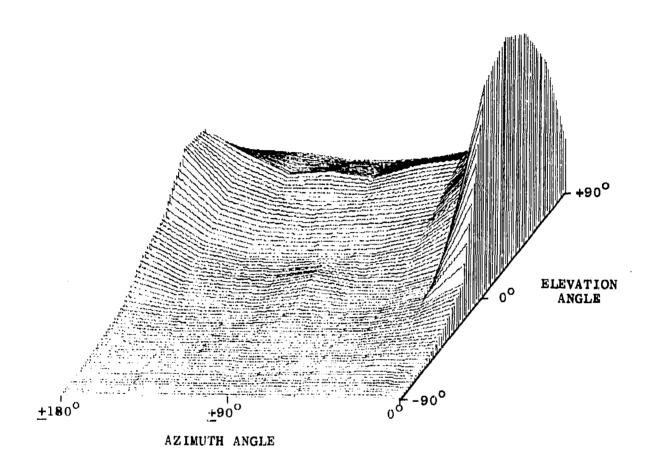


FIG. A-11- TAPE 5 - FIGHTER 2 - ELEVATION ANGLE VERSUS AZIMUTH ANGLE VERSUS FREQUENCY OF OCCURRENCE.

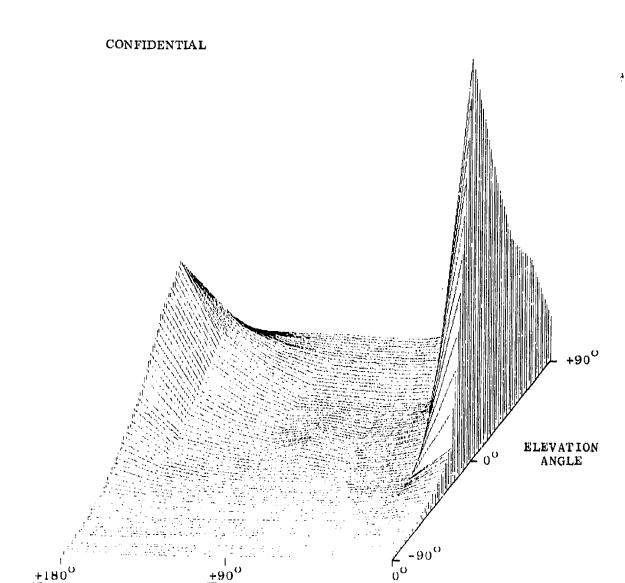


FIG. A-12- TAPE 6 - FIGHTER 1 - ELEVATION ANGLE VERSUS AZIMUTH ANGLE VERSUS FREQUENCY OF OCCURRENCE.

AZIMUTH ANGLE

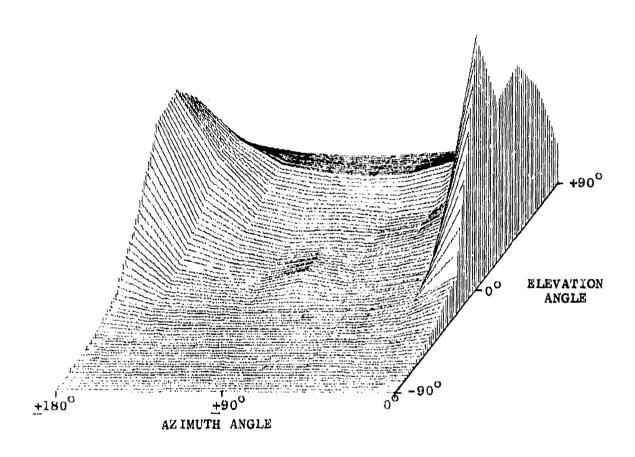


FIG. A-13 - TAPE 6 - FIGHTER 2 - ELEVATION ANGLE VERSUS AZIMUTH ANGLE VERSUS FREQUENCY OF OCCURRENCE.

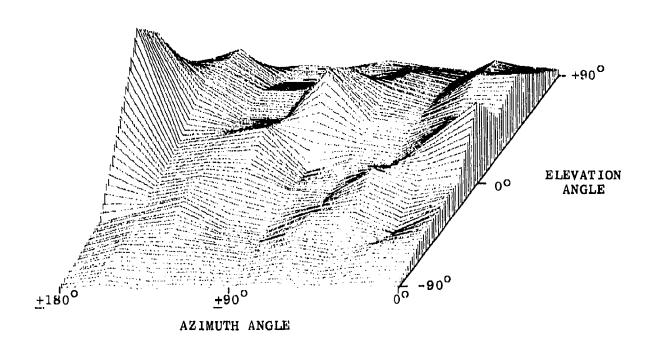


FIG.A-14 - TAPE 101 - FIGHTER 1 - ELEVATION ANGLE VERSUS AZIMUTH ANGLE VERSUS FREQUENCY OF OCCURRENCE.

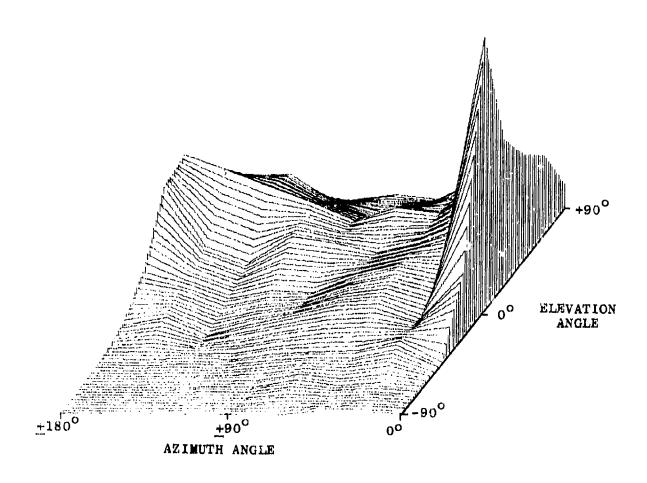
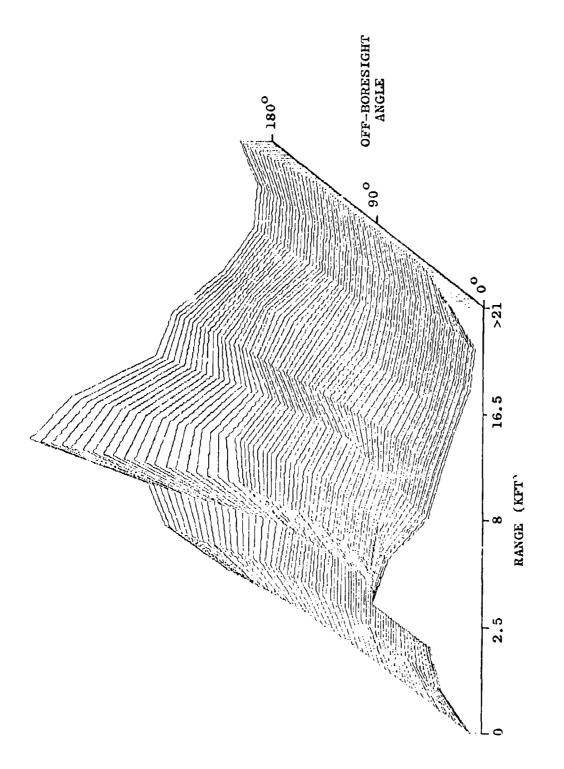


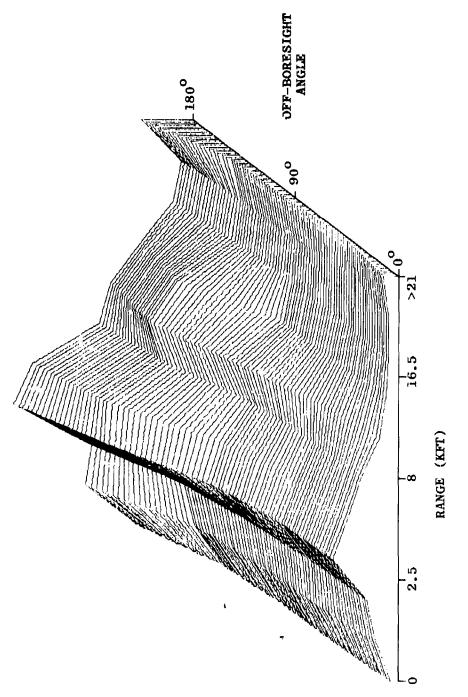
FIG. A-15- TAPE 101 - FIGHTER 2 - ELEVATION ANGLE VERSUS AZIMUTH ANGLE VERSUS FREQUENCY OF OCCURRENCE.

3. Angle off boresight versus range to the target versus frequency of occurrence plots are shown in Fig. A-16 through A-29.

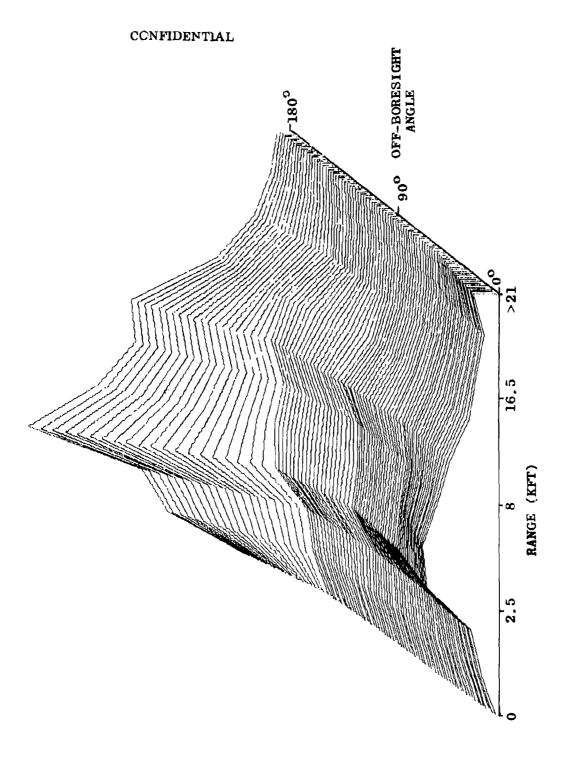


TAPE 1 - FIGHTER 1 - RANGE VERSUS OFF-BORESIGHT ANGLE VERSUS FREQUENCY OF OCCURRENCE. FIG. A-16 -

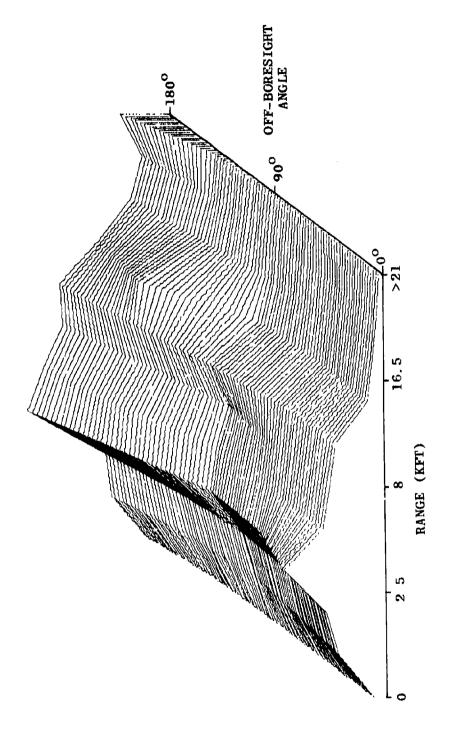




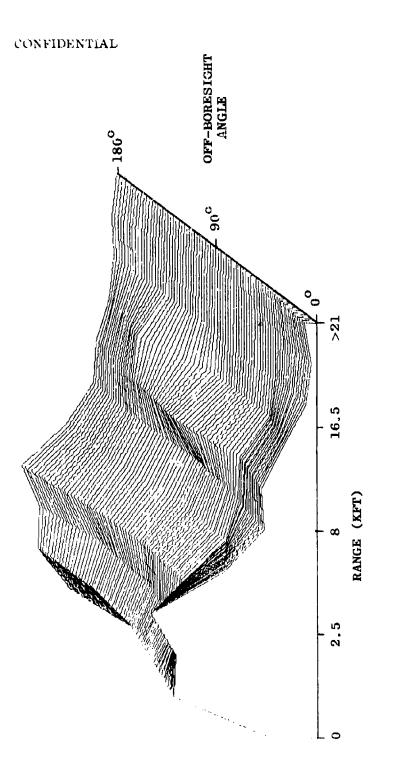
TAPE 1 - FIGHTER 2 - RANGE VERSUS OFF-BORESIGHT ANGLE VERSUS FREQUENCY OF OCCURRENCE. FIG. A-17



TAPE 2 - FIGHTER 1 - RANGE VERSUS OFF-BORESIGHT ANGLE VERSUS FREQUENCY OF OCCURRENCE.



TAPE 2 - FIGHTER 2 - RANGE VERSUS OFF-BORESIGHT ANGLE VERSUS FREQUENCY OF OCCURRENCE.



TAPE 3 - FIGHTER 1 - RANGE VERSUS OFF-BORESIGHT ANGLE VERSUS FREQUENCY OF OCCURRENCE. FIG. A-20-

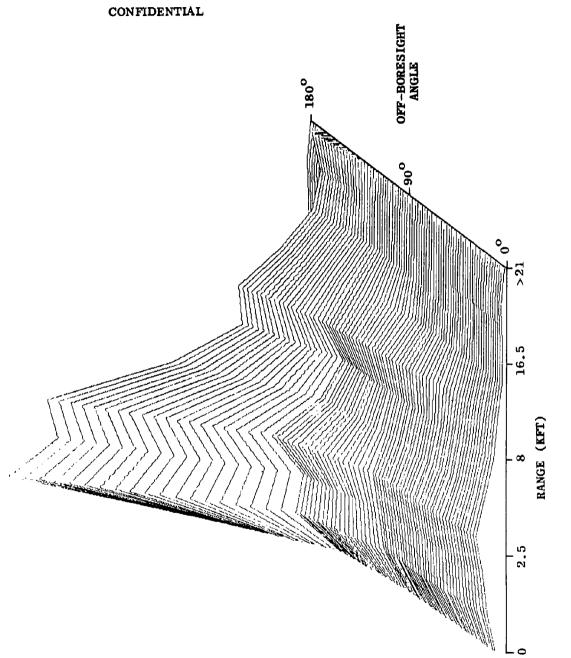


FIG. A-21- TAPE 3 - FIGHTER 2 - RANGE VERSUS OFF-BORESIGHT ANGLE VERSUS FREQUENCY OF OCCURRENCE.

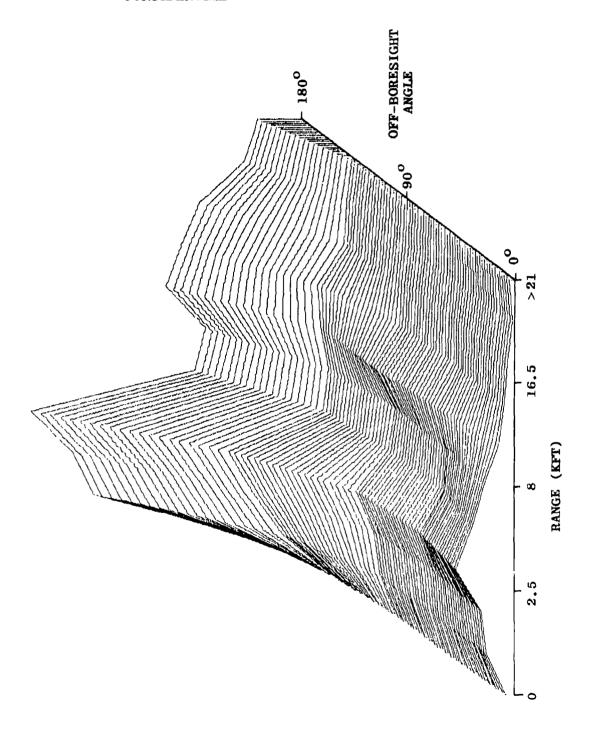
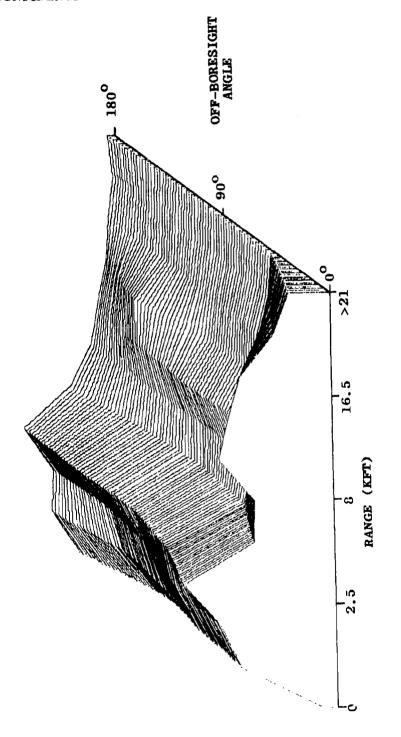
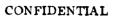
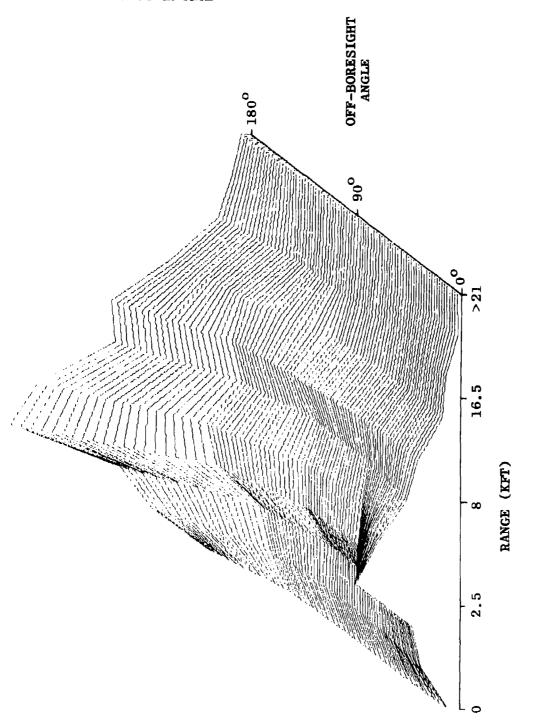


FIG.A-22 - TAPE 4 - FIGHTER 1 - RANGE VERSUS OFF-BORESIGHT ANGLE VERSUS FREQUENCY OF OCCURRENCE.

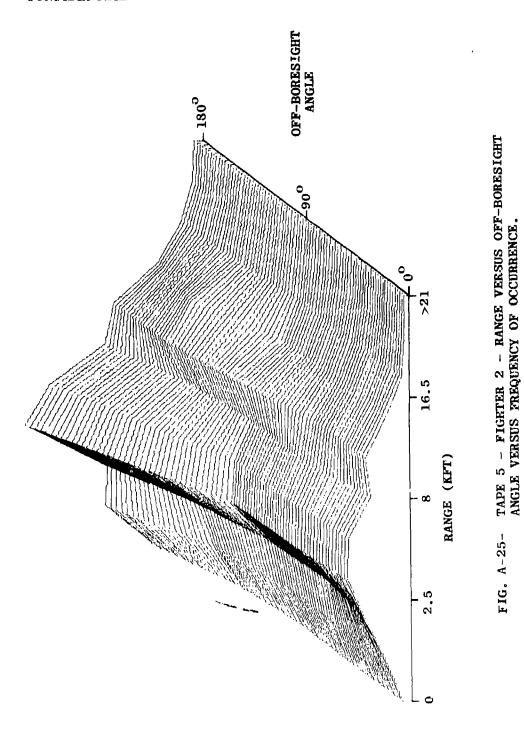


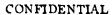
IG. A-23- TAPE 4 - FIGHTER 2 - RANGE VERSUS OFF-BORESIGHT ANGLE VERSUS FREQUENCY OF OCCURRENCE.

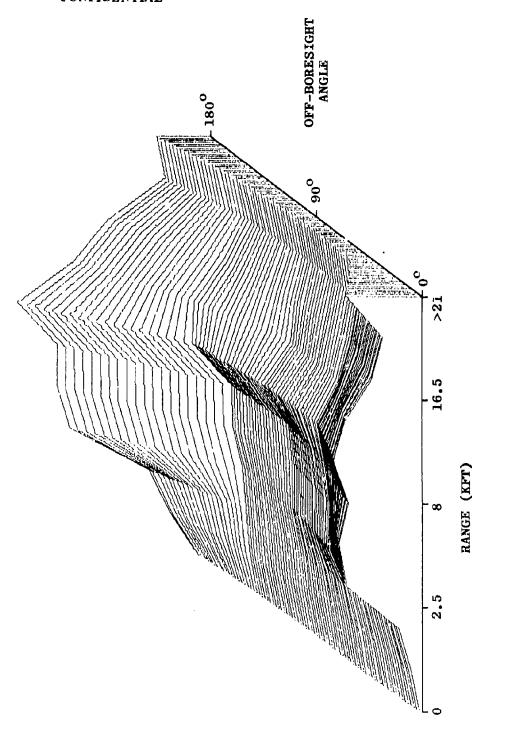




TAPE 5 - FIGHTER 1 - RANGE VERSUS OFF-BORESIGHT ANGLE VERSUS FREQUENCY OF OCCURRENCE. FIG. A-24-







TAPE 6 - FIGHTER 1 - RANGE VERSUS OFF-BORESIGHT ANGLE VERSUS FREQUENCY OF OCCURRENCE. FIG. A-26-

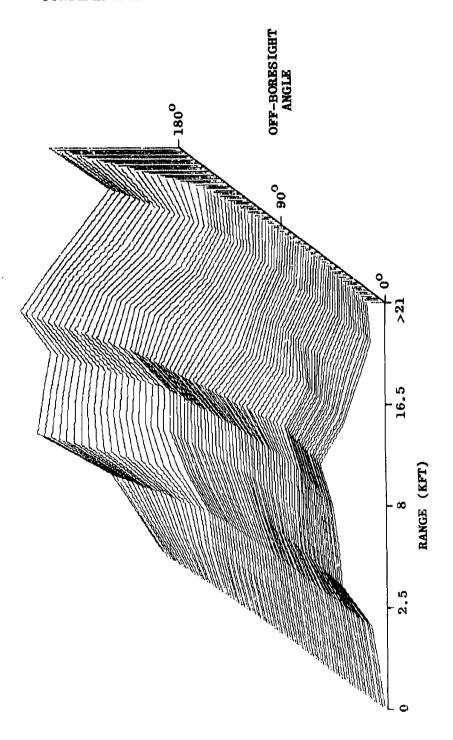


FIG. A-27 - TAPE 6 - FIGHTER 2 - RANGE VERSUS OFF-BORESIGHT ANGLE VERSUS FREQUENCY OF OCCURRENCE.



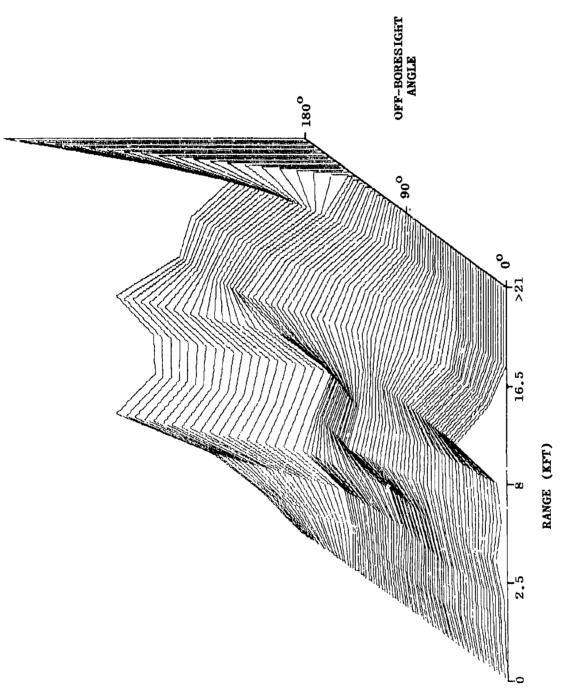
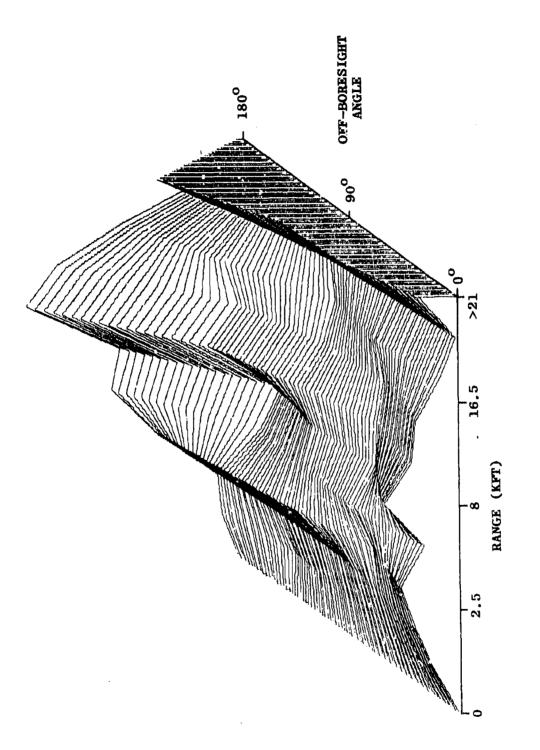


FIG. A-28 - TAPE 101 - FIGHTER 1 - RANGE VERSUS OFF-BORESIGHT ANGLE VERSUS FREQUENCY OF OCCURRENCE.

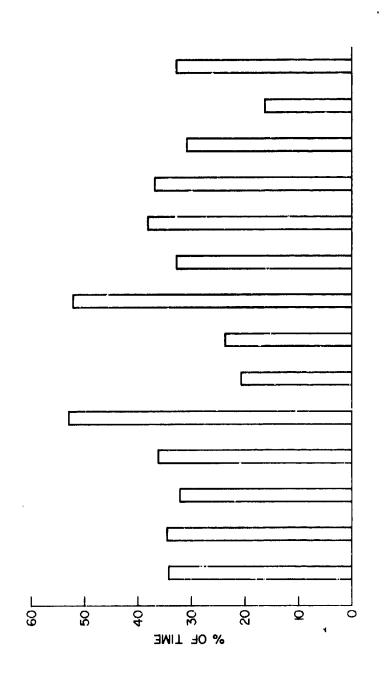


TAPE 101 - FIGHTER 2 - RANGE VERSUS OFF-BORRSIGHT ANGLE VERSUS FREQUENCY OF OCCURRENCE. FIG. A-29

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- 4. Tracking parameters as a function of target position are contained in the tollowing figures:
  - a. Percent of time target is in sector Fig. A-30 thru A-37.
  - b. Range Figs. A-38 through A-45.
  - c. Range rate Figs. A-46 through A-53.
  - d. Range acceleration Figs. A-54 through A-61.
  - e. Azimuth line of sight rate Figs. A-62 through A-69.
  - f. Azimuth line of sight acceleration Figs. A-70 through A-77.
  - g. Elevation line of sight rate Figs. A-78 through A-85.
  - h. Elevation line of sight acceleration Figs. A-86 through A-93.
  - i. Azimuth gimbal rate Figs. A-94 through A-101.
  - j. Azimuth gimbal acceleration Figs. A-102 through A-109.
  - k. Elevation gimbal rate Fig. A-110 through A-117.
  - 1. Elevation gimbal acceleration Figs. A-118 through A-125.

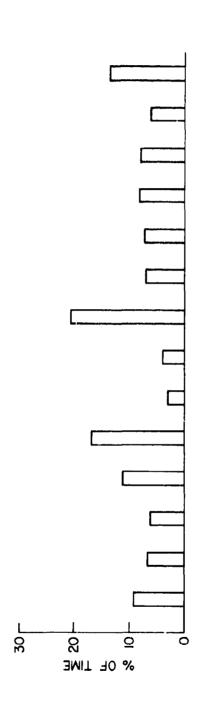
AZIMUTH GIMBAL ANGLE -0° TO ±60° ELEVATION GIMBAL ANGLE - 0° TO +60°



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FIG. A-30- SUMMARY OF GIMBAL ANGLE

AZIMUTH GIMBAL ANGLE - 0° TO ±60º ELEVATION GIMBAL ANGLE - -60º TO 0º

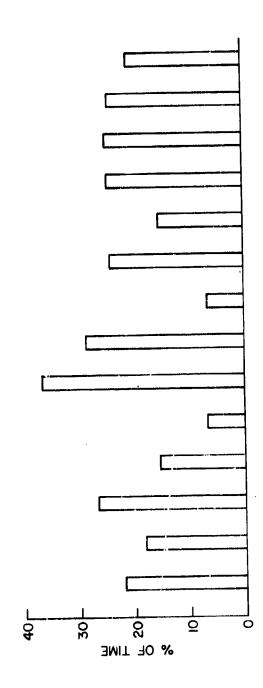


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FIG.A-31 - SUMMARY OF GIMBAL ANGLE

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AZIMUTH GIMBAL ANGLE - ±120° TO ±180° ELEVATION GIMBAL ANGLE - 0° TO +60°

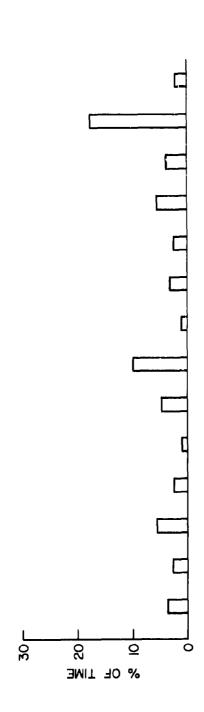


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FIG. A-32 - SUMMARY OF GIMBAL ANGLE

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AZIMUTH GIMBAL ANGLE - ±120° TO ±180° ELEVATION GIMBAL ANGLE - -60° TO 0°



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FIG. A-33 -SUMMARY OF GIMBAL ANGLE

AZIMUTH GIMBAL ANGLE -0° TO ±180° ELEVATION GIMBAL ANGLE - +60° TO +90° P 09 호 5 8 0 8 8 % OF TIME

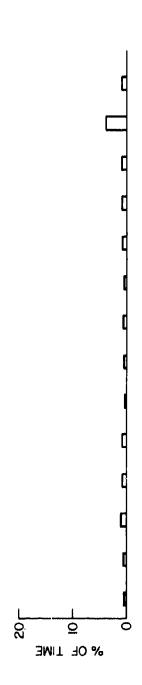
<u>9</u>ш 98 FIG. A-34-SUMMARY OF GIMBAL ANGLE 50 282 40-4 4 0 Mul-N 4-20 20

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AZIMUTH GIMBAL ANGLE - 0° TO ±180° ELEVATION GIMBAL ANGLE - -90° TO -60°



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FIG. A-35 - SUMMARY OF GIMBAL ANGLE

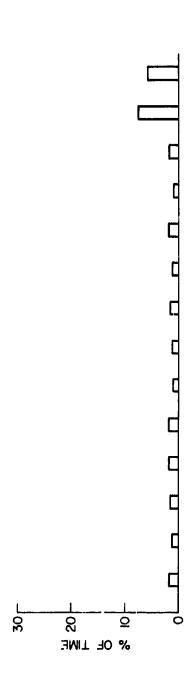
AZIMUTH GIMBAL ANGLE - ±60º TO ±120º ELEVATION GIMBAL ANGLE - 0º TO +60º

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FIG. A-36-SUMMARY OF GIMBAL ANGLE

AZIMUTH GIMBAL ANGLE - ±30° TO ±120° ELEVATION GIMBAL ANGLE - -60° TO 0°



	_	$\equiv$	2	2	6	3	4	4	2	2	9	9	◙	ᅙ
AIRCRAFT (C	S	E	ပ	[Q]	۷	Ш	۷	O	8	ā	18	ū	F	4
NEAPONS [	2	_	-	=	=	=	2		[2]					_

FIG.A-37 - SUMMARY OF GIMBAL ANGLE

CASE NO.	-		-	2	2	3	3	4	4	4	5	5	9	9	ΙΟΙ	ĵO,
AIRCRAFT	Ü	Ī	Ш	U	٥	∢	Ш	<b>4</b>		a	B	a	В	Ε	F	F
WEAPONS	2	<u> </u>	_	_	-	-	~	2		1	2	1	1	1	11	

FIG. A-38 - SUMMARY OF RANGE

FIG. A-39 - SUMMARY OF RANGE

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9	63	
•	3	1
5	O	1
5	8	2
4	D	1
4	٧	2
3	E	
3	٧	
2	٥	1
2	C	+-
	ш	į
-	C	2
ç	FT	S
CASE NO.	RCRAI	APO
CA	A	¥ E

FIG. A-40 - SUMMARY OF RANGE

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A Driver

2.
A ANGLE
H GIMBAL AN ION GIMBAL 95% VALUE MIN & MAX
Oz Z
ELEVATION M PELEVATION M PELEVATION M PELEVATION M PELEVATION M PER PEN
51200 256001 .28001 64001 64001 64001 64001 64001 64001 64001

CASE NO.	1	-	2	 2	3	3	4		4	5	2	9	Ů,	9	δ	
AIRCRAFT	U	Ш	U	a	٧	Ш	∢		۵	æ	 a	8		E	ц	
WEAPONS	2	-	-	-	-	1	2	_	1	2	-	-	Ì	_	1	

FIG. A-41 - SUMMARY OF RANGE

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+	ر ر	1	<b>」</b> ←	- اد	2 -	۲ -	٠	K (7)	2 -	2 2	2 -	n	<u> </u>	L e

FIG. A-42 - SUMMARY OF RANGE

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ELEVATION GIMBAL ANGLE AZIMUTH GIMBAL ANGLE MAX

CASE NO.	1	[4]	2	2	3		3	4	_	4	2	5	9	9	Q	
AIRCRAFT	U	ш	υ	O	∢	_	E	4	٥	10	В	D	8	3	F	
WEAPONS	2	-	1	1	ŀ	Ì	1	2	_		2	1	1	1	1	

FIG. 4-43 - SUMMARY OF RANGE

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RANGE (R) 1600

25600

12800

6400

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	9 0 B C	4
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16. A-44 - SUMMARY OF RANGE

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Ø ₹ >	
AZIMUTH GIMBAL ELEVATION GIMBA MIN 8 MA MIN 8 MA	
AZIMU ELEVA	
51200   25600	RANGE (R) (FT) 200 100 100 100 100 100 100 100 100 100

0 9 9 5	D B E F	1 1 1
5	В	2
4	a	1
4	٧	2
3	E	1
9	4	1
2	٥	1
2	Ü	•
1	Е	1
Ξ	C	2
CASE NO.	AIRCRAFT	WEAPONS

FIG. 4-45 - SUMMARY OF RANGE

**₽ r** ğμ ωw •09• 9 8 --ANGLE AZIMUTH GIMBAL ANGLE ELEVATION GIMBAL MAX 4 RANGE RATE (R) (FT/SEC) -400 900 -1600 -3200 3200 1600 900

RATE RANGE OF SUMMARY

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AIRCRAFT C CASE NO.

WEAPONS

32001

1600

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RANGE RATE (A) (FT/SEC)

RATE RANGE OF SUMMARY FIG

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2 8 2

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N 0 +-

70-

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AIRCRAFT WEAPONS

CASE NO.

-3200L

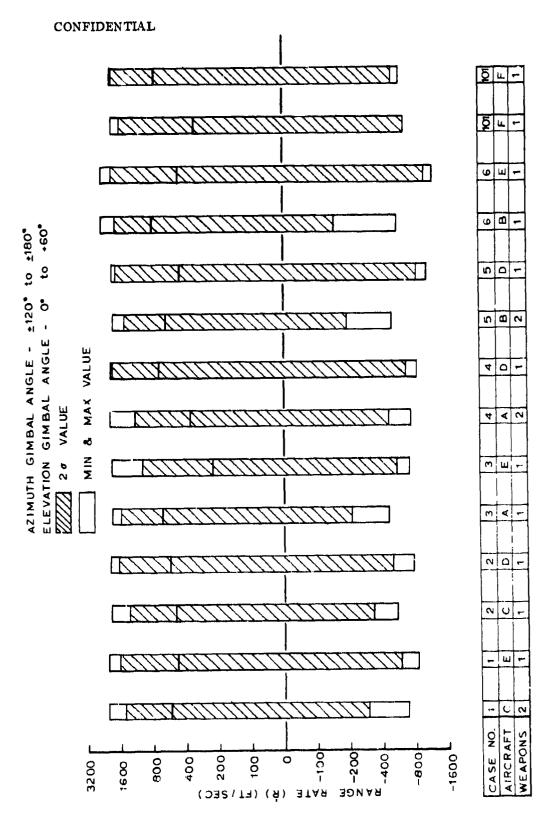
-1600

-800

-400

-200

-100



A-63

1000 mm 1000 mm

±180°

±120°

AZIMUTH GIMBAL ANGLE

FIG. A-49 - SUMMARY OF RANGE RATE

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E H

m **∢** -

N U -

7

CASE NO

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-3200

-800

-1600

400

RANGE RATE (R) (FT/SEC)

400

900

1600

3200

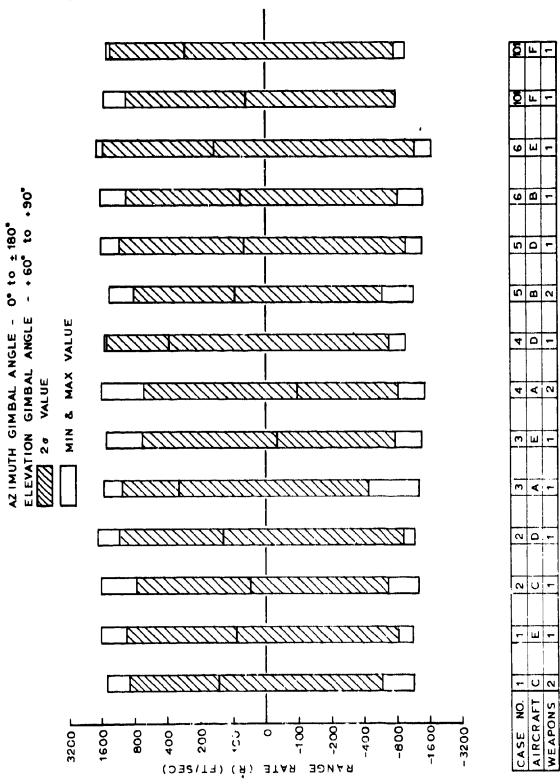


FIG. A-50 - SUMMARY OF RANGE RATE

iOI F o w -9 B -5 0 2 8 2 4 0 -4 4 0 m < -20-4 U F - W F 0 4 CASE NO.
AIRCRAFT
WEAPONS

RANGE

SF OF

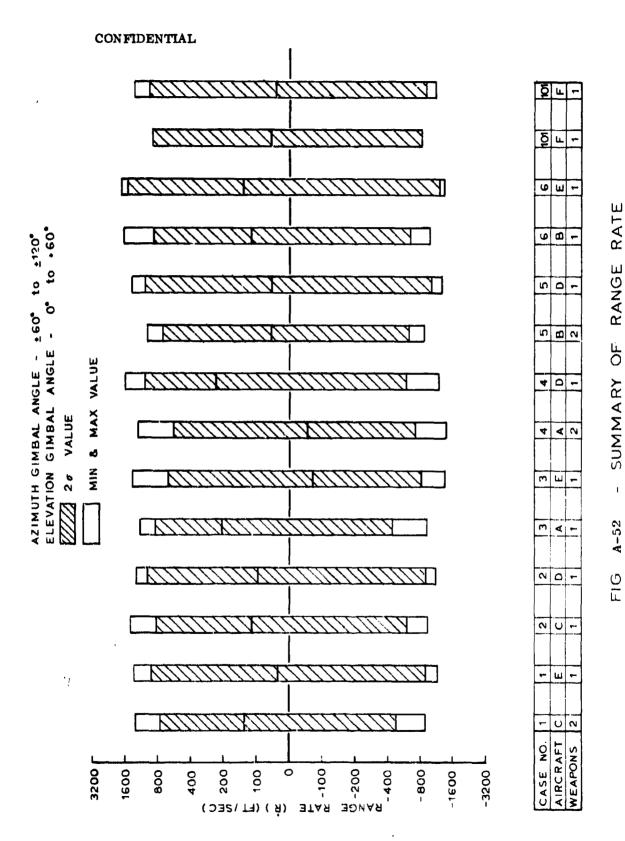
SUMMARY

A-51

FIG.

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RANGE RATE (A) (FT/SEC)



MARINE TO THE POPULATION OF THE PARTY OF THE

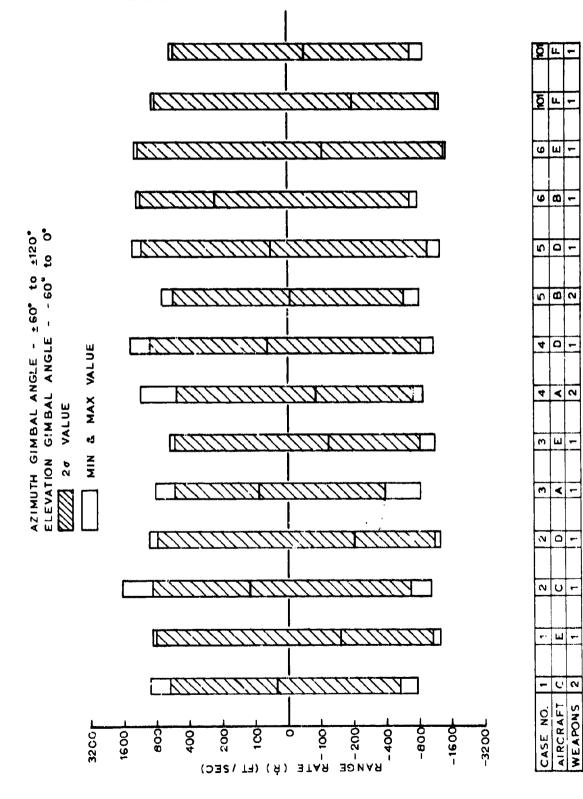


FIG. A-53 - SUMMARY OF RANGE RATE

A-68

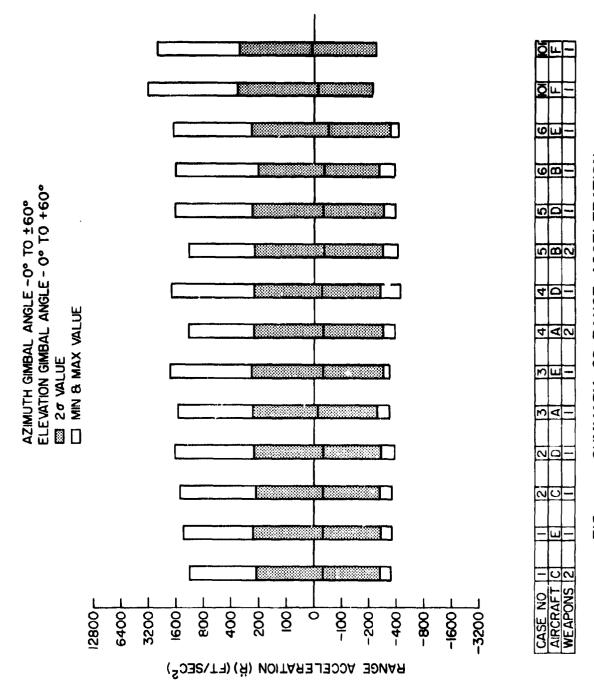


FIG. A-54-SUMMARY OF RANGE ACCELERATION

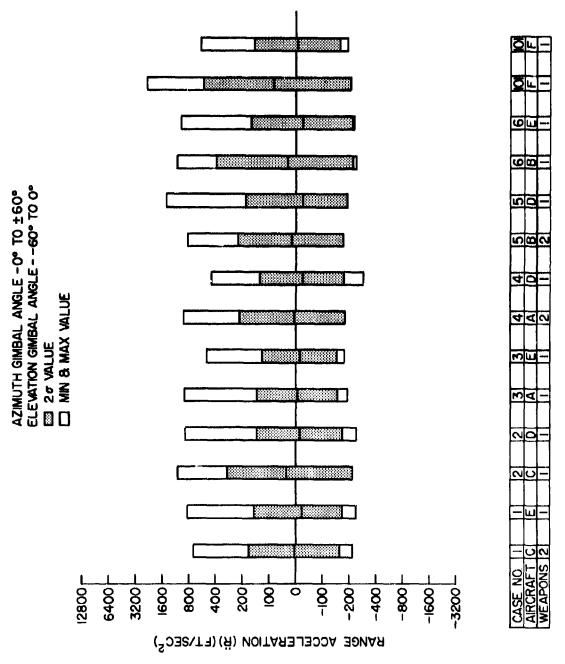


FIG. 4-55-SUMMARY OF RANGE ACCELERATION

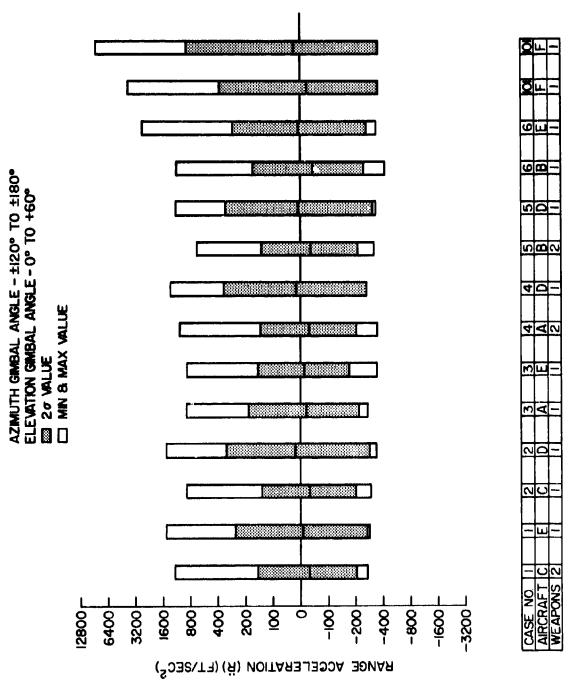


FIG. A-56-SUMMARY OF RANGE ACCELERATION

A-7i

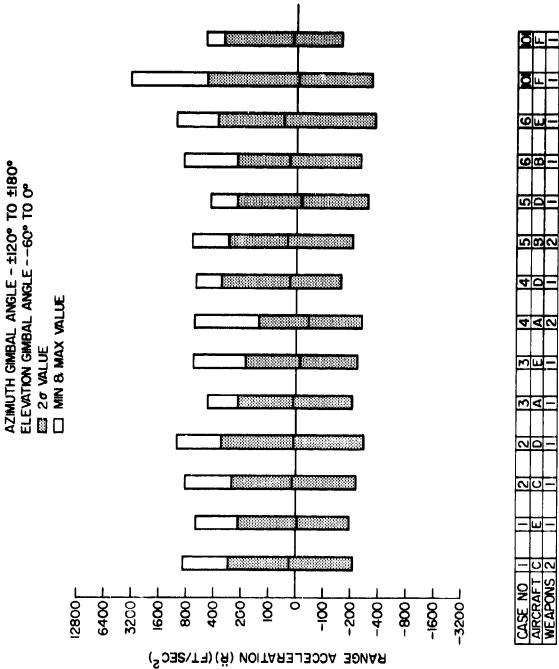


FIG. A-57-SUMMARY OF RANGE ACCELERATION

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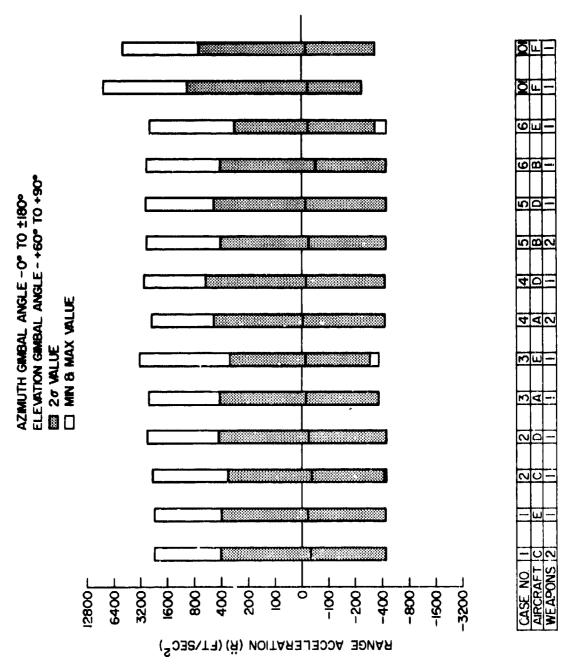


FIG. A-58-SUMMARY OF RANGE ACCELERATION

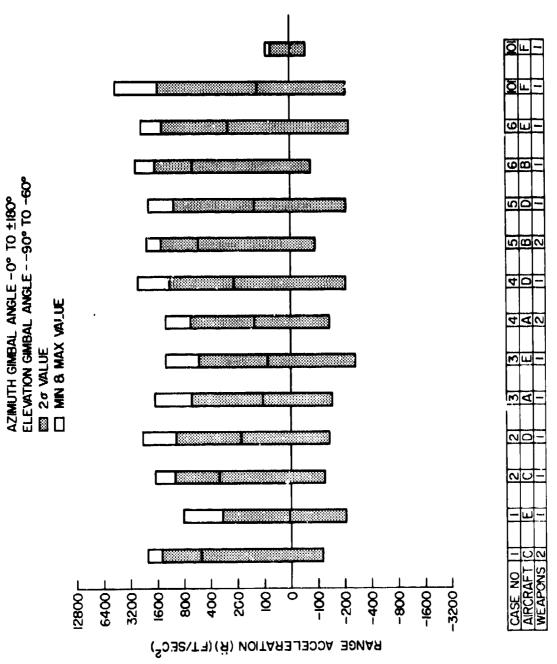


FIG. A-59-SUMMARY OF RANGE ACCELERATION

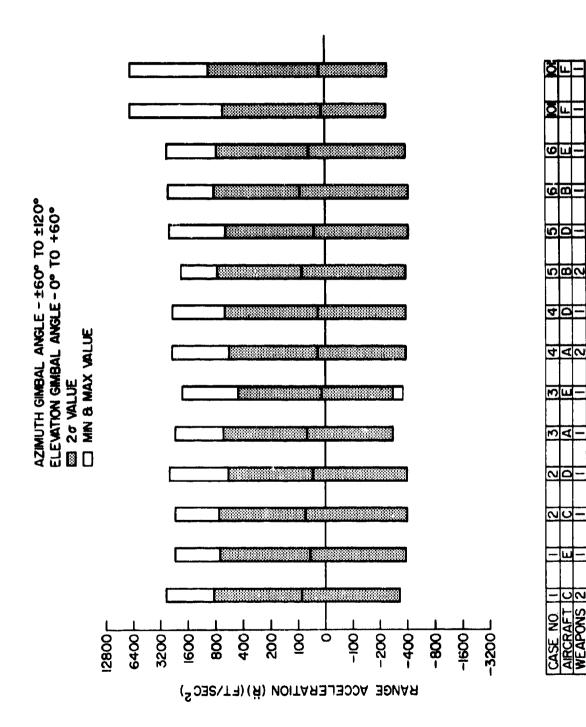


FIG. A-60-SUMMARY OF RANGE ACCELERATION

ш

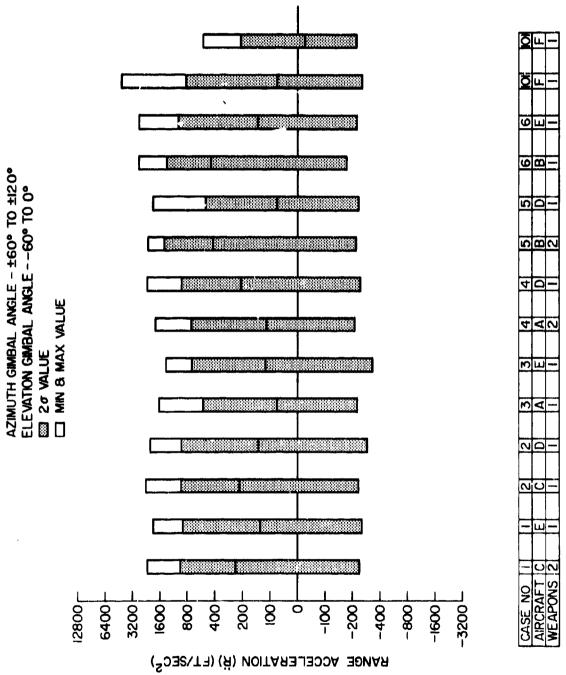


FIG. A-61-SUMMARY OF RANGE ACCELERATION

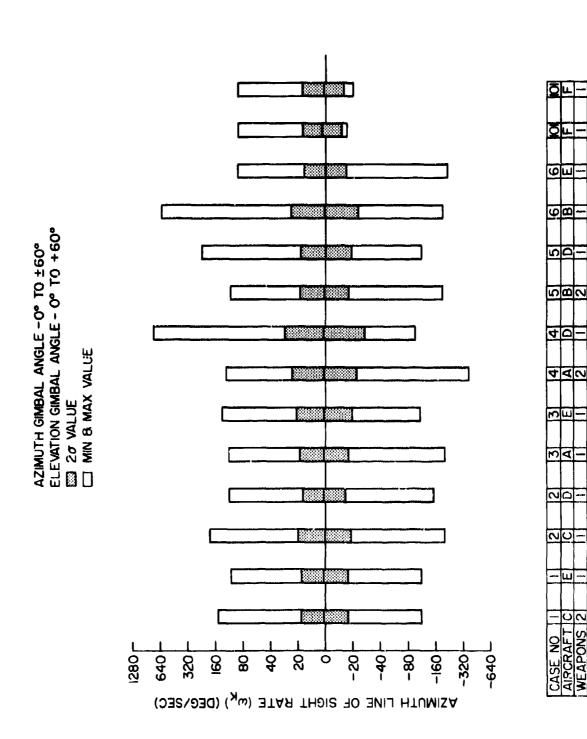


FIG. A-62-SUMMARY OF AZIMUTH LINE OF SIGHT RATE

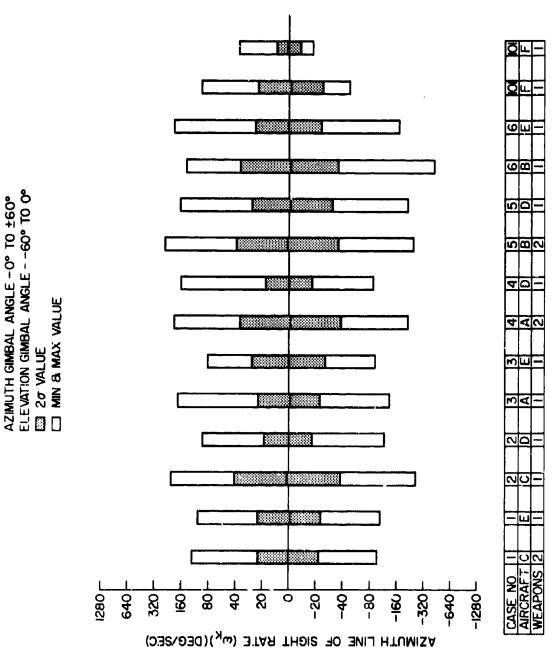


FIG. A-63-SUMMARY OF AZIMUTH LINE OF SIGHT RATE

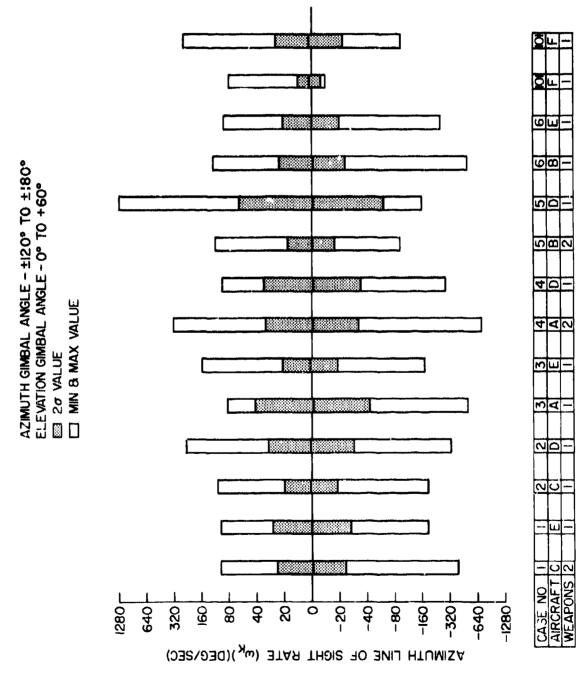


FIG. A-64-SUMMARY OF AZIMUTH LINE OF SIGHT RATE

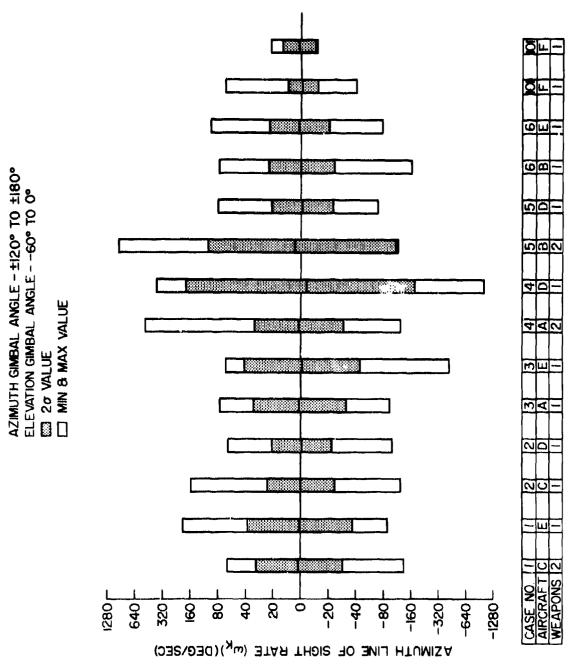
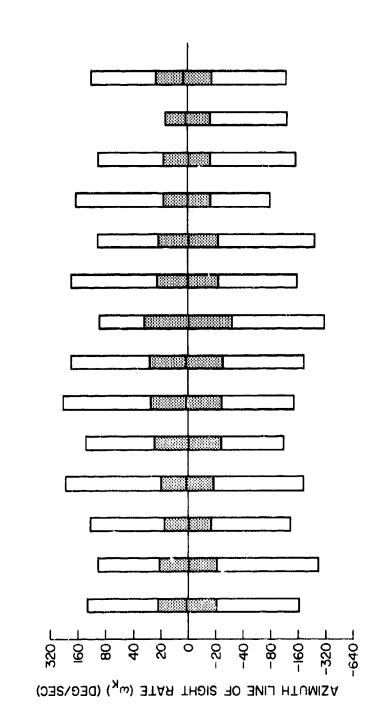


FIG. A-65-SUMMARY OF AZIMUTH LINE OF SIGHT RATE

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AZIMUTH GIMBAL ANGLE -0° TO ±180° ELEVATION GIMBAL ANGLE - +60° TO +90° E 20 VALUE □ MIN 8 MAX VALUE



OF SIGHT RATE <u>6</u> 98-S 0 -282 FIC. A-63-SUMMARY OF AZIMUTH LINE 40 4 A S ЮШ-3 A 2 20 ш CASE NO 1

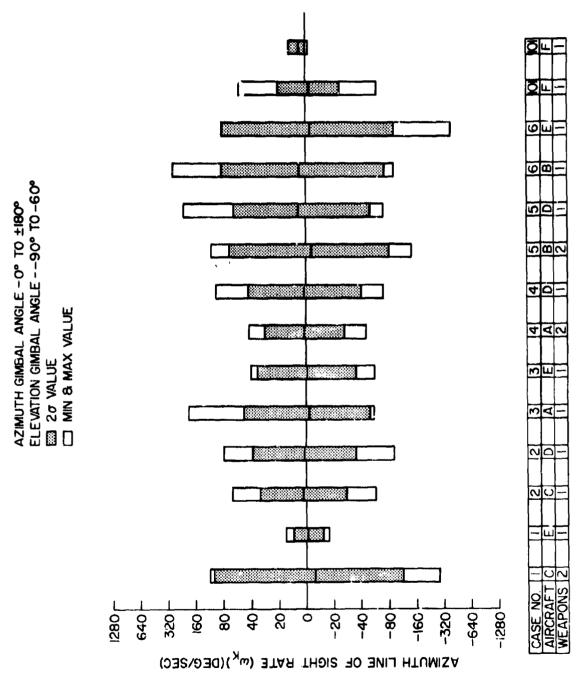


FIG. A-67-SUMMARY OF AZIMUTH LINE OF SIGHT RATE

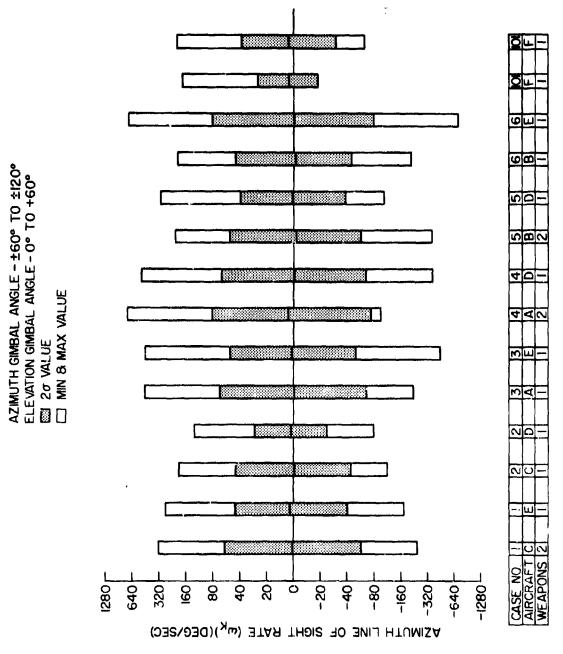


FIG. A-68- SUMMARY OF AZIMUTH LINE OF SIGHT RATE

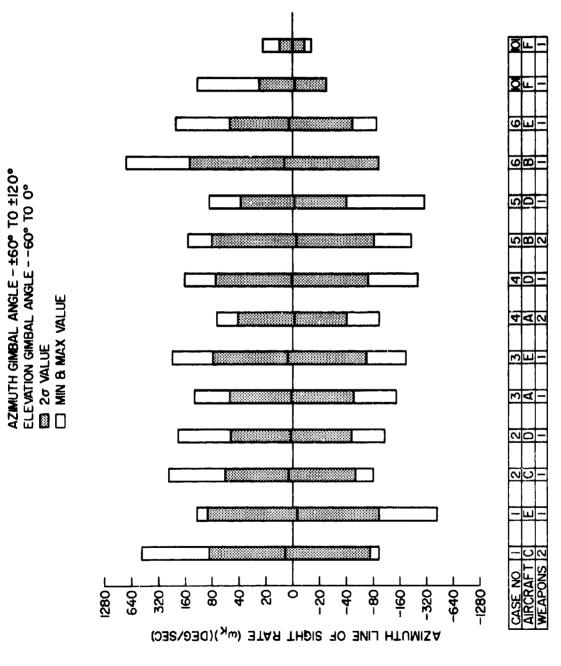
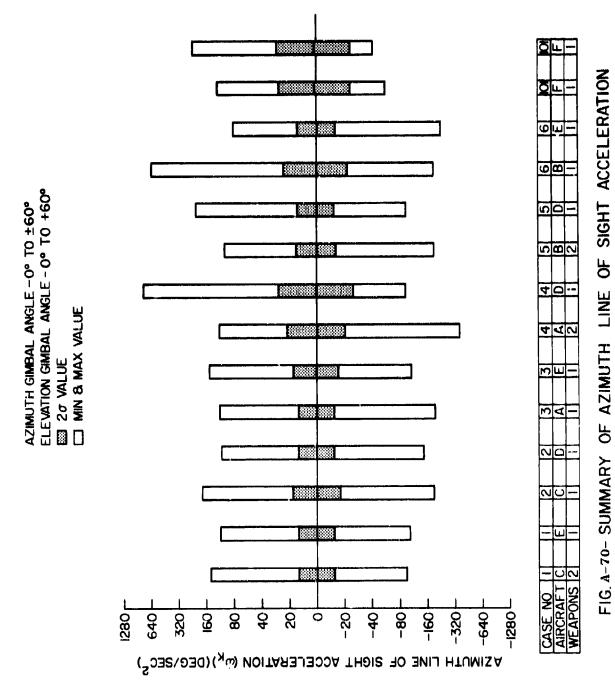


FIG. A-69-SUMMARY OF AZIMUTH LINE OF SIGHT RATE



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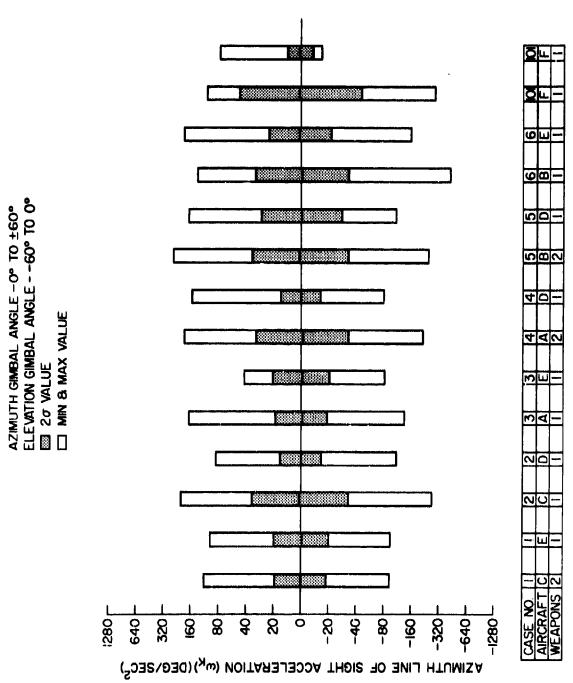
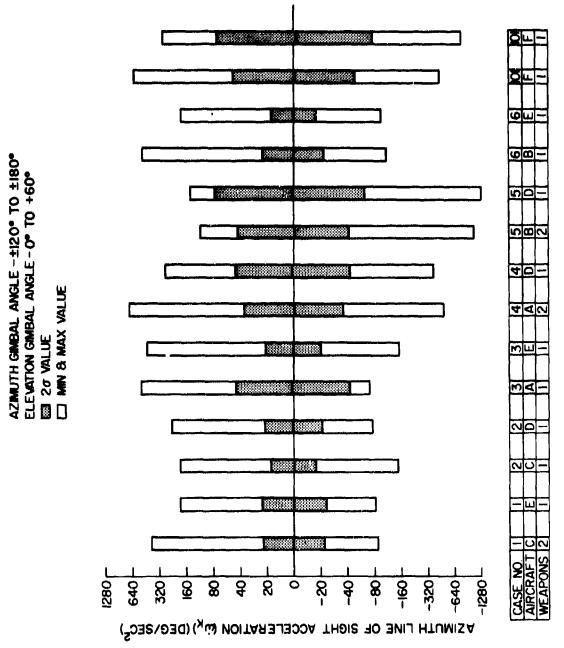
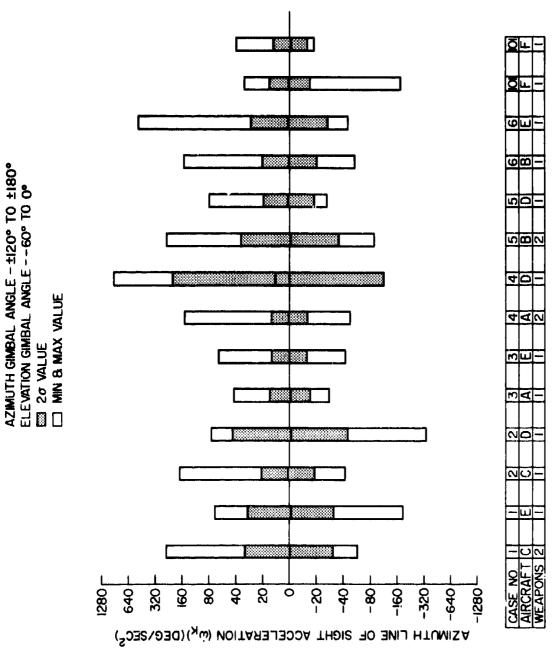


FIG. A-71-SUMMARY OF AZIMUTH LINE OF SIGHT ACCELERATION

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SIGHT ACCELERATION R FIG. A-72- SUMMARY OF AZIMUTH LINE



SIGHT ACCELERATION FIG. A-73-SUMMARY OF AZIMUTH LINE OF

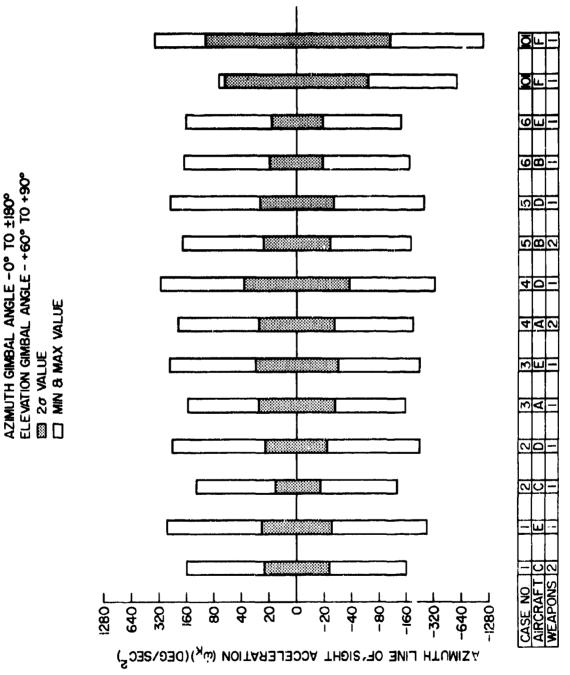
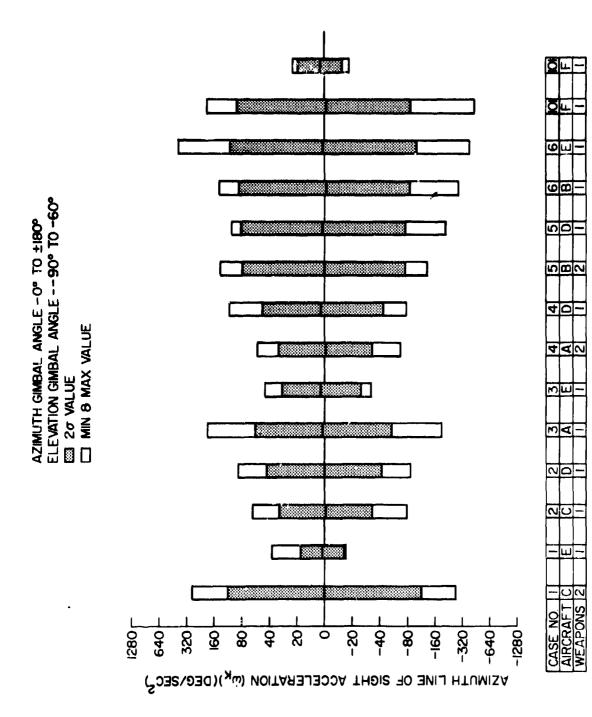


FIG. A-74- SUMMARY OF AZIMUTH LINE OF SIGHT ACCELERATION

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OF SIGHT ACCELERATION FIG. A-75-SUMMARY OF AZIMUTH LINE

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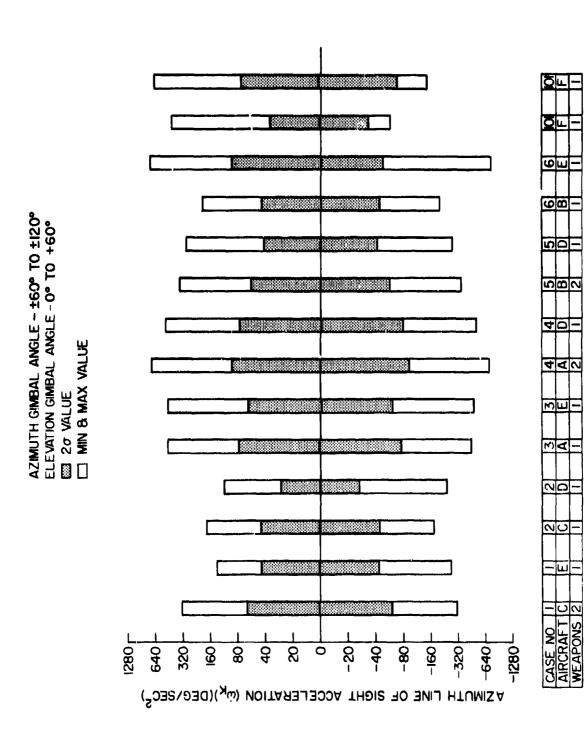


FIG. A-76- SUMMARY OF AZIMUTH LINE OF SIGHT ACCELERATION

Λ**-9**1

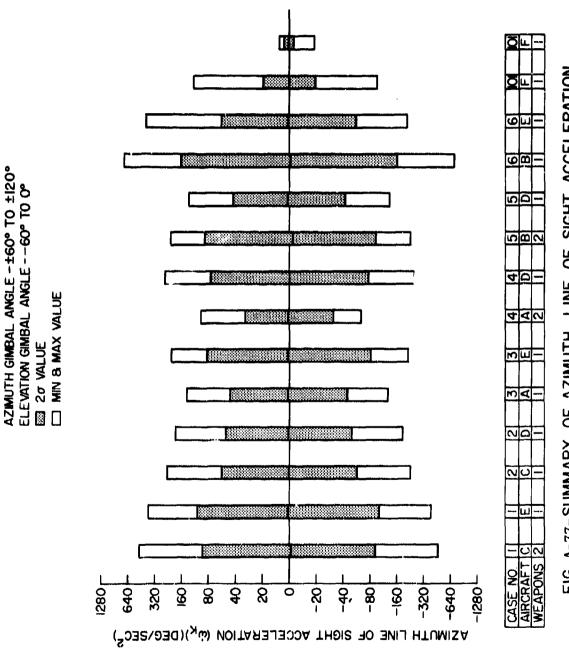


FIG. A-77-SUMMARY OF AZIMUTH LINE OF SIGHT ACCELERATION

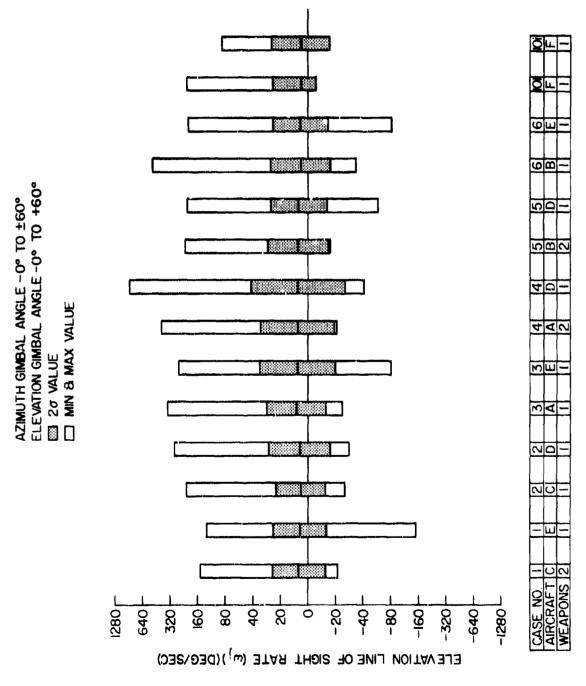


FIG. A-78-SUMMARY OF ELEVATION LINE OF SIGHT RATE

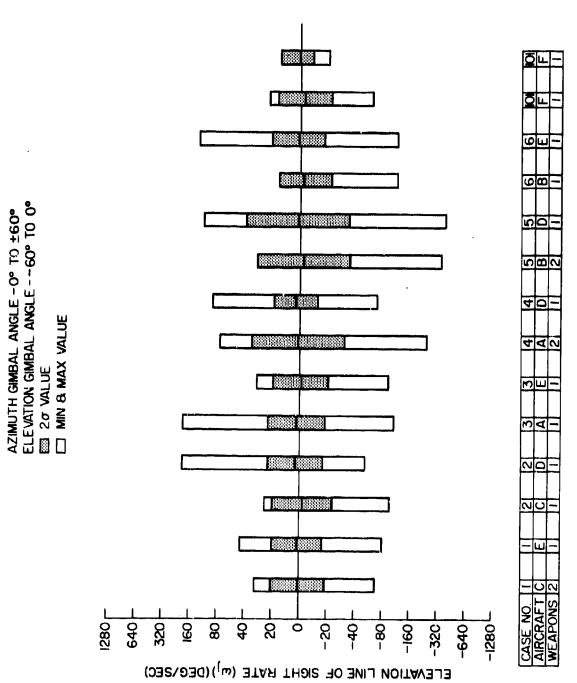


FIG. A-79-SUMMARY OF ELEVATION LINE OF SIGHT RATE

The state of the s

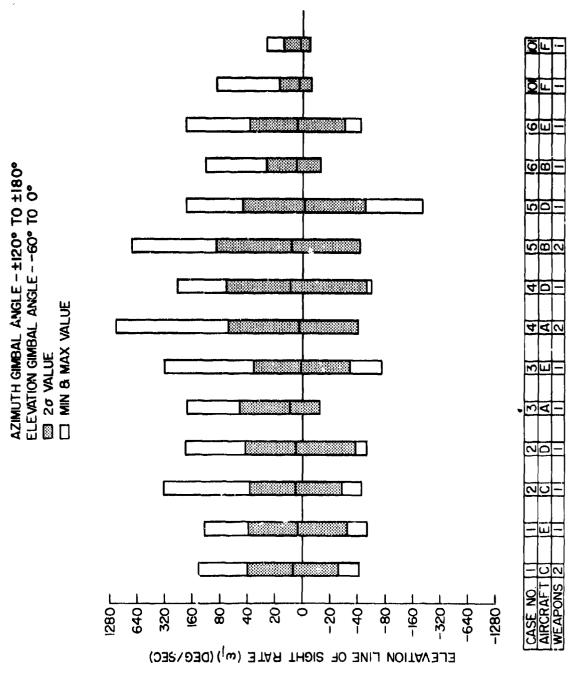


FIG.A-80 - SUMMARY OF ELEVATION LINE OF SIGHT RATE

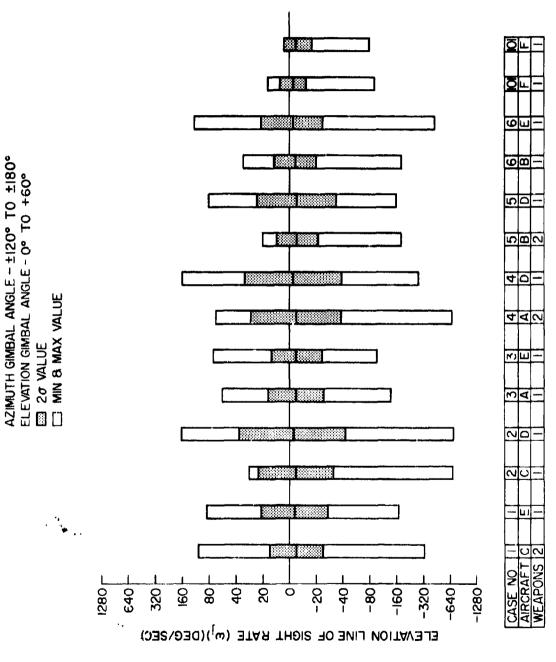


FIG. A-81- SUMMARY OF ELEVATION LINE OF SIGHT RATE

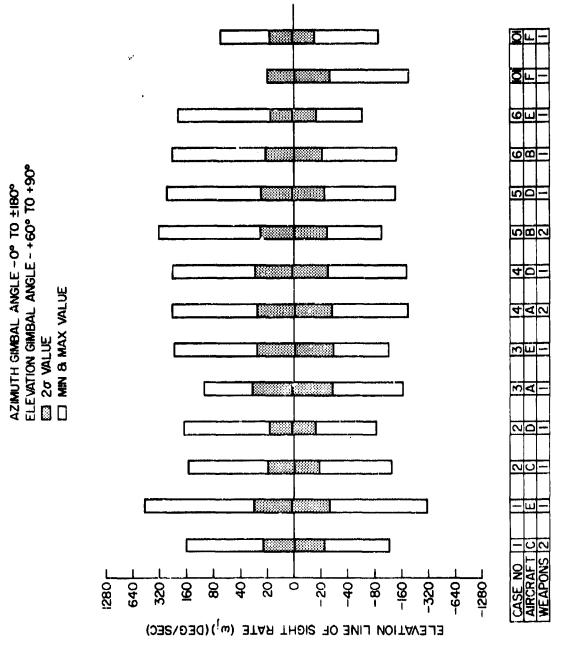


FIG. A-82- SUMMARY OF ELEVATION LINE OF SIGHT RATE

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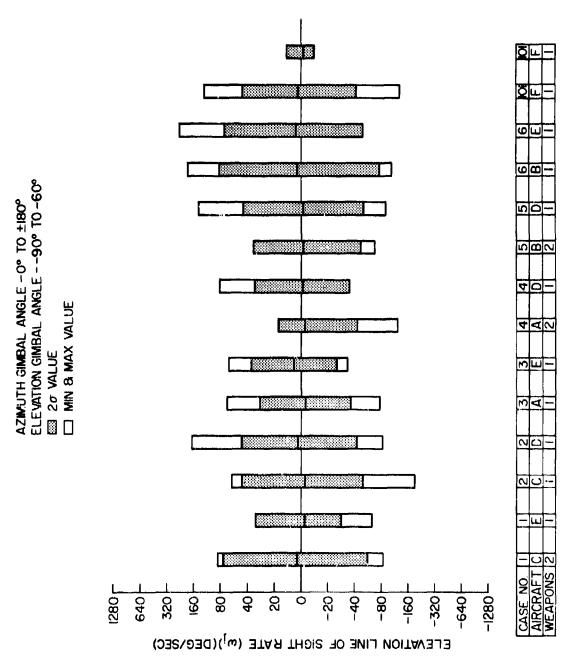


FIG. A-83- SUMMARY OF ELEVATION LINE OF SIGHT RATE

The state of the s

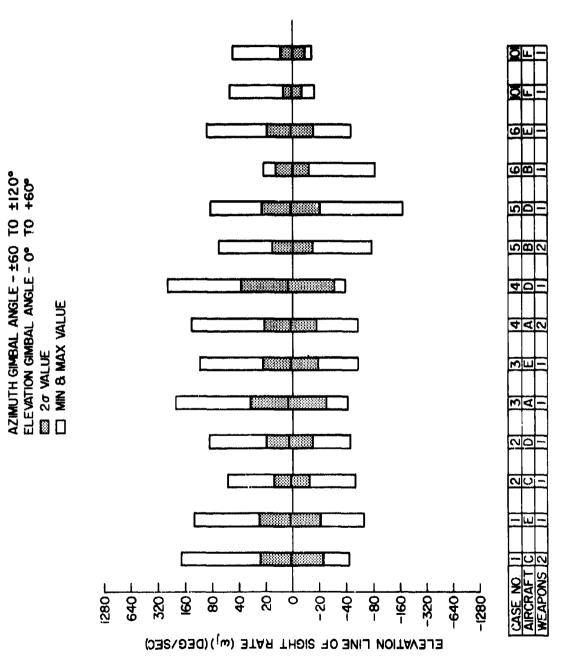


FIG. A-84- SUMMARY OF ELEVATION LINE OF SIGHT RATE

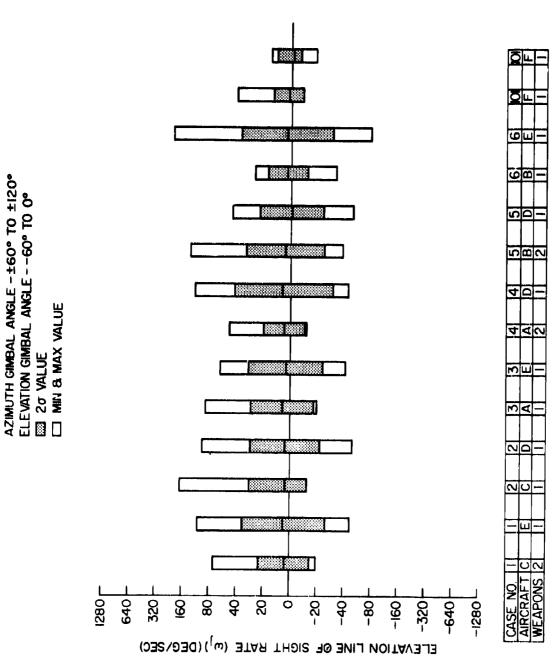
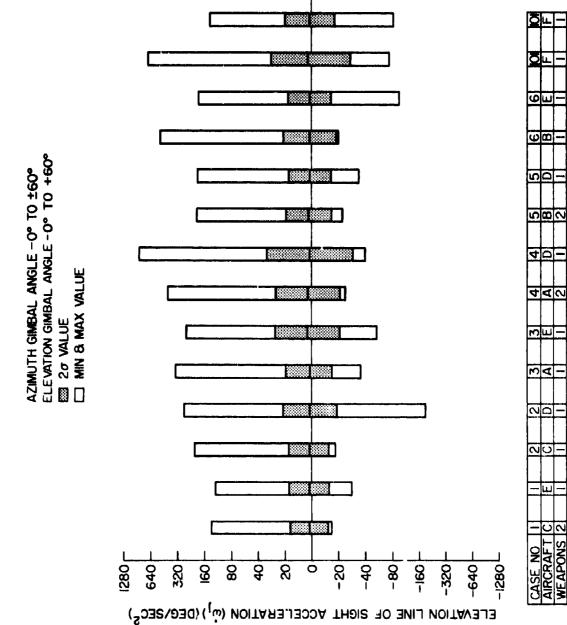


FIG. A-85- SUMMARY OF ELEVATION LINE OF SIGHT RATE



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さんしょう こうべいしょう

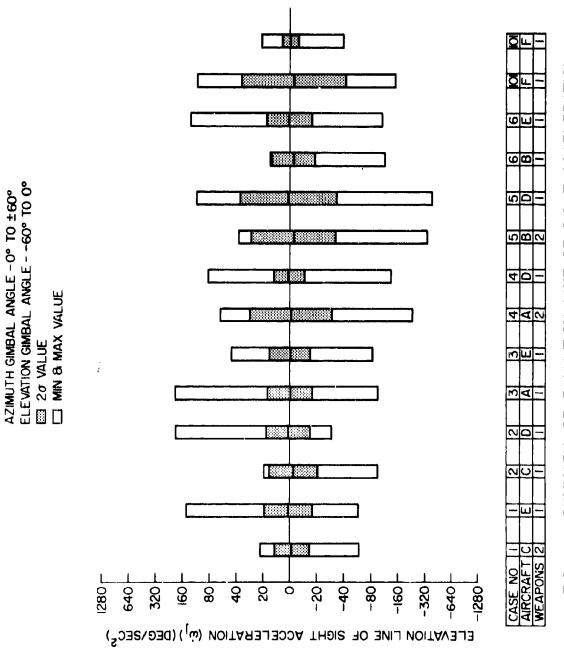
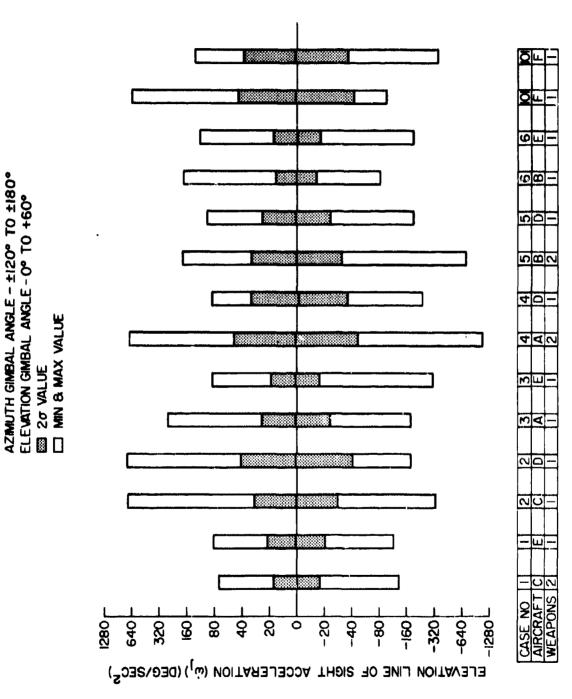
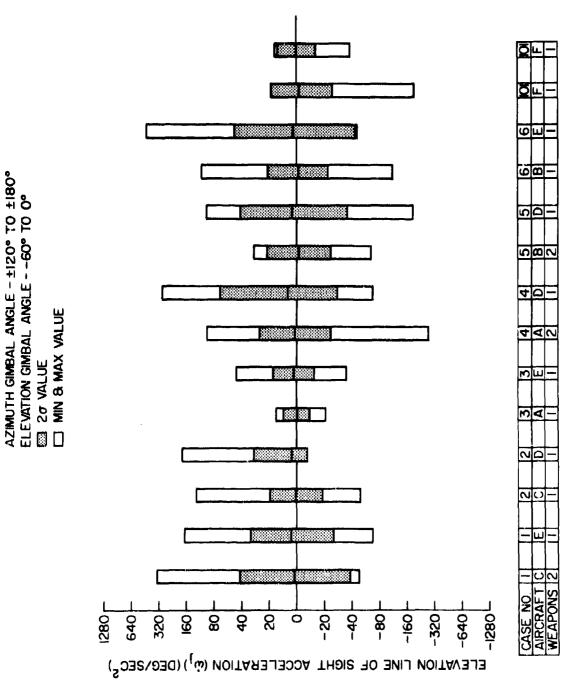


FIG. A-87- SUMMARY OF ELEVATION LINE OF SIGHT ACCELERATION



ELEVATION LINE OF SIGHT ACCELERATION FIG. A-88- SUMMARY OF



ELEVATION LINE OF SIGHT ACCELERATION FIG. A-89 -SUMMARY OF

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一個なることでは、これにあるとしてはなるとのできる。

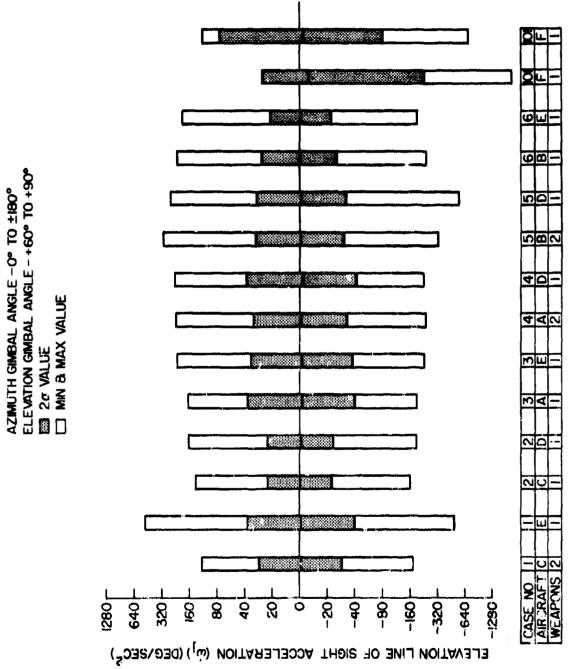


FIG. A-90 - SUMMARY OF ELEVATION LINE OF SIGHT ACCELERATION

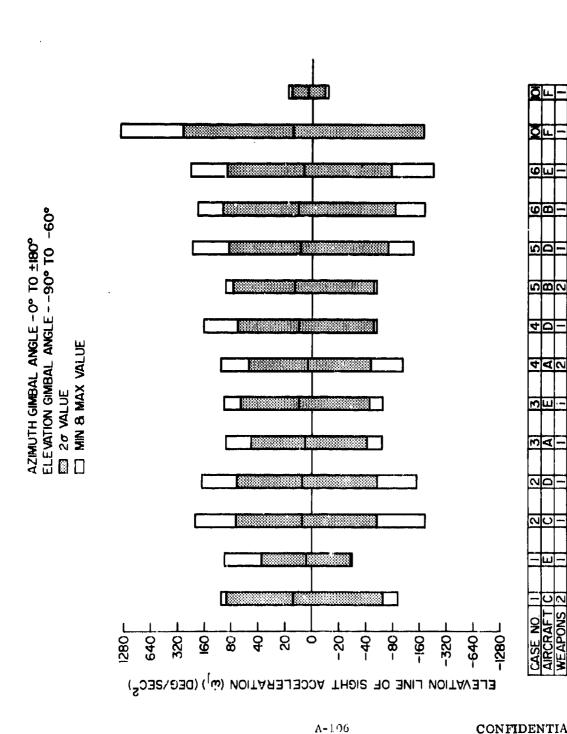
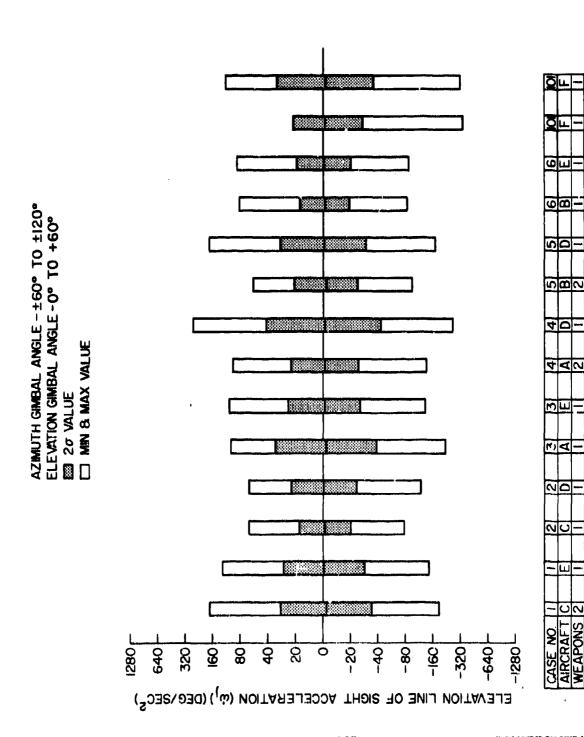


FIG. A-91-SUMMARY OF ELEVATION LINE OF SIGHT ACCELERATION

THE PROPERTY OF THE PARTY OF TH



ELEVATION LINE OF SIGHT ACCELERATION FIG. A-92- SUMMARY OF

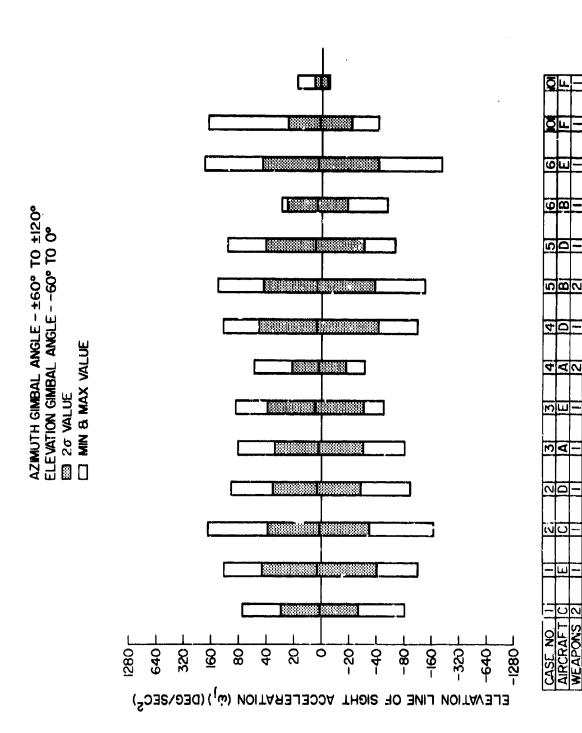


FIG. A-93- SUMMARY OF ELEVATION LINE OF SIGHT ACCELERATION

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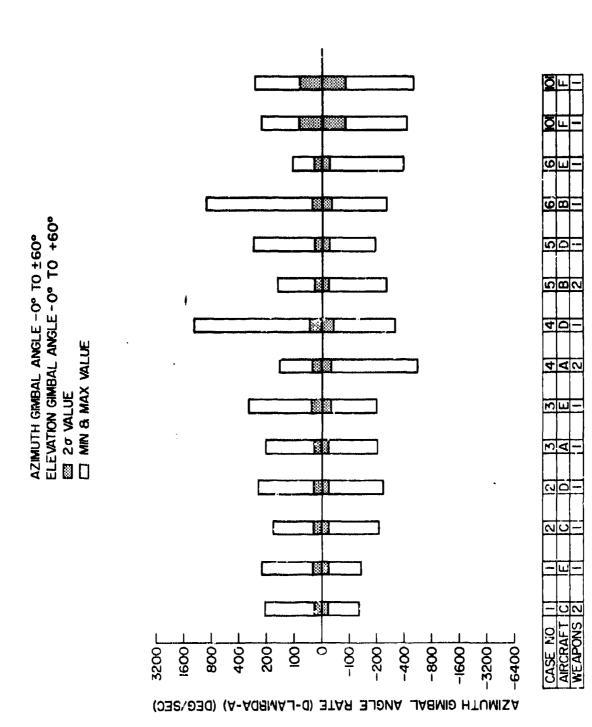


FIG. A-94- SUMMARY OF AZIMUTH GIMBAL ANGLE RATE

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province the province of

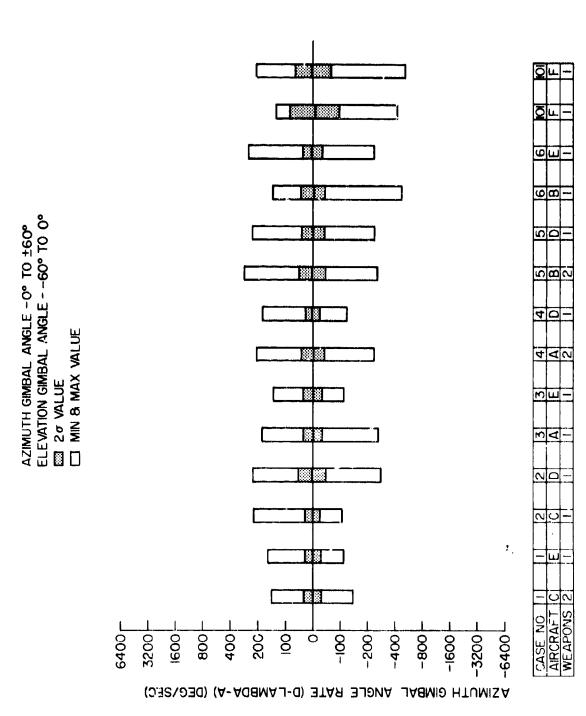


FIG. A-95-SUMMARY OF AZIMUTH GIMBAL ANGLE RATE

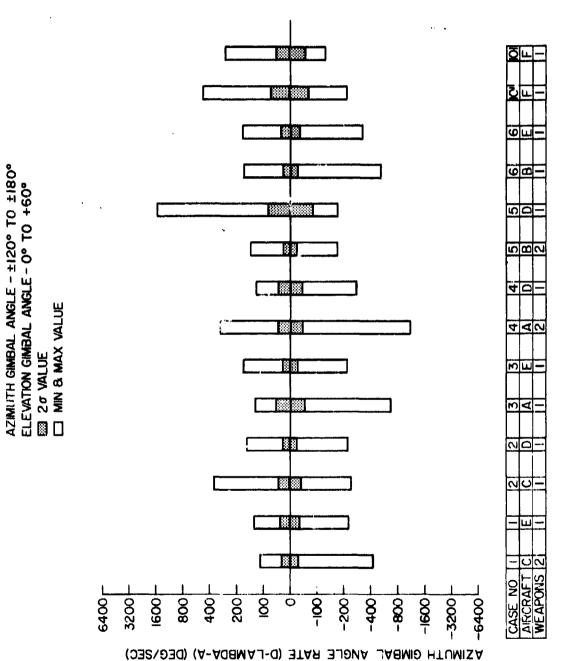


FIG. A-96-SUMMARY OF AZIMUTH GIMBAL ANGLE RATE

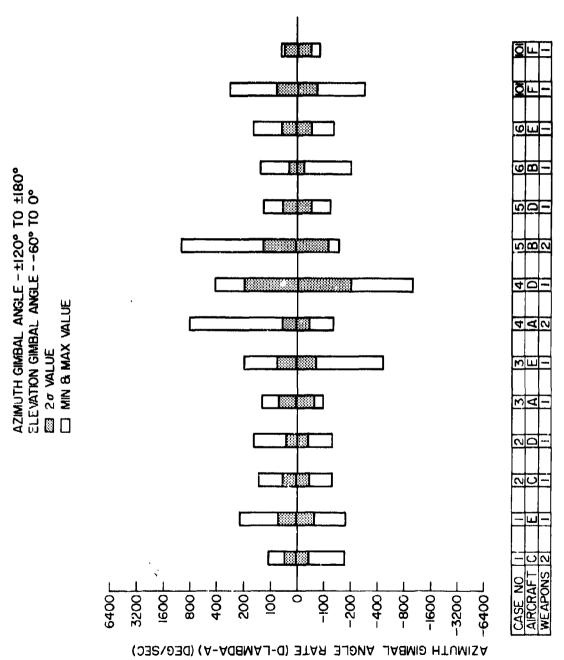


FIG. A-97- SUMMARY OF AZIMUTH GIMBAL ANGLE RATE

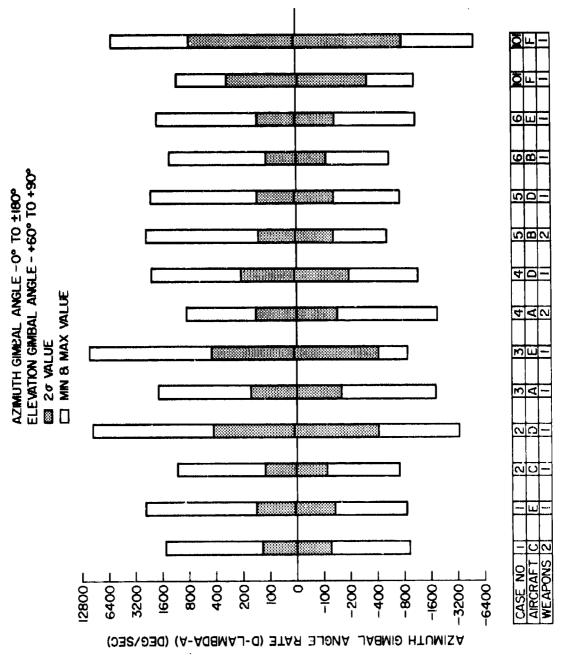


FIG. A-98-SUMMARY OF AZIMUTH GIMBAL ANGLE RATE

AZIMUTH GIMBAL ANGLE RATE (D-LAMBDA-A) (DEG/SEC)

9 98 ELEVATION GIMBAL ANGLE - -90° TO -60° AZIMUTH GIMBAL ANGLE -0° TO ±180° 5 **2007** XEE 870 E 200 PER BERE 200 STEAR FFE STEAR STEAR FE STEAR 40 ■ 2σ VALUE ■ MIN 8 MAX VALUE 4 **4 0** \$\$10\$\$00\$ \$10\$\$\$\$\$\$ E 3 S 4 -20 70-CASE NO 1 AIRCRAFT C WEAPONS 2 2007 -3200 -6400<sup>[</sup> 3200g 88 400 8 --200 -400 009 8 -800 <del>-1600</del>

FIG. A-99- SUMMARY OF AZIMUTH GIMBAL ANGLE RATE

AZIMUTH GIMBAL ANGLE RATE (D-LAMBDA-A) (DEG/SEC)

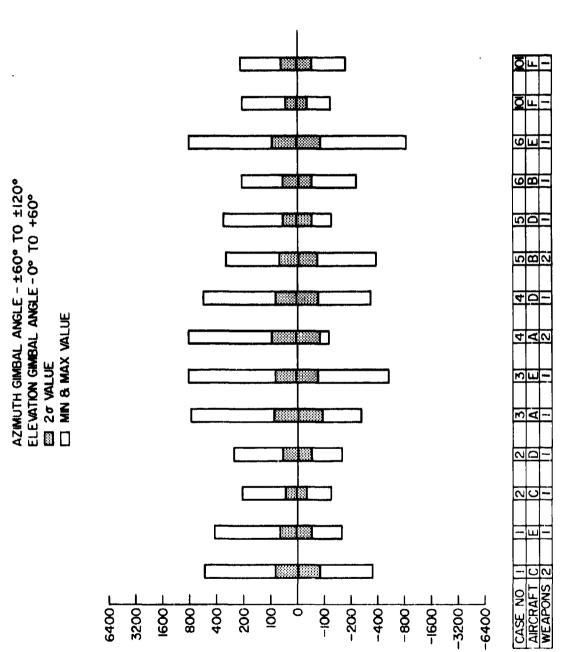


FIG.A-100-SUMMARY OF AZIMUTH GIMBAL ANGLE RATE

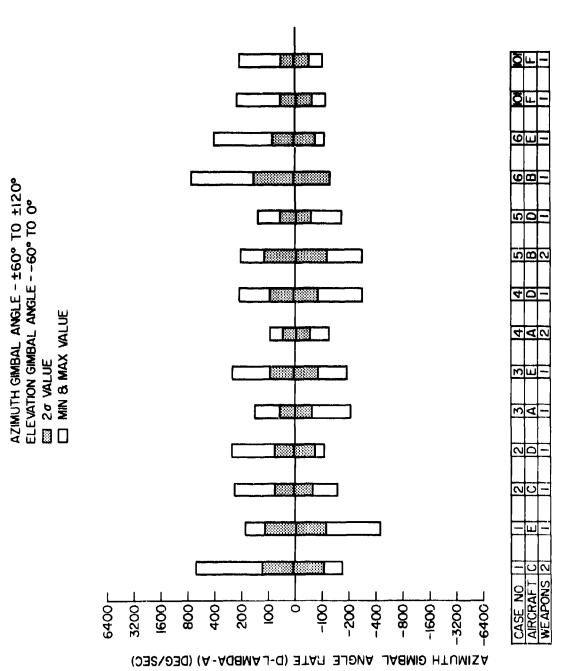
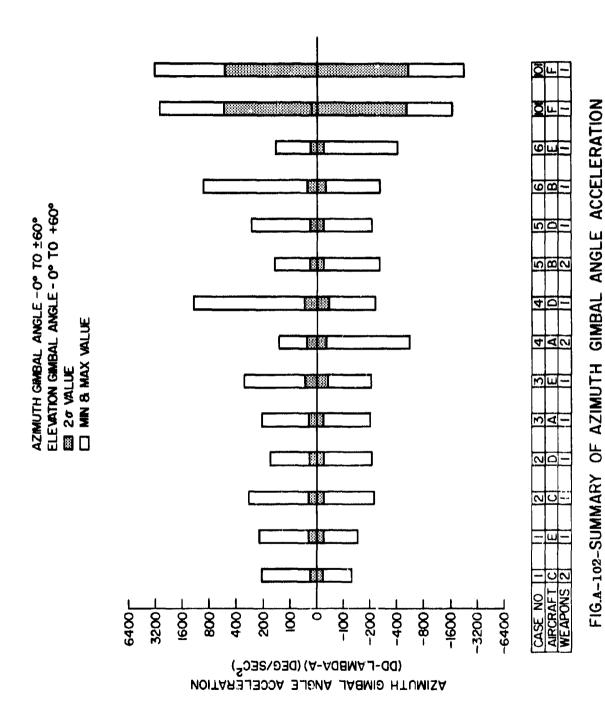


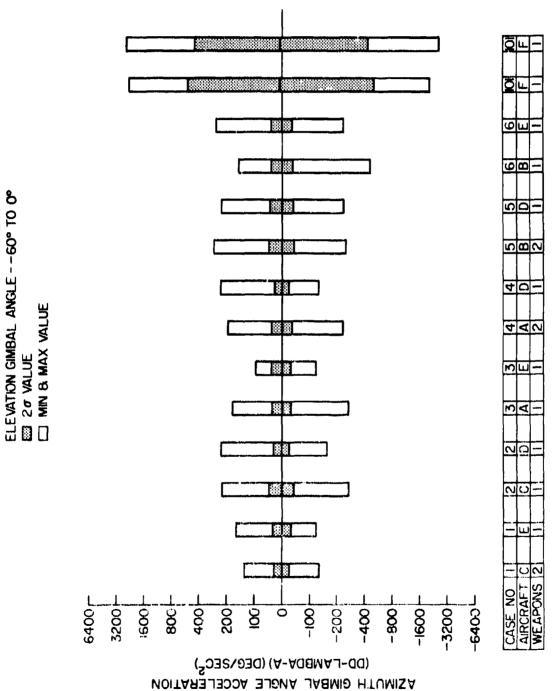
FIG.A-101-SUMMARY OF AZIMUTH GIMBAL ANGLE RATE



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AZIMUTH GIMBAL ANGLE -0° TO ±60°

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FIG.A-103-SUMMARY OF AZIMUTH GIMBAL ANGLE ACCELERATION

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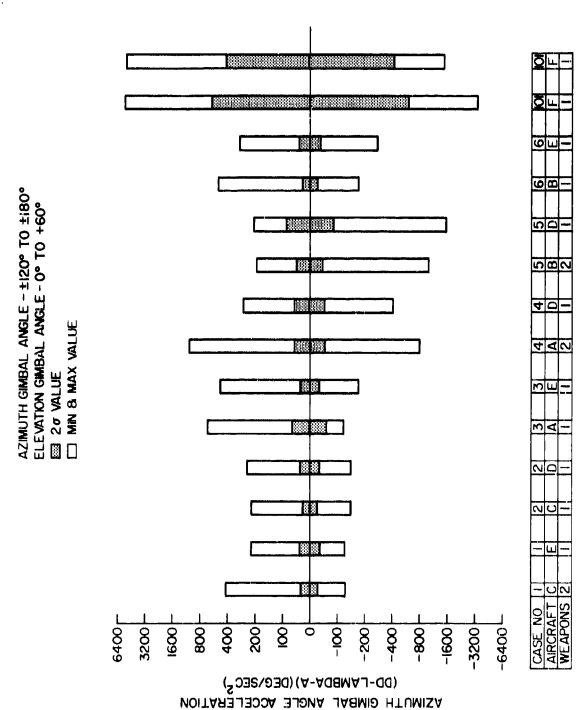
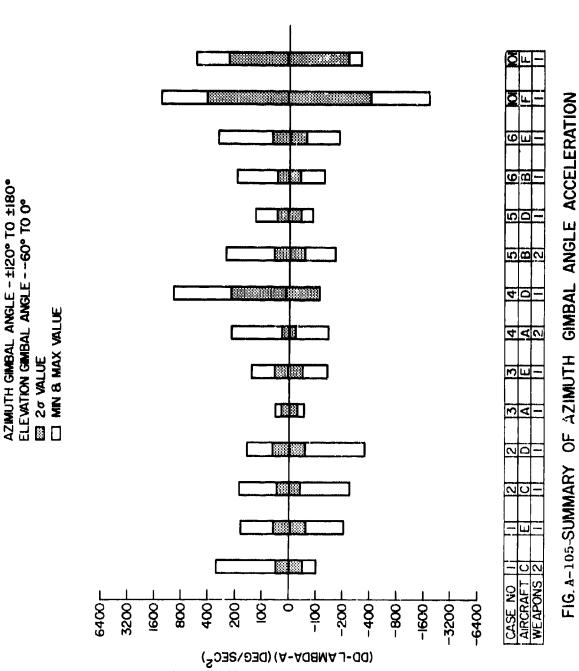


FIG.A-104-SUMMARY OF AZIMUTH GIMBAL ANGLE ACCELERATION

AZIMUTH GIMBAL ANGLE ACCELERATION



AZIMUTH GIMBAL ANGLE -0° TO ±180° ELEVATION GIMBAL ANGLE - +60° TO +90°

AZIMUTH GIMBAL ANGLE ACCELERATION (DEG/SEC<sup>2</sup>)

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FIG.A-106-SUMMARY OF AZIMUTH GIMBAL ANGLE ACCELERATION

**E** 98 ELEVATION GIMBAL ANGLE - -90° TO -60° AZIMUTH GIMBAL ANGLE -0° TO ±180° - D SB 2 4 E 20 VALUE
☐ MIN 8 MAX VALUE 4 **4** 0 S 3 2 d 2 CASE NO 11
AIRCRAFT C
WEAPONS 2 6400<sub>L</sub> -1600--3200 -6400<sup>L</sup> 3200 1600 88 200 8 901 -200 -400 98 0 (DD- $\Gamma$ AMBDA-A) (DEG\SEC<sub>S</sub>) AZIMUTH GIMBAL ANGLE ACCELERATION

FIG.A-107-SUMMARY OF AZIMUTH GIMBAL ANGLE ACCELERATION

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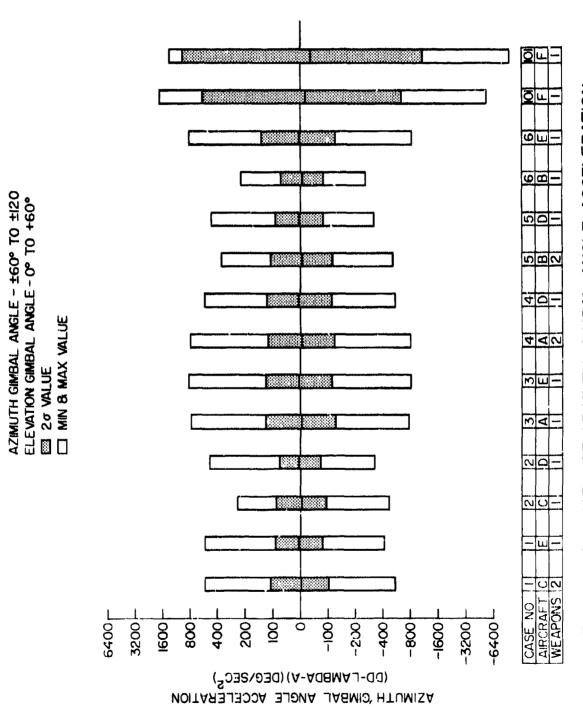


FIG. A. 108-SUMMARY OF AZIMUTH GIMBAL ANGLE ACCELERATION

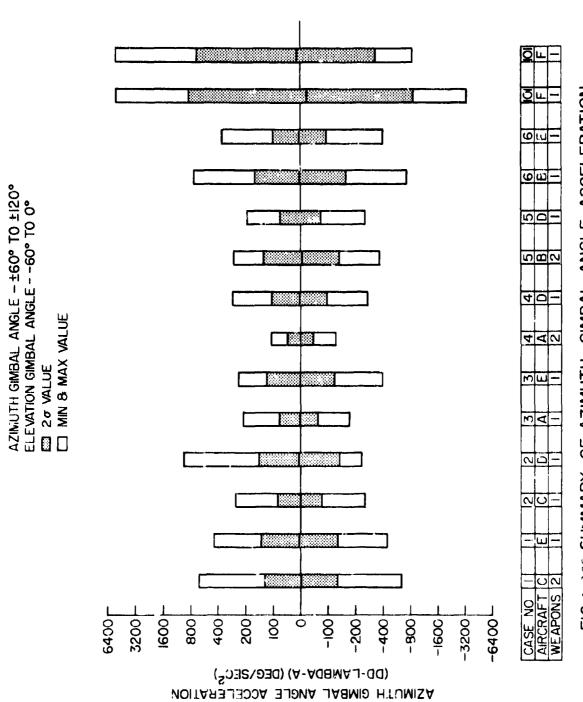
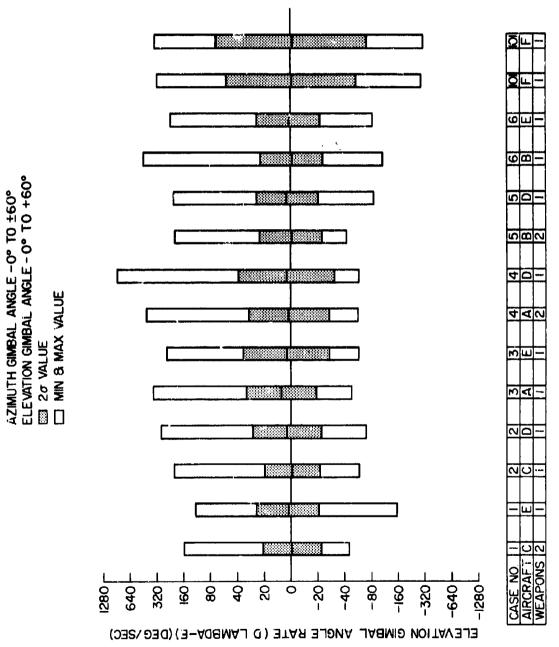


FIG. A-109-SUMMARY OF AZIMUTH GIMBAL ANGLE ACCELERATION



RATE FIG. A-110-SUMMARY OF ELEVATION GIMBAL ANGLE

98 AZIMUTH GIMBAL ANGLE -0° TO ±60° ELEVATION GIMBAL ANGLE - -60° TO 0° -02 282 40-E 2σ VALUE ■ MIN 8 MAX VALUE 440 MI -MA 20 2 -1280<sup>L</sup> 8 -20 4 8 -160 -320 -640 \$ 640 320 ဖွ 80 ELEVATION GIMBAL ANGLE RATE (D LAMBDA-E) (DEG/SEC)

RATE FIG. A-111-SUMMARY OF ELEVATION GIMBAL ANGLE

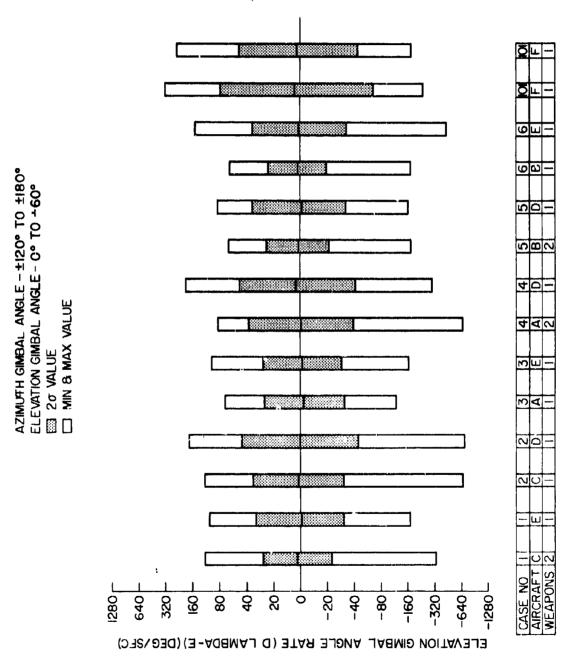


FIG. A-112-SUMMARY OF ELEVATION GIMBAL ANGLE RATE

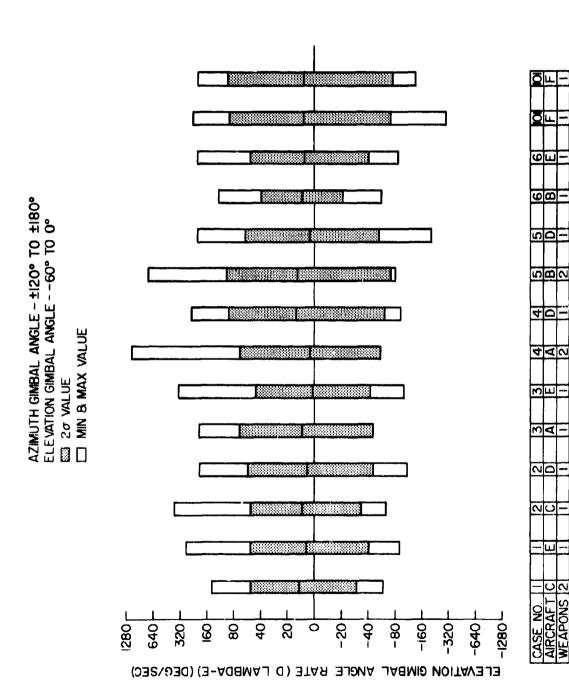


FIG. A-113-SUMMARY OF ELEVATION GIMBAL ANGLE RATE

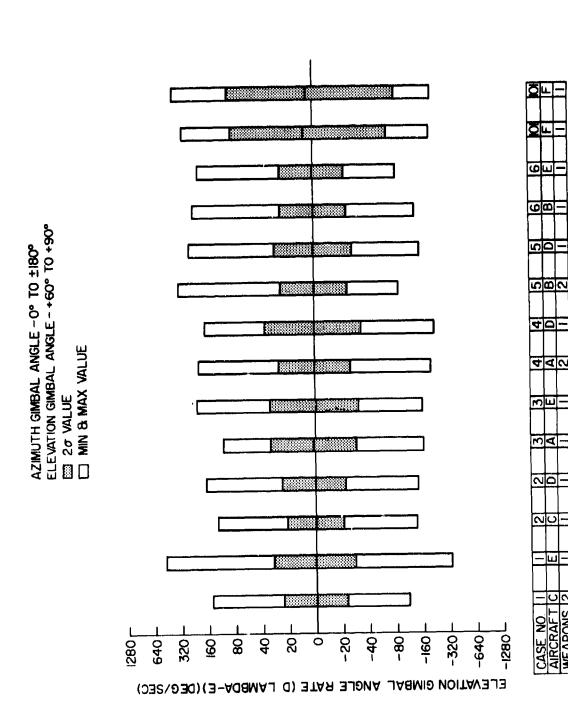


FIG. A-114-SUMMARY OF ELEVATION GIMBAL ANGLE RATE

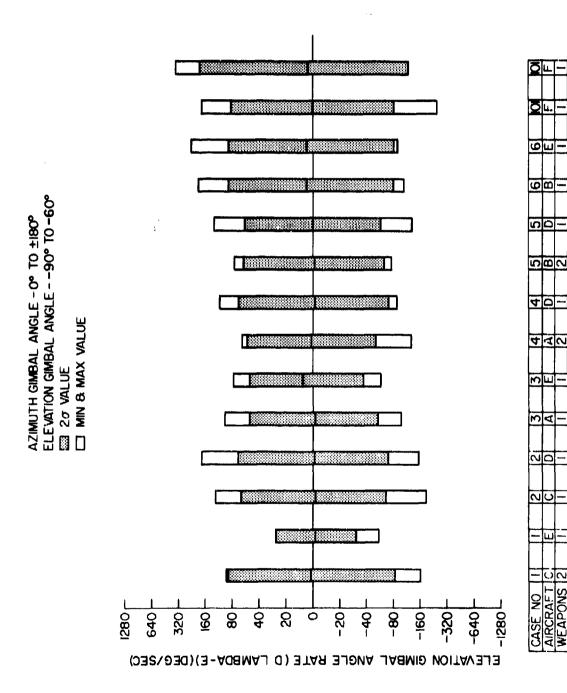


FIG A-115-SUMMARY OF ELEVATION GIMBAL ANGLE RATE

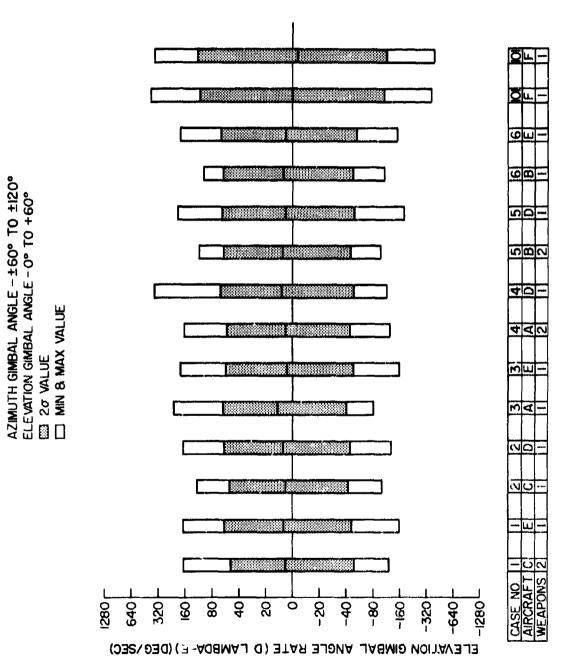


FIG.A-116-SUMMARY OF ELEVATION GIMBAL ANGLE RATE

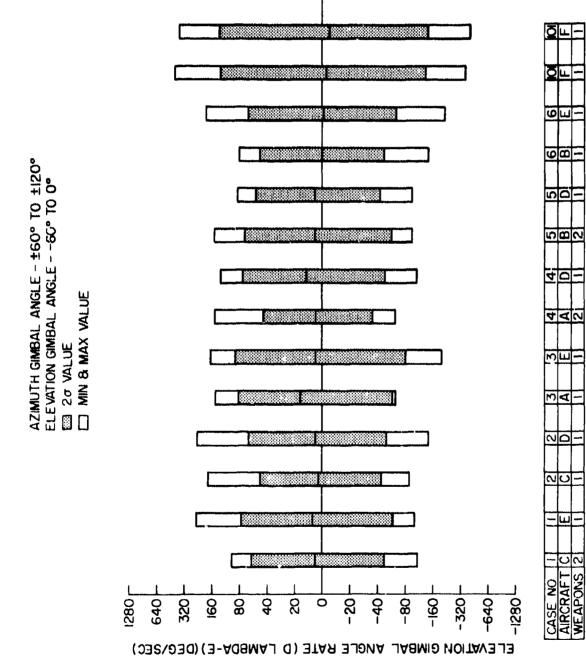


FIG.A-117-SUMMARY OF ELEVATION GIMBAL ANGLE RATE

**のできないからなっていますがある。** 

1-132

**E** 6 B ELEVATION GIMBAL ANGLE - 0° TO +60° AZIMUTH GIMBAL ANGLE -0° TO ±60° S 280 40 ☐ 2σ VALUE ☐ MIN 8 MAX VALUE 4 A S 3 E 20 3200<sub>F</sub> -1600 -3200L -800 8 -200 -400 0091 800 400 2002 8 ELEVATION GIMBAL ANGLE ACCELERATION (DP-LAMBDA-E) (DEG/SEC $^{\rm S}$ )

FIG.A-118-SUMMARY OF ELEVATION GIMBAL ANGLE ACCELERATION

AIRCRAFT C WEAPONS 2

A-133

ELEVATION GIMBAL ANGLE - -60° TO 0° AZIMUTH GIMBAL ANGLE -0° TO ±60° ☐ 2σ VALUE ☐ MIN 8 MAX VALUE -1600 -3200<sup>L</sup> 3200<sub>F</sub> 1600 800 400 -800 200 8 001--200 -400 ELEVATION GIMBAL ANGLE ACCELERATION (DD-LAMBDA-E) (DEG/SEC<sup>2</sup>)

2<u>B</u>2

40-

440

E 4-

20

NO-

FIG.A-119-SUMMARY OF ELEVATION GIMBAL ANGLE ACCELERATION

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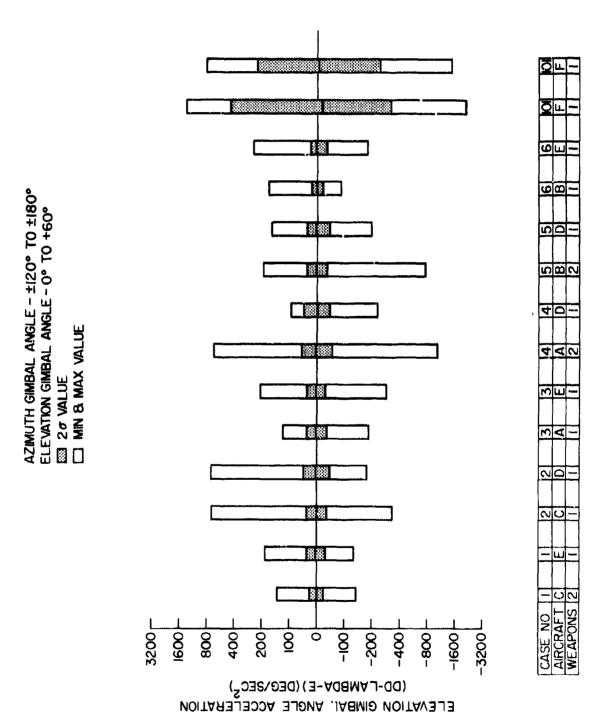


FIG. A-120-SUMMARY OF ELEVATION GIMBAL ANGLE ACCELERATION

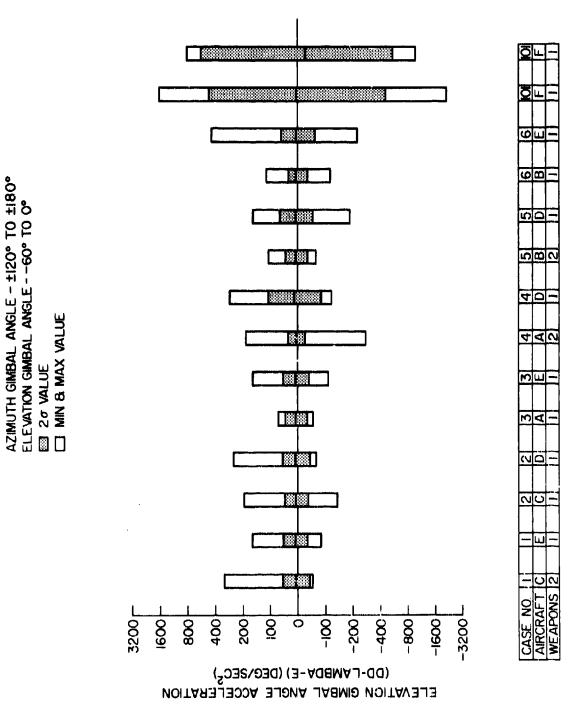


FIG. A-121-SUMMARY OF ELEVATION GIMBAL ANGLE ACCELERATION

ω<sub>0</sub> ELEVATION GIMBAL ANGLE - +60° TO +90° AZIMUTH GIMBAL ANGLE -0° TO ±180° 50 2 B Z 40-E 20 VALUE ■ MIN 8 MAX VALUE 4 A S **М** — BA-20 **NO-**3200 F -1600 -3200<sup>[</sup> 1600 80 4004 200 -200 -400 -800 ELEVATION GIMBAL ANGLE ACCELERATION (DD-LAMBDA-E) (DEG/SEC<sup>2</sup>)

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FIG.A-122-SUMMARY OF ELEVATION GIMBAL ANGLE ACCELERATION

AZIMUTH GIMBAL ANGLE -0° TO ±180° ELEVATION GIMBAL ANGLE - -90° TO -60° ES 2 VALUE IS MAX VALUE 3200 F -800 -1600 -3200<sup>L</sup> 1600 300 40C 200 8 00 --200 -400 Ó

FIG. A-123-SUMMARY OF ELEVATION GIMBAL ANGLE ACCELERATION <u>6</u> 98 20 2 8 2 40 4 A S <u>Б</u> — 3 A 20--20 CASE NO 1 AIRCRAFT C WEAPONS 2

A-138

ELEVATION GIMBAL ANGLE ACCELET ATION (DP-LAMBDA-E) (DEG/SEC<sup>2</sup>)

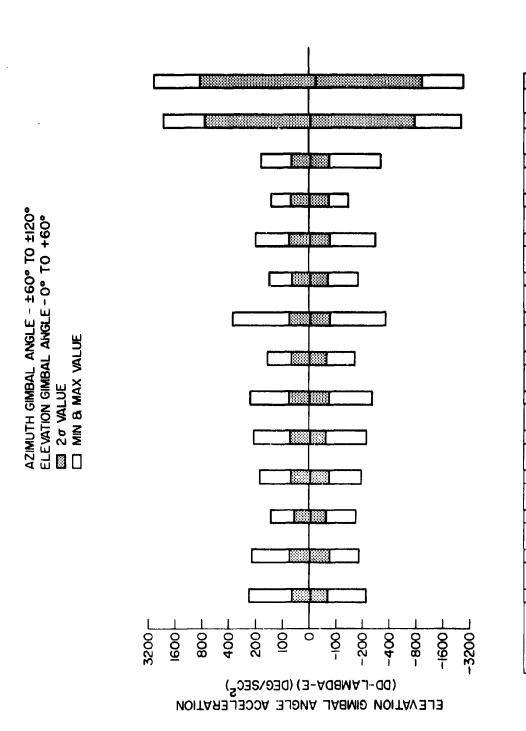


FIG. A-124-SUMMARY OF ELEVATION GIMBAL ANGLE ACCELERATION E G 9 50-282 40 4 4 2 20 **~**∪~ CASE NO 1 AIRCRAFT C WEAPONS 2

A-139

AZIMUTH GIMBAL ANGLE - ±60° TO ±120° ELEVATION GIMBAL ANGLE - -60° TO 0° **\*\*\*** \*\*\*\*\* □ 2σ VALUE
□ MIN 8 MAX VALUE 3200 r 800 400 200 -3200<sup>L</sup> 0091 8 8 -200 -400 -800 -1600

ELEVATION GIMBAL ANGLE ACCELERATION (DP-LAMBDA-E) (DEG/SEC<sup>2</sup>)

A-140

FIG. A-125-SUMMARY OF ELEVATION GIMBAL ANGLE ACCELERATION E G 98 50 **SB** S 40-4 40 3 MA 20 NO. CASE NO 1 AIRCRAFT C WEAPONS 2

## B. Parameters Interaction

This program performs a numerical bivariate cumulative probability distribution. It also has the additional capability to perform, at the same time, a frequency distribution of another variable. These capabilities are quite general; however, the remainder of the options of the program are more specific. These include classifying the data into three groups according to gimbal angle or restricting the data to a minimum range.

An important facet of the program is its capability to study the distribution of dwell times. For instance, the probability distribution gives the likelihood that a particular value of a variable is exceeded but it is also necessary to know for how long the value of the parameter is exceeded. To this end, the program gives the average dwell times and their standard deviations.

Following is a glossary of terms used in work completed with Program Inact. Additional details on the program: logic, inputs, and flow charts, are available.

ABS VC - Absolute value of the closing velocity.

ARDDOT - Absolute value of the range acceleration.

A VCBT - Absolute value of the target's contribution to the closing velocity.

AWJDF - Absolute value of the elevation stabilized line of sight acceleration.

AWJF - Absolute value of the elevation stabilized line of sight

AWKDF - Absolute value of the azimuth stabilized line of sight acceleration.

AWKF - Absolute value of the azimuth stabilized line of sight

DELTAR - Range to closest main beam ground return (given a 2.5° half beam width), minus the target range.

LAMB-T - Off-boresight angle of the target (total target aspect angle).

LT-DOT - Total rate of rotation of the target =  $(\lambda_E^2 + \lambda_A^2 \cos^2 \lambda_E^2)^2$  where  $\lambda_E$  = elevation gimbal angle,  $\lambda_A$  = azimuth gimbal angle rate  $\lambda_E$  = elevation gimbal angle rate.

RANGE - Range from fighter to target

R-DOT - Range rate

R-H - Absolute value of range minus fighter altitude

- (U) Using the following table as an example, an explanation of how to interpret the tables in Appendix B is given below:
- a. The top line identifies this interaction as one that is restricted to the zone off the nose of the fighter.
- b. The second line identifies the restrictions on the data as a minimum range of 225 ft and the off nose interaction is defined by  $\pm$  60° in azimuth and elevation.
- c. The third line identifies the parameters interacted. (refer to the glossary in Appendix B). In this case the Y parameter (listed down the page) is designated ABS VC which is absolute value of the closing velocity, and the X parameter (listed across the page) is designated A WJDF which is the absolute value of the elevation line of sight acceleration.
- d. In this case, the Y parameter is collected such that the absolute value of the closing velocity is less than 25, 50, ...., 250 ft/sec as shown in the first column on the left. The LIMIT is all values of the closing velocity less than infinity (unrestricted Y parameter). These restrictions on the Y parameter hold for the entire row.
- e. In this case, the X-parameter is collected such that the absolute value of the elevation line of sight acceleration is greater than 50, 40.5, ..., .5°/sec² as indicated at the top of each column. The LIMIT in this case is all values of the X parameter greater than zero (unrestricted X parameters). These restrictions on the X parameter hold for all numbers in each column.
  - f. Each block within the table contains four numbers:
    - NO. = number of entries into the zone defined by the X and Y parameters.
    - ii. PCT. = percent of the total combat time the conditions of the X and Y parameters were met.
    - iii. DT. = average dwell time in seconds that the conditions of the X and Y were met.
    - iv. STD. = standard deviation of the dwell time in seconds that the conditions of the X and Y parameters were met.
- g. As an example, take the X parameter value as 8.00 and the Y parameter value as 200.00. Referring to the intersection of these two values, it can be seen that for the absolute value of the elevation line of sight acceleration greater than 80/sec2 and the absolute value of the closing velocity less than 200 ft/sec2 the results are:

TABLE 1 PARAMETER INTERACTION OFF NOSE SHALIFFT TO CONDITIONS BRIN # 225.00 LANDA 60.00		34.00 24.50 48.04 2.00 8.00 4.50 2.00 6.50		6,01 0,01 6,01 0,01 6,02 6,07 0,12 6,23	1,00 1,00 1,00 1,00 1,00 1,13 1,25 1,16	6,00 6,00 0,00 0,00 0,00 0,00 0,00		0.01 0.02 0.03 0.03 0.09 0.17 0.27 0.51	1,00 1,00 1,00 1,00 1,22 1,24 1,36 1,23	5,00 0,00 0,00 0,00 0,63 0,55 0,42 0,50 1,79	;	7/ 96 17 77 1 9 19 19 19 19 19 19 19 19 19 19 19 19	1.00 1.00 1.00 1.17 1.19 1.19 1.18 1.180 1.180	0,00 0,00 0,00 0,00 0,55 0,50 0,96 0,62 2,92			1,06 1,00 1,60 1,80 1,20 1,25	0,00 0,00 0,60 0,00 0,54 0,63 0,64 0,62 2,91	201 100 17 20 101 100	0,02 6,04 0,06 0,09 0,16 0,26 0,36 1,32	1,00 1,00 1,00 1,00 1,10 1,21 1,21 1,32 1,52	0,00 0,00 0,00 0,00 0,51 0,61 0,62 0,97	2 5 8 10 20 34 38 129 129	0,02 0,04 0,06 0,08 0,18 0,33 0,45 1,68	1,00 1,00 1,00 1,00 1,15 1,21 1,41		3 6 10 14 25 43 75 155 219	0,02 0,09 8,08 0,11 0,22 0,42 8,81 2,02	1,00 1,00 1,00 1,00 1,00 1,00 1,00 1,00		3 7 41 14 26 48 68 182	60 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			3 7 12 19 26 93 46 199 0.00 0.00 0.00 0.00 0.00 0.00 0.00	1,00 1,60 1,00 1,07 1,14 1,26 1,40 1,74	0,00 0,00 0,00 0,25 0,44 0,68 0,40 1,20 3,91	3 6 13 16 36 96 109	C, 62 G, 00 0, 10 G, 14 0, 27 0, 56 1, 21 3, 06	1,00 1,00 1,00 1,00 1,00 1,13 1,25 1,39 1,73		35 75 122 192 283 461 571 833	0,26 0,60 1.04 1.76 2.99 5.45 10,22 28,83	1:00 1:00 1:00 0.25 0.46 0.96 0.99 1:67 0:12 9:71		471.93 701.10 724.52 739.05 722.89 684.56 678.55 662.49
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- i. number of entrance into this condition is 26
- ii. the percent of the total combat time this occurred is 0.24%
- iii. the average duration of this occurrence is 1.15
- iv. the standard deviation of this duration is 0.46 seconds
- h. The average values listed with the LIMIT cases denote the average values of the unlimited parameter while the other parameter is limited. As an example, the case where the Y parameter is less than 100 ft/sec. Going across the row to the case unlimited by the Y parameter, it is seen that the average X parameter is 2.48°/sec<sup>2</sup>.
- i. The bottom, right hand, corner block is noteworthy. This is the case where neither the X nor Y parameters are limited. Thus the only restrictions on these data are the initial conditions, in this case a minimum range of 225 ft and  $\pm 60^{\circ}$  in azimuth and elevation.

# 2. Tracking Parameter Interaction

- (U) The purpose of this section is to discuss the results of the tracking parameter interactions for the forward  $\pm 60^{\circ}$  field of view and for the total sphere coverage. The data for the graphs used in this section are contained in Tables Bl to B79 in Appendix B. The tabulated data contains a quantity and quality of information not possible to include on the graphs. The detailed explanation of the use of the graphs is contained in a preceding section of this report.
- (U) When interpreting the graphs for the interaction study (Figs. B-1 to B-57) it becomes obvious that several different sets of values of the interacted parameters produce the same probability of track with nearly the same average dwell time in track. When a limit is imposed on one parameter, only one value of the other parameter corresponds to a particular probability of occurrence. This, in essence, is the main use of these graphs: i.e., the influence of one parameter on the other. Keeping this in mind, a tradeoff analysis between the two parameters can be made.
- (U) When studying these parameter interactions, it should be kept in mind that three separate tracking loops are being investigated. The overall probability of track is the product of the three separate tracking loops. For example, a 0.95 probability in each loop yields a total of 0.86 probability of track. Further probabilities may be included such as range probability, clutter track-through probabilities, etc.

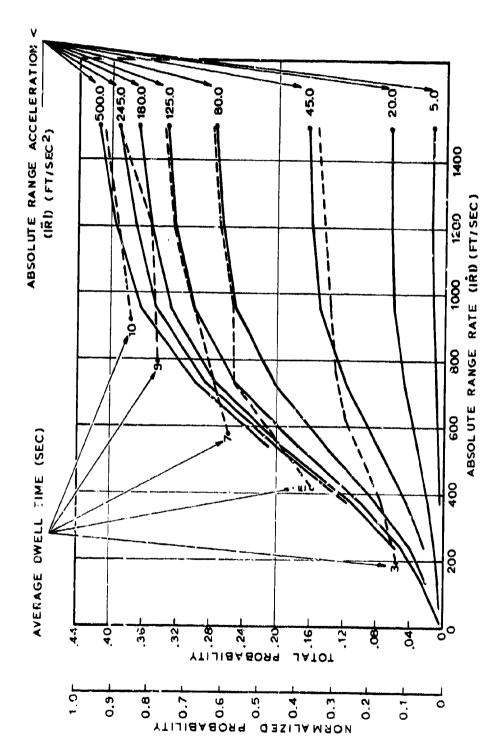
- (U) The preceding calculation assumed that the three tracking loops (range, azimuth and elevation angle) are independent, that is, not influenced by one another. The parameters interacted were chosen in an attempt to study variables which were not likely to be independent, that is, not influenced by one another. The parameters interacted were chosen in an attempt to study variables which were not likely to be independent, such as range acceleration and range rate. The next logical step is to combine all the variables and determine one overall probability. This is best accomplished in a tracking model, which is planned as the next step in this study. The output of the parameter interactions will provide the logical point at which to begin in the tracking model and provides an indication of the necessary steps for further improvement of tracking capabilities required of the weapon control system in a dogfight environment.
- a. (C) Range rate versus range acceleration (Fig. B-1, B-2, AI coverage; Fig. B-3 Total sphere coverage)

In the case of the AI radar, a range tracking loop with a range rate capability of  $\pm 1500$  ft/sec and a range acceleration capability of  $\pm 500$  ft/sec would provide a 0.95 probability of range track within gimbal limits of  $\pm 60^{\circ}$ . The average length of track is approximately 10 seconds. Figure B-2 is an expanded portion of the data in Fig. B-1 as shown by the shaded area in the upper right corner. For high probability of track considerations this is the most important region for trade-off consideration.

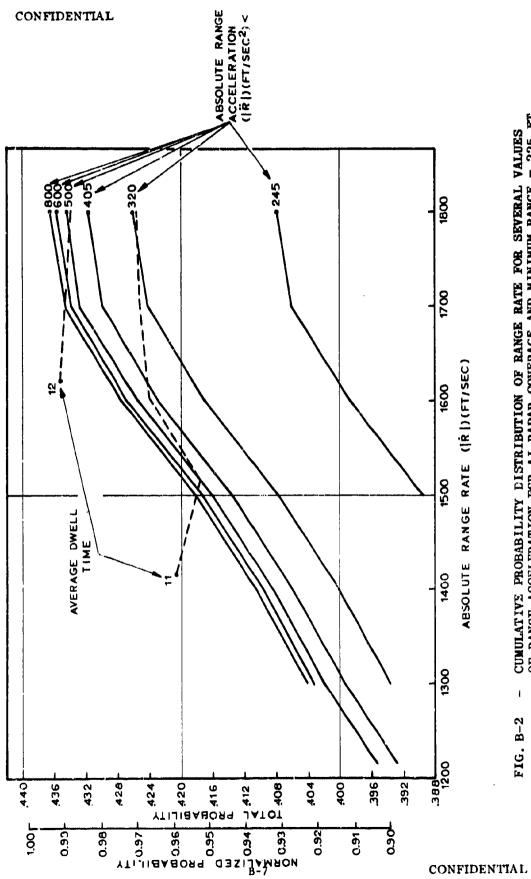
b. (C) Azimuth line of sight rate versus azimuth line of sight acceleration. (Fig. B-4, B-5, AI coverage; Fig. B-6, Full sphere coverage).

In the case of the AI radar, a 25°/sec azimuth line of sight rate and a 25°/sec<sup>2</sup> azimuth line of sight acceleration capability provides a 0.97 probability of track while within gimbal limits. The average duration of track is 12 seconds.

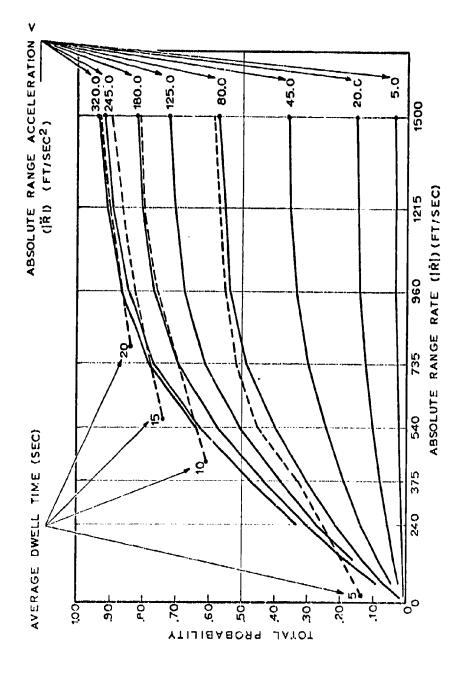
- (C) In the case of the full sphere coverage, the same values yields a 0.94 probability of track for an average duration of 38 seconds.
- (U) In order to determine the requirements for a higher probability of track, it is necessary to refer to the data contained in the tables in this appendix.



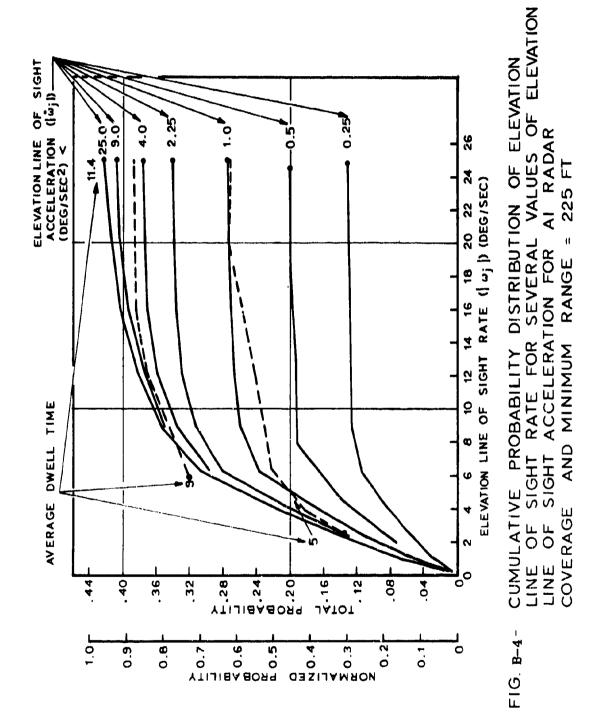
PROBABILITY DISTRIBUTION OF ABSOLUTE AND COVERAGE A RANGE RATE FOR SEVERAL ABSOLUTE ACCELERATIONS FOR AI RADAR COVE RANGE = 225 FT CUMULATIVE MINIMUM B-1 FIG

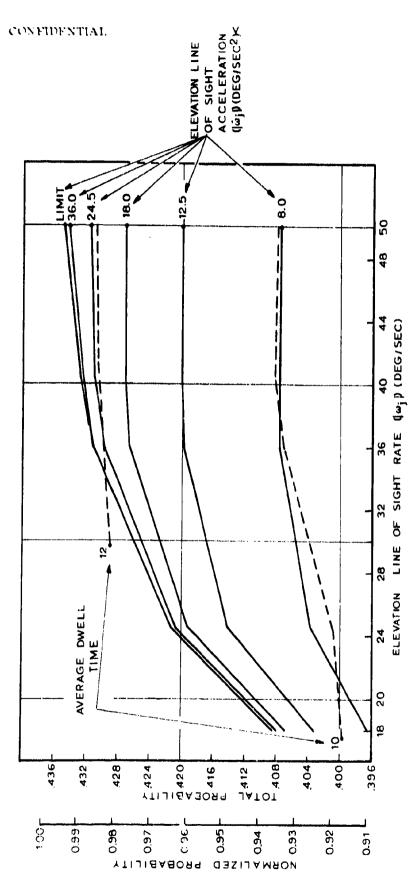


CUMULATIVE PROBABILITY DISTRIBUTION OF RANGE RATE FOR SEVERAL VALUES OF RANGE ACCELERATION FOR AI RADAR COVERAGE AND MINIMUM RANGE - 225 FT

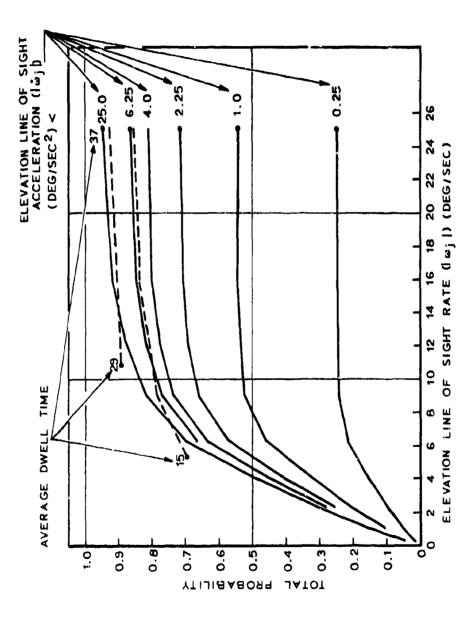


PROBABILITY DISTRIBUTION OF ABSOLUTE COVERAGE RANGE SPHERE SEVERAL ABSOLUTE FOR TOTAL = 225 FT RANGE RATE FOR SEV ACCELERATION LIMITS AND MINIMUM RANGE CUMULATIVE FIG.B-3 -





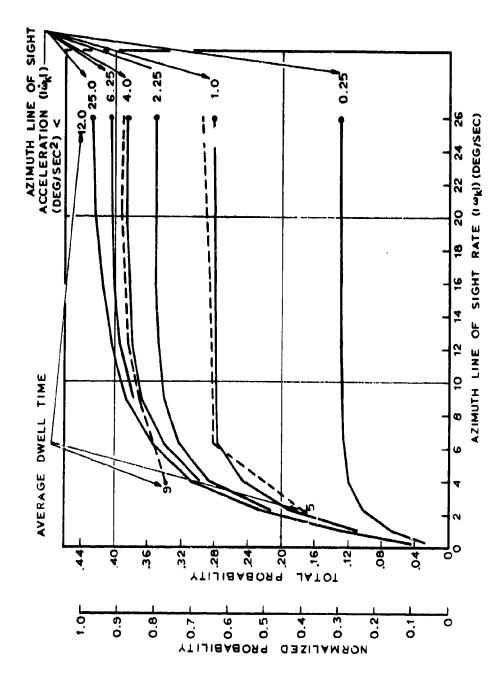
CUMULATIVE PROBABILITY DISTRIBUTION OF ELEVATION LINE OF SIGHT RATE FOR SEVERAL VALUES OF ELEVATION LINE OF SIGHT ACCELERATION FOR AI RADAR COVERAGE AND MINIMUM RANGE - 225 FT FIG. B-5



ON OF ELEVATION VALUES OF ELEVATION FULL SPHERE CASTRIBUTION OF 225 FT RATE FOR SEVERAL ACCELERATION FOR RANGE MINIMOM PROBABILITY AND SIGHT CUMULATIVE COVERAGE 0F 0F LINE FIG.B-6 -

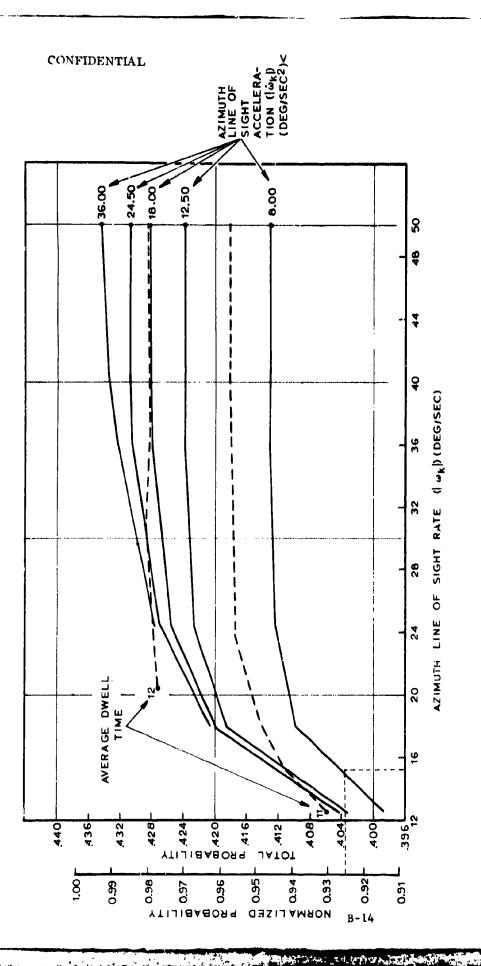
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- c. (C) Elevation line of sight rate versus elevation line of sight acceleration. (Fig. B-7, B-8, AI coverage; Fig. B-9 Full sphere coverage.)
- (C) In the case of the AI radar coverage, 25°/sec elevation line of sight rate and 25°/sec<sup>2</sup> elevation line of sight acceleration yields a 0.95 probability of track with an average duration of track of 11 seconds.
- (C) In the case of the full sphere coverage, the same values yield again a 0.95 probability of track with now an average duration of track of 37 seconds.

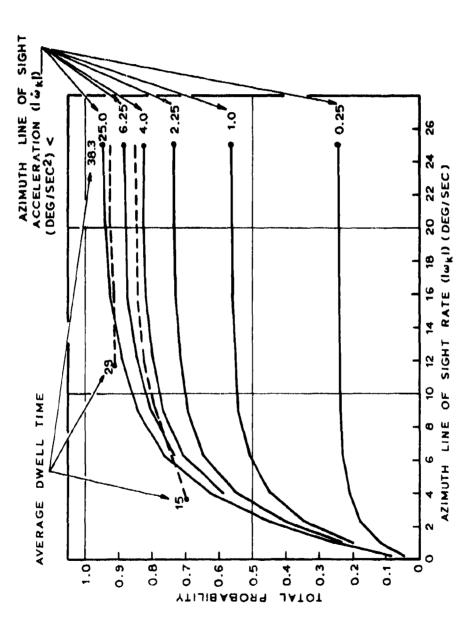


DISTRIBUTION OF AZIMUTH 225 FT FOR OF SEVERAL VALUES ACCELERATIONS RANGE = AND MINIMUM FOR SIGHT CUMULATIVE PROBABILITY SIGHT RATE OF CCVERAGE LINE AZIMUTH LINE OF RADAR FIG. B-7

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CUMULATIVE PROBABILITY DISTRIBUTION OF AZIMUTH LINE OF SIGHT RATE FOR SEVERAL VALUES OF AZIMUTH LINE OF SIGHT ACCELERATION FOR AI RADAR COVERAGE AND MINIMUM RANGE - 225 FT



SEVERAL VALUES OF AZIMUTH ACCELERATION FOR FULL 225 FT DISTRIBUTION OF AZIMUTH RANGE MINIMOM AND SIGHT SIGHT RATE FOR CUMULATIVE PROBABILITY OF COVERAGE LINE LINE OF SPHERE FIG. B-9 -

- Tracking Requirements Interaction Data Tables
   Tables for tracking requirements interactions
  - a. Range track
    - 1. Nose section (AI radar coverage) Table 2-1
    - ii. Tail sector Table B-2
    - iii. Full sphere Table B-3
  - b. Azimuth angle track
    - i. Nose sector (AI radar coverage) Table B-4
    - ii. Tail Sector Table B-5
    - iii. Full sphere Table B-6
  - c. Elevation angle track
    - i. Nose sector (AI radar coverage) Table B-7
    - ii. Tail sector Table B-8
    - iii. Full sphere Table B-9

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	<b>40,0</b>		2050.00	216		7,45		907	35.12		90'9	447	16.95	10.85	8,99	į	424	***	20.0	•	427	40,22	11,00	9.42	767	40.35	11,02	9.50	į	77.		96.6		422		10 57	!	422		70.01		422	40.47	12,02		421	46,49	12:05		92,44
į	8FF MUSE 225,00 LAMBAR		1000.00	216		7,45	. ;	-	77.00			457	39.58	10.85	64.4	ļ	421	10 mm	.22	1	427	40,22	11,80	. 42	7.57	40.35	11.02	4.50	ţ	77.			,	422		16.21	•	422	40 47	76'77	<u> </u>	422	40.47	12,02	* 2 *	421	46,49	12.05		82,44
			1800,00	216		7,46		487	90.00		124	454	39.51	10.61	9,00		900	24.42	25.	:	428	40.16	11,76	.43	367	60.70	11.88	1610	į	42.0	14.65	96.0	,	423		17.0	}	423	**************************************	11,47		423	40,41	11,97	66.	422	40,43	12,50		82,45
SLE B-1	TANAMETER INTERACTIONS	TAPE 40.	1700.00	12 71 14 71		7.50		244	27	2	6,36	797	30.83	10.62	90.04		999	34.45	17171	2	434	76 62	11,54	67.5	•	77.47	11.63	4.57	į	45.04		4.62		430	, , , , , , , , , , , , , , , , , , ,	17.0	<u>:</u>	430	40,22	11.	;	430	40,22	11,72	1	429	40,25	15,76		82,53
TABLE	TO CONDITI		1600,00	14 74 B		7.63		510	37,16	2	۲, ۱ ۵	483	38.61	10.02	9,16	. ,	777	20 65		-	454	39,26	10,63	19.	;	10.10	10.89	4.73	į	164	40.01	44.6	•	157	***	, a	•	187	16.18			451	39,51	10,98	0,1	451	59,55	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	9	82,96
	SUBJECT		1900,00	482		7,70		200	26.23	, d	1010	476	37.68	98.6	9,27	. :	9 P		70.0		454	38,32	18,98	4.77	137	18.4	10.64	98'6	١	104 67		06.6	•	453	C .	9 6 0		454	56,57	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6		434	38,57	18,65	D * *	454	38,60	10,65		85,98
			1496,63	19.11		7,67	. !	472	35,47	7	20.0	472	54.92	9.8	9,28	. !	454	27,55	35.0	-	**	37,57	1012	9.78	977	67.63	10.52	4.87	;	17 73		26.4	•	451	0/1/0	10120	•	452	37,61			452	37,81	10,48	1	452	37,84	10,49		62,18
			1300,00	44, 22		7,46	, !	432	34,50	1364	210	447	15.27	9.73	42 d	, ;	452	3616	74.0		447	26,62	62 TO 1	9,65		17.75	1 0 M	95 6	, ;		P	4.0		451	21.0	7,101	2	269	37,117		-	269	37,117	001	9,1,	45.5	57 £ 14	10,28	DATA	#1 # C4
	4800			D .	; ;	STD		2	5	-	1016	ž			STO.		E .				, ,	-	5	570,	5	ב ב ב		STE	•			STE.	•	9				ě	֡֞֜֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֜֓֓֓֓֓֓֡֓֡֓֡֡֓֡	-	•		PCT	5	5 L C	₩ Θ	2	<u>.</u>	- - -	, 9VG
	PARAMETER			160,66	-	,,		245,00	-			A. 0. A.	_		-		405.00	-	J		500,00	-				2011				00.007				800,00		-		900,00	-	•		1000.00						-		

	•
	00.09
	OFF TAIL 225,00 LAMBA =
TABLE B-2	PARAMETER INTERACTION OFF TAIL Subject to Conditions RHIN = 229,00 LANDA

200 2745464			250000	ום רמצהזי	PILL SEDI	1677	. 40447 00	70,00		72766	74 200 420	
משטבונים שוחת					TAPE NO	•					A. 504 KM	
	1300,00	1490,00	1505,00	1600,00	1700,00	1800,00	1900,00	2000,00	2100,03	2200,00	LIMIT	
160,00 %6,	415	416	421	421	424	423	454	454	425	454	454	
LO4	19,56	19,67	12,77	19,86	19,93	19,95	19,97	20,01	20,02	50,05	20.05	
010	5,65	5,94	5.65	5,91	5.89	5.91	5.90	5.91	9,0	5.92	5.65	
STE	6125	62,9	6,23	6,23	6,21	6,21	4,21	6,21	6.21	6,21	6,21	
		i			į	-		į			423,08 AVE	
24.00 NE	700	400	999	383	200	287		207			200	
	20122	20.4	23,03	21,12	21,21	47.12 6.88	21.25	21,29 6,88	21,31	21,53	21.53	
מומ	62 6	À.0	* *	1440	•	A9 * 0		0.0		9 . 6	420.05 AVG	
320.00 he.	365	365	368	366	367	366	368	367	367	166	366	
1	21.52	21,69	24.81	21,91	24.08	22.00	22.03	22.07	22+04	22.11	22.11	
	7.29	7,45	7.43	7.50	7.90	7,93	7.50	7.93	7.54	7.57	7.57	
STC.	7,23	7,24	7.24	7,26	7.27	7,29	7,00	7,39	7.38	1,58		
	•		•	•	•	۲	•	,	•	•		
405,00 he,	763	356	358	356	357	256	258	157	397	<b>98</b> 2		
PCT.	21,47	22,04	22,15	22,25	22,32	22,35	22,37	22,41	22,43	22.45		
	7,168	7,76	7.75	100	7,83	7,87	7.87	7,67	7187	4,40		
STE	7,150	7,31	7,52	7,33	7,34	7,36	<b>1</b> 7	7.47	7,46	7.47		
40.00	×	163	791		161	16.3	787	18.1	188	-		
108 201000	200	376	200	325	25.00	350	4	200		30.00		
	7.1.7	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	7.88	40.4	90.6		7.96	7.00	70.7	10.0		
	1	7.76				7.4	4.					
,	), T			•	3	•		•	1	<u>.</u>		
_	352	351	350	165	352	351	393	352	352	351		
PC1	22,51	42,18	22,31	22,40	22,47	22,50	22,53	22,57	22,59	22,61		
1	7,84	7,92	7,92	8,00	00.	6,03	00.4	8,93	9104	101		
STD,	7,36	7,37	7,37	7,39	7, 30	7,41	7,43	7,34	7154	7,55		
	1	;	•		•	,	į	į	į			
700.00 86,		9 6 6	100		330		167	390	250	97		
_	52122	77:29	62,52	22,44	22,51	22,24	76,55	72,01	\$912Z	22,63		
1	7.10	7.17	0 P	9 7 7		7.42	7.4.7	7.5	757	56.7		
5	-	•	<u>:</u>				-		-			
600.00 NS.	350	349	351	349	350	349	351	150	330	349		
	22,06	22,23	22,35	22,46	22,53	22,56	22,59	22,63	22,65	22,67		
5	05"4	7,98	6 · ·	90	6.07	0 T	8,07	8,10	## 			
200	0,7	100	(5)	100			?	100	121	661/		
900.00 NE.	064	349	191	348	986	340	351	350		140		
104	32,05	22,24	22,57	22,47	22,95	22,56	22,61	22,65	22,67	22,49		
	7.63	7,99	7,99	6,07	6,07	11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	8,87	11 0	6,114	57.0		
STC	136	7437	7,37	7,39	7,60	7,62	7,43	7,34	7,54	7,55		
*000 00 PB.	60 60 60	199	351	946	351	350	355	867	465	340	9AV 56"344	
	22.68	22.25	22.38	22.48	22.36	22.50	22.63	22.67	22,68	22.73		
	7,91	7,99	4.09	8,07	6.03	80.0	90	110	6112	8,15		
STE	7.26	7,37	7,38	7,39	7.40	7,42	7,43	7,94	7434	7,55		
	. :	. ;	. ;	. ;	. 1		. 1	į				
102 CE 14			167		351	37 60	25.					
	11177	86 Z		8C 122	20.22	66,63	1, 7	7,77	7,57	27.27		
STD	7.36	73.7	7, 48	7.39	7.30	7,42	24.4	7,94	7.94	7.55	7.95	
•	•	•	,	•	,	' '		,	. !	'	443,87 AVB	
J A C	91,08	92,49	10,56	95,34	95,57	95,75	95,97	95.43	20156	95,67	95,87	

	X PARAMETER ABS VC		756	65,82 85,85 65,85	15,51	17.60	X14 X14		15, 80	17,70 17,70	•	04 00		24.44 24.47 24.47		374	95,77	10°20 10°00 10°00		E-1 ACCINES NOT SOC	96.80	40156 40,79 60,78	34,62 34,62		262		40.69				47°B6 47,07 47,07		101	50.00 00.00			55		_		146 149 145		77.00					000 34.044 44.044 44.044	
			-	83,81	11,50	12,01	753	11.61	15,79	17.71	708		23,24	21.68		275	95,73	66'17	42.65	288	96,76	68,85	34,96	•	767	48.24	40,04	•	212	57.00	65,43		25	75.26	19.56		85	77.77	7	,	91			<b>1</b> 3.57		÷	762.67		
360 DE65		0000	216	63,77	11,50	10'21	71.3	89,80	15,78	17,71	***	/0C	28.00	24.67	•	176	92.60	31,89	62147	67	96.72	7.5	75 77	786	44.40	70.07	40,05		512	57.54	47,06	,	163	75.22	58.57		150		66.99		147			63151	7	962.34	724,22	119.48	
		. ·	•				713	89,72	15,77	17,71	70%	14.71	23.2	21.67		275	93.60	100	92197	299	29.96	40.49	36,52		67.76	48.17	16.09		777	57.76	47,03	,	192	77.77	58.55	•	151	101	61.65	ı	167				7,7	735.18	598 54	119.47	• •
TABLE B-3 PARAMETER INTERACTION TO CONDITIONS RMIN =				63,48				16'61				210						11,20		307		20,26		24.3		46.42					47,38				58.62			72.24				66.20					340,96	119.26	
PARAM CT TO COND				82,71				88,73			***			21.78				29.62		326		46 90		6		42,77					47,52				58.5						176						140,00	119,44	•
Suesent	<b>i</b>	1560.68	1	61,71				67,70			904			24,77				12 42		328		36,14				42.02			700	4.00	47,11	1	215	70.07	58,02	•		60.00			182					70.74		118,62	•
		1466.00	)	90'10				86,83			422	127						24.47				26,45		28.4		42.06					44,65	,	212	12.4	25.75	•		40.00			182	10,04	1			117.95		118,11	
	767	1366,16	970	80° 6	111		477	86,10	15,154	17,54	23.7	95-68	21.80	21,69	•	750	74 75	32142	4,1,7	124	12,85	15,21	14,14	280	89.50	11	39 65	776		48,24	46,07		212	70.75	53,40	•	111	40 L	199.47								15,81	117,29	•
	PARAMETER APDOGT		160,00 NE	ະວິດ	14,	-	245,00 hB	PCT		STD	320.00 MB.		1	STE.		405,00 NB			- - -	500,00 %8,		1	1015	94 66 664			STD			6	ste,			3 6	\$10.				STD		1006,00 115,				LINIT NG.		src.	AVG	

	R AWKF		LIMIT	74.57	, W. W.	8.43	2.92 AVB	264	10.72	9.15	3.34 AVG	435	11.32	E .	3.51 AVG	426	39.65	1.2.00 0.1.00	3.67 AVG	55	11.76	9.57	3.81 AVG	52	11.67		3.93 AV6	422 46-18	11.93	9.59		40.24	11.95		4-08 AVB	+0.32	12.00		421 421	+0.36	12,01	9.58		64.04	12.05	4.48 AVG	
	X PARAMETER	•	20.00	36.57		8.43	į	250	10.77	9-15		435	11.37	9.38		426	39.65	00°10		\$24	11.76	9.57	• •	*2*	11.83	9.58	. !	423	11.89	9.58	423	40.20	11.91	9.58	724	40.53	11,95	47.53	422	40.24	11.95	9.58	422	40.25	11.95		1.95
			45.00	26.57	8.86	B.4.3		<b>P</b> 0.0	10.07	9.15	, ,	<b>433</b>	11.37	9.36		425	39.63	9.50		<b>424</b>	11.78	9.57	, ,	524	11.85	9.58		422	11-91	9.58	422	40.16	11.92	9-58	124	40.18	11.36	- A- 128	421	40.18	11.96	9.58	124	40.19	11.96	00.0	1.92
:	00-00		0 0 0	110	A	8.49	į	450	10.77	9.15	i !	433 20	11.37	8E'6		425	39.62	9.58	,	424	37-00C	9.57	; ;	<b>4</b> 23	11-84	9.57	. !	423 40-04	11.86	9.57	423	40.08	11.87	9.57	422	40.10	11.91	9.56	422	40.10	11,91	9.56	422	+0-10	11.91	000	1.84
OSE	225+00 LAMUA*		35.00	74.67	A 8	8.43	•	054	10-27	9-15		433 20	11,47	85.0		425	39.60	9.58	•	424	18466	9.57		*2* 0.0	11.79	9-57	٠.,	\$2 <b>\$</b>	11.80	9.56	425	39.96	11.78	9.57	454	39.98	11.31	9.57	454	39.98	11.01	9.57	424	39.98	11.91	15.5	1.17
			30.00			8.43		<b>4</b> 20	10.77	9-15		433 30	1 2 3 4	96.98		425	39.56	9.58		424	11.74	9.57	į į	424	11.75	9.57	į	424	11.76	9.57	Š	19.61	11.74	9-58	424	39.82	11.77	4.57	424	39.82	11.77	9.57	424	39.82	11.11		1.68
TABLE B-4	Kith Pho	TAPE NO.	25.00	36.56	8.37	200	į	, e	10-01	9.16	į	434 30 18	11.31	9,31		427	39,39	9.51		426	11.62	9.50		20 60	11.63	9.50	į	39.54	11.63	9.50	427	39.56	11,61	9-50	427	39.56	11.61	05.0	427	39,56	11,61	9.50	427	39.56	11.61	70.4	1.58
TABLE B-4 PARAMETER INTERACTION	1.10%07.01	,	00.05	24.46	8.00	8.44		X .	10.75	9.16		4 35 0 0 0 0	11-21	9.29	•	624	39.06	9.45		\$ 5 S	11.42	9.45	! !	DF • 6€	11040	9.45	!	430	11.40	9.45	24	39.15	11,35	51.5	432	39-15	11.35	54.6	432	39.15	11,35	9.45	21.0	39-15	11.35		1.46
1	308366	1	15.00	36.15	26.0	8.4.5			05.00			98.00	19.87	9.25		<b>+35</b>	38-06	9*35	į	96	10.95	9-35		154 90	10.93	9.35	į	38.12	10.93	9.35	438	38-12	19.61	9+35	438	30-12	10.91	9.35	438	38.12	10.91	9.35	438	38.12	16.01	ח יה	1.28
			10.00	4.45	20.00	8.51	į	45. 26. 95.	00.00	F 10 - E	;	94.49	10.08	90.6		844	36.16	9.12		449	10,10	11.6	;	000	10.05	9.11	į	96-19	10.08	9.11	451	36.20	10.06	9.11	<b>451</b>	36.20	10.06	9.11	451	36.20	10.06	9.11	(54	36.20	10.06	11.	1.11
			2005	29.82	7.99	8.41	ţ	4 5	30 - 16 10 - 16	8.52	į	476	0.00	8.49		478	30.47	0 4 a	i	67.9	00.1	8	į		06.2	6.49	i	47A	7.99	6 <b>4.</b> B	470	30.49	7.97	8-48	479	30.49	7.97	80 4.	479	30.49	7.97	80 4.	479	30.49	7.97	0	0.85
	PARAMETER 18KDF		C 2		ב	stn.		. D. C.	֓֞֞֝֓֓֞֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֡֓֓֓֡	STn.		.CM 00.41		STO		20.00 NO.	PCT.	STD.		25.00 NO.		sto.		30.00	֖֭֭֭֭֭֭֭֭֭֭֭֭֭֓֞֞֞֞	STD.		35.30 NO.	o.	STD.	40.00 NO.		.10	sto.	45.00 NO.	PCT.	PT.	ST9.	50.00 NO.	PCT.	oT.	STO.	LIMIT NO.			SID	PAG.

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		IKF.		. M	٠	Ñ			2 M		ŵ	O AVG	20	, <u>c</u>		7 AVG	2 0	•	9	S AV6		2 5	•	9 AVE	، ب	ıņ.	٠,		9	æ	•	ιō.	A AVG	• •			9 4 9	. N	•		7 AVG		-	8 AVG		•	~ .	Y VE	
		TER AWKE	177		19.8	6.1	6.61	9	53.15	2.5	7.7	2.9	ה ה ה	7.7	7.4	2.9	22.1	7.9	7.5	3.0	֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓		-	3.0	#	22.4				22.4	8	7.5	3.1	22.5	8	2.5	~ *	22.5	6.3	() ·	3.17	22.6		, F	m	25.7			3.1
		X PARAMETER	C. 67	405	19.86	6+15	6.61	356	21.53	T-58	7.43	196	50°.	7.78	7.47	ý	22.18	7.94	7.50	1	,	22.34	7.50	•	746	22.45	8.11	PC=/	348	22.48	8.69	7.55	6	22.52	8.69	7.56	249	22.55	8.10	7.56	340	09*22	9-11	<b>5</b> 0.	349	22.75	6.17	60.	3.95
			45.00	10 <b>4</b>	19.86	6.15	6.61	35.6	53.12	7.58	7.43	9	50,15	7-78	7.47	,	22.18	7.94	7.50		346	26.34	7.50		347	22.45	H. 1	06.7	346	\$2.48	8.09	7+55	9	22.52	60.0	7.56	946	22.55	8.10	7.56	945	22.60	8-11	D	349	22,75	8-17	0	3.05
	60.00		40.04	405	19.86	6.15	6.61	750	21.53	7.58	7.43	,	59,15	7.78	7.47	ğ	22.18	7.94	7.50		348	200	7.50		347	22.45		00.	348	22.48	8.09	7.55	4	22.52	8.09	7:56	046	22,55	8.10	7.56	340	22.50	8.11	0	340	22.75	8.17		3.05
i	TAIL 30 LAMDA =		35.00	405	19.86	6.15	6.61	356	21.53	7.5A	7.43	196	20.15	7.78	7.47	į	22.18	7.94	7.50	1	848	20.00	7.50		347	22.45	11.6	96.	348	22.48	60.0	7.55	Č	22.52	9	7.56	012	22.55	8.10	7.56	946	22.60	9-11	064	349	22,75	9-17	(6.2)	3.65
	FION OFF T	,		404	19.86	6.15	19-9	356	21.53	7.58	7.43		60.10	7.78	7.47	ý	22.17	7.94	7.50		36.00	55.55	7.50	•	347	22.44	3.10	900	348	22.47	8.09	7.55	676	22.51	80.00	7.56	946	22.54	8.09	7.56	946	65.22	A.11	BC •	349	22,73	9:10	66.4	3-03
ABLE B	PAWAWELEW INTERACTION TO CONCITIONS RMIN =	10.4	25.00	402	19.84	6.18	29.9	25.2	21.51	7.63	7.43	9	21.99	7.84	7.48		22.15	7.97	T.51	1	348	20°8	7.50	•	347	22.41	9 0 0	0 0 1	348	22.44	80.8	7-56	046	22.48	B.07	7.56	945	22,53	8.08	7.56	641	22,55	0.00 0.00 0.00 0.00		348	22,68	\$1.6 F	•	2+98
	TO CONCIT		20.00	462	19.43	6.1B	6.62	78.7	21.49	10.6	7.44	046	21.88	7.86	7.48	•	22.12	7.97	7.50	1	3 7	12.22	7.49	,	347	22-38		n C	348	22.41	8.07	7.55	Č	22.4E	8.06	7.55	346	22.47	8.07	7.56	346	22.51	9.08	D .	349	55.65	B	56.	2.06
	SUHJECT		15.00	397	19.73	6.23	6.63	151	21.37	7.63	7.43	546	21.76	7.81	7.47	845	21,97	7.91	7.49	ć	340	7.97	7.48		347	22.20	7.55	00	348	22.23	4.0 E	7.54	946	22.27	8.00	7.55	646	22,29	8.00	7.55	6.46	22,33	8.02		349	22.44	90.06		2.78
			10.00	387	19,39	6.28	99.9	345	20.86	7.58	7.43	243	21.16	7.73	7.47	445	21,31	7.76	7.48	į	34.5	04.7	7.48		344	21.45	7.48	•	344	21.46	7.82	7-48	446	21.49	7.83	7.49	**	21.50	1.83	7.49	**	21.53	7.84	•	344	21.62	7 - 88	•	2.43
			5,00	364	16.96	5.84	6.67	97.6	17.81	6.21	6.74	176.	17.95	6.23	6.73		18.00	6.23	6.74	•	705	36.4	6.74		362	18.06	6.25	n . • 0	362	18.04	6,25	6.73	676	18,04	92.9	6.74	262	18,09	6.24	6.74	362	18.09	6.24		362	18.13	6.28	•	1.75
		PARAMETER ANKIDE		5.00 NO.	֖֖֭֭֝֟֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֟֝֓֓֓֓֓֓֓֓֟֓֓֓֟֓֓֓֟֓֓֓֓֓֓֟֓֓֓֓֓֡֓֡֡֡֡		<b>410</b>	10.00 NO.	PCT.	o1.	STO.	15.60 10.	PCT.	T.	STD.	20.00	PCT.	nT.	stn.			- E	STD.		30.00 40.	בים		•0.4	35.60 NO.	PCT.	Ţ.	510.	60	PCT	DT.	STD.	45.60 NO.	PCT.	Ţ.	sto.	50.00 NO.	-	-	•	LIMIT NO.	<b>•</b>	• • •	•	405.

						AVG	·			AV6				AVG				AVG				AVG				AVG				AVG			,	940			775	2			ų				AVG	<u>:</u>
	77,47		1 1 M 1 T	85.95	13.72			92.39	26.65		04.40	1.13			7 7 7	37.48				42°14	50.11		223	.6.4			13.5	64.05			97,93	73,04		, A	98.24	55.55		211	9.00	160.30			26.6	9:10	5.62 A	4.05
	PARAMETER										Ĭ						•		•		un.																		•		=					
	PAG N		50.00 787	96.95	13.72	0	994	92.36	26.67	111	04-47	31.37	33,72		96.66	38.29	38.47	260	44.44	46.48	50.11		217	56.02	58.73		97.79	63.56	62.37		97.6	68.71	68-4)	3	· / · 89	74.76		156	80.0		78.71	346	98.8	85.41	9	3.36
		!	09.64	85,92	13,77	10.00	458	92.30	26.71	349	94-30	32-02	33,79	406	96.54	39,12	38.31	240	96.30	46.41	49.65	ì	922	53.69	55.06	,	200	59.13	58,31	90	97.42	62.60	62.25	1.05	97,63		62.29	179	97.R6	00.20	68.03	171	98.58	72-23		3.31
	60.00		00.04	A5.89	13.83	DA •C I	<b>†</b> §†	92.27	26.73	263	46.24	32.53	33,83	ě		39°73	38,23	256	96.19	4.7.0A	49.52	í	22.40	52.90	53.93	į	052	55.24	55,31	;	97.20	57.72	58.72	202	97.40	60.42	61.4	961	97.62		63.25	161	98.32	05.49	C * * * * * * * * * * * * * * * * * * *	3.25
FGS	225-00 LAMDA =		35.00	85.84	13.93	74.61	447	92.21	26.76	36.	94.17	33.05	33.A6		46.39	39.66	37.54	250	96.49	***9	48,35	;	23.0	10.00	51.97	į	462	51.76	53.00	9	96.86	53,23	55•A2	122	97.06	55.03	57.50	712	97.26	26.14	58.24	215	97.93	57.07	34.34	3.15
B-6		8	30°06	85.79	14.03	******	:	92.89	26.77	754	43.97	30°08	33.54	5.55	96.00	38.03	36.45	276	25.65	43.42	46.17	í	203	45.74	48.56	i	96-19	46.54	49.38	Ş	96.38	47,73	51.43	268	96.54	48.78	52.85	542	96.75	4.64	53.26	245	97.41	49-82	370	3.06
TABLE	ONS RHIN	TAPE NO.	757	85.65	14.18	1	044	91.75	25.36	767	93.50	32,36	31,03	128	94.41	36.06	33.04	111	96.96	38.25	34,38	9	95,27	39,92	35,48	è	95.45	40.41	35.50	60	95.62	<b>*0</b> *83	36-03	500	95,75	41.37	30-15	290	56.65	•	36,12	290	96.57	21.14		2.94
PARAMETE	SUBJECT TO CONDITIONS RMIN #	;	735	85, 15	14.55	! •	436	91-18	24.59	375	92.77	31.00	27.79	24.7	93.53	33.77	2A, A5	314	93.94	35.24	50-62	į	94.25	36.22	54.45	į	17.76	36.62	24.42	i	96	36.57	54.62	324	94.67	36.41	54.43	324	74.82	30.4	20°#	324	95.19	36.89		2.7A
	SURJECT	9	730	84.30	14.47		458	84.49	22.54	01+	69.06	27.71	24.17	258	91.25	26:73	54.96	392	91.65	29.30	25.06	100	91.85	29.43	25.20	606	92-00	29.33	25.22	305	92.10	29.22	52.52	345	92.15	29.23	*2*67	365	17.74	12.62	\$2°\$2	345	92.68	25.20	, , ,	2.44
		:	717	80.38	14.05		497	54.57	19.81	475	85.48	22.55	20.25	474	95.86	22.70	20.36	477	66.99	22.61	20.32	70	46.21	22,55	20,33	•	86.26	25.55	20.34	***	86.34	22.40	50.32	£84	R6.37	22.41	05.00	+8+	10.40	16.30	76.05	484	A6.74	22.45		2.05
			749	66,37	11.10	•	722	6. E	13.79		69.20	11.69	13.72	74.8	69,35	11.62	33.70	751	69.45	11.59	13.69	ŭ	69.46	11.59	13,69	e y	59.51	11.59	13.69	753	69.54	11,57	13.69	153	69,55	11.57	70.5	755	50.5	55.11	13.64	757	69.76	11.55		1.58
	ANDE		ç	PCT.	510.	•	Š	• <u>•</u>	STO.	ç	ČT.	Ħ.	STn.	Č	Ļ	Ę.	ST.	NO.	Ļ	T.		ş	• • • • • • •		STD.	;	; ;	o.	stn.	Ş	Ļ	64	STIS	Ç	בַּי		•	ç	• •	• • •	<b>510</b>	Š	T.	, L	•	• PAU
	PARAMETER ANIME		5.00	_			10.00			15.00				20-00				25.00				6	0000			4	00,456			40.00				45.0n				20.00				LIMIT	ı			

						AVG	)			9	•			•	2				AVG				AVG				Ave	<u>}</u>			274	:			224	•			4	9			,	9 4 6				AVG
	ANJE		11417 532	5.56	97.0		į	18.27	52.	9.07		13	1.10				11.50	_	•	457		55			11.05	11.80 24.60		22	10.19	11.93		421	10.29	11.99		5.5	10.33	2			10.36	2.01			17. 61	2.02	56	6.64 A 2.50
	ETER			10				•	-			-	=				· 🕶			•	•	•			•	~																						
	X PAPAHETER		532	35,56	8,36	6.19	468	38,27	•	9.07	442	39,15	11,10	9,31	424	39.64	11,61	95.5	•	426	44 44 44 44	46.0	•	423	40°09	11.87		422	49.14	11.92	4.57	421	40.19	11,96	<b>9</b>	421	40.22	11.97		12	40.22	11,97	9.56	43.	20.00	11.97	9.56	2,16
		;	532	35,56	30° 50	8.19	466	38.27	10,25	9.07	775	39,15	11,10	9,31	437	39.63	11.63	95.6		475	74.74	0.54	•	423	40 n2	11.00 00.11		422	40.07	11,90	6.57	422	40,12	11,91	16.0	425	40.14	11,92	٧٠.٥	422	40,14	11,92	0,57	733	70.	11,92	9.56	2,11
	90.09		532	35,56	9.79	6.19	468	3A.27	10,25	0.07	742	36,15	11,10	9.31	757	30.61	11.62	4.55	. !	425	70.07	0.54	•	423	20.05	11.85		422	30.96	11.86	9.57	422	30.98	11.87	9.57	472	30.08	11.87	4.27	422	30.08	11,87	4.57	733	20 01	11,47	9.56	2.00
π	, 00 LAMBA:	,	35,00 530	35,55	6.40	8.20	464	38,21	10,32	4.07	446	39,98	11,13	9.31	424	30,40	11.56	50.0		<b>4</b> 26	AD' A7	12.0	•	<b>*</b> 2 <b>*</b>	39,77	11.75		423	39,78	11,78	9.56	169	39.79	11.79	9.56	423	39.80	11,79	9.56	167	39,82	11,79	9.56	•	200	11.79	9.0	1.92
148	22	<b>.</b>	50,00	35,49	6	42.8	467	38.86	10,22	9.01	577	39,92	10.06	9.17	717	39.26	11,33	9,42	. !	107	¥	7 2 4	•	429	30.43	11.72	1	459	39.45	11,52	4,42	429	39.45	11,52	2 .	479	34,45	11,52	4.42	429	39,45	11,52	9,42	907	46.45	11,52	9,42	1.80
TABLE B-	NDITIONS RRIN B	TAPE NO.	25.70	35.36	6,55	22.8	465	37,76	10,17	9.00	648	38,56	10,77	<b>9</b>	7	38.75	11,04	9,18		*	200	9.16	•	438	36.17	11,12		438	38.86	11,12	9,17	400	38.88	11,12	7.17	438	36.38	11,12	4,1/	47.4	38,56	11,12	9.17	94.7	100	11,12	9.17	1,67
Œ	Te CONDITTO	;	20.00 See	35,11	<b>9</b> 0.0	6.20	463	37,18	90.01	4 E.	55.5	37.73	10,52	6,92	445	17.96	10.69	80° 0		7 .	70.05	6.62	•	+45	40 ' BA	72.77	•	445	36,96	10.69	20.0	446	33.06	12,69	2.5	446	34,06	13,69	70.0	444	38.36	10,69	9.62	***	0 d	54 E	9.05	1,53
	Subject 1	;	15,16 500	34,30	E	5112	466	35, 96	34.0	E, 77	456	34.75	2 <b>6</b> 6	ر د ، ع	454	36.36	9,	8.84	. 1	456	70.00		•	459	36.43			460	26,44	50°0	м) 8. «	460	36,44	£0.0	5 t . t	160	36,44	56,4	, a	, <b>44</b>	36.44	56.0	Ω α . α .	,,,,,	104	55.6	3, r • K	1.32
		;	17,00	31. P.	90	0 • •	451	32,79	9,11	5 × 4	949	94. 27	0,21	, S.	45.7	4 1 1 1	0	F.54		459	7 600		•	454	9 T T T	0 1	) L	454	33,18	0.0	α 4,	9.0	B 4 . E	9.	a.	40.4	53,10	90.0	40,	7	10 4 4 15	0	и 4.	4	X * E *	9.0	a, n	\$ E.
			را ا ا		_	F4	_	23,90	e.	-1	_	23,97	-	6,11	424	24.61	7	96° B		n e		) C		~	•	50.0	,	454	24,51	400	dr C. Mi	*2*	24.01	7.99	ه. د د	454	24,01	56.7	r α	767	24.01	5u 2	de la	Ç		50° Z	gs e ct,	m) d r
	AUCDA		9,	PCT.	· La	SID.	œ.	PCT,	Ε.T.,	510.	a	۲. در	ET.	sta.	9	 	בין.	STD.			֓֞֞֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֓֡֓֡֓	- L	<b>.</b>	Уe.	, c.t.		n n	.89	PCT.	11:		ď	PCT.	i i	۲1 ت.	ď	PCT.	4		9	D L	1	ATB.			; ; ;	410.	4 W 2 .
	PARAHETER ANJOR	;	5,00	•			10.00				15.00				20.00	9				25.00				30.00				35.00	•			10 07				45.00				ה ה	3							

							•				AVG				Ave	•			,	9 ^ 6				AVB				Ave	!			974	:				9 × 6				AVG				AVG				AVG	
	ER AWJF		418	19.32	5.79			21.16	7.22	7.14	-	352	21.79	7.70	4 62 4		22.13	7.97			22 44		7.54	-	347	22.43	7.55		-	22.48	6.			22.54	8.31			22.55	9.12	7.54		349	R. 4	7 8 6		349	22.76	7.55	4.90 A	3.24
	X PARAMETER	6	2.4	19,32	5.79	6.23	347	21.16	7.52	7.14	ł	352	21.79	9,0	63.7	348	22,13	7.97	*5*/	344	22 44	100	7.54	-	347	54.55	7.55	•	348	27.48	C .	***	348	22.54	A.11	7.54	2	22,55	8.12	7.54	ļ	349				349	27.74	7.55	•	3,14
		4	A 4	19,32	5.79	6,23	36.7	21.16	7.22	7,14		352	21.79			346	27,13	7.07	*	345	22 11		7,54		347	27.43	7.55	•	348	27.48	e. 1		348	22.54	B. 11	7.54		27.00	P.12	7.54	;	349			•	349	27.74	7.53 5.53	•	1,14
:	95.29		418	10.32	5.79	6,23	367	21,16	7.22	7.14	,	352	21.79	20,0	2.	348	22.13	7.97	***	445	22 34		7.54	!	347	27.43	7.55		348	22.48	e .	1.34	348	22.54	7.7.	7.54	;	22.55	1.12	7.54	•	349	A	7 2	•	349	22.74	7.55	•	3.14
SFF TAIL	LAMBA =	6	4.00	19,32	5.79	6.23	367	21.16	7.22	7.14		352	21.79	7.7	65.	348	22,13	7.97	*0.	144	22 44	90.0	7,54	;	347	22.43	7.55		348	22.48	e 1	1.54	348	22,54	P.11	7.54	•	22.55	21.4	7.54		349	R. 11	7 54	0	340	22.74	7.55		7.14
M		.15	417	19,31	5,60	6.24	365	21.13	7.25	7,15		349	61.7	10.7	2	347	22,10	7,98	26.	346	20.00	70.1	7,54	!	347	50.00	7.54	•	348	22.45	80 s	***	348	22.51	9.10	7.54	078	22.52	11.	¥5.	;	349 52 53	1 4 G	7 56		344	22.71	7,53		71° ••• •••
TABLE B-		TAPE NB.	415	19,29	5,82	6,24	364	21,11	7.27	7,15	;	9,0	7.17	7.05		347	22.07	7.97	25.	346	22.24	8.75	7,54	;	347	26,30	7.54		548	22,42	F. 07	**	346	22,47	6 C * 60	7,53	372	22.4B	60.4	7.53	,	5 5 C C	900			345	77.57	7.54		3,12
		5	415	19,26	5,81	6,24	364	21.04	7,24	7,15	•	10 y C	7,03	7.23		347	21,99	7,04	20.	346	22,15	50.6	7,53	,	347	02',7	7.52		345	22,31	7 C	)· )	RY E	22,35	η. 2.	7.52	4.0	27,36	£: £:	2.52	;	345	7	7		340	M3 + 10 10 10 10 10 10 10 10 10 10 10 10 10	7.52	•	₩3  -  -
	* COURT	7.00	<b>414</b>	19,43	5,76	6,25	363	20,73	7,16	7,13	;	24.0	7,136	7.20		348	21,60	7,78	454	347	21.72	7,84	7.49	,	7	7.1.7	7,47		350	21.47	M . W		352	21,50	7.04	7.47	3	71.63	7.44	7,47	i.	رد ا	7.46	7	•	35.	رد در در در در	7.48		7,16
		000	395	18,00	5.71	6.25	349	10,47	66.9	7,00	į	200	2,00	7	•	336	24,21	7.54	100,	918	22.27	7.56	7,21	į	D . C	7	7.20		434	36 1 M) 1	<b>1</b> 1	174	339	2.41	1.54	7.20	73.0	25.75	7.55	3.7.	:	3 4 V W)	, u, r	7 20		455	N. 1	37.	•	7.
		0D. 2	311	12,14	4,89	99.9	376	13,19	5,40	6,31	;	3 P P	200	10		317	13,56	40.0		317	17.54	5,35	6 F.A.				100	•	少いか	13,40	4,14	J	326	14,51	5,33	ų.	::	14	5,43	T t t		.) + (\)	1 M		1	375	12,47	4	•	£: " \
	AWJDF			₽CT.	rī.	, iii		PCT.	ET.	, ale			, ,	, al c									ığı.							٠ د ا	1	•				נו נו			, L.	בוני.		٠ ١ ١		6	•	r,	():		•	*. 5.**
	494MPTER		5.00				10.01				40	12.00				26.00				25.00	•				30.00				35,00				40.00				5				£	34.E				1417				

				T	HATERAC	200		•			
TOTAL ESTERA			SubuEnt	w.	ir in	522	G LAMBA =	90° 40		X PARAMETI	ER AWJE
					TAPE NB.	+		;			•
	20	19,00	15.70	27,00	25.90	00.0	35,00	Du . u4	45.50		11811
5. 00 C	753	357	9.	967	917	9 7 8	900		7 7 7 7	•	A4. 12
	יים היים ביני	* * * * * * * * * * * * * * * * * * * *	10 10 10	N * * * * * * * * * * * * * * * * * * *	10 87	12.77	12.60	10.57	12,55	•	12.55
- L	50	94.81	ν α * ε <b>τ</b>	14.92	13.96	13.96	13,92	13.92	13.91	13,91	13.91
		•	•	  - 	!	•	,	į	į	į	4.47 AVE
10.00 .5.	7.8	:3 []	5.7	495	497	495	494	498	\$ a c	4 T	200
[2]	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	4 1	7, 7,	7.70	00.00	12.12 12.12	2.10	74.14 CG FC	22.76	22.76	22.67
	,	r		24 32	21 56	24 73	24 80		21.00	21.90	21.90
	* : • · · ·	7	·	7.17			40.13			•	4.91 AVG
15.00 %.		475	426	398	356	372	368	369	377	377	379
PCT.	52.45	27.70	25.49	91.50	93,10	97,76	94.03	94,13	94,19	94,19	94.21
٠ ١		20.62	6 C C	24.42	30,22	5. 1. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	32.92	31.70	21.71	10,15	11.13
415		T4 - L3	62.13	0.4.	27.62	ני. ני	31.61	31.63	3115		5.09 AVG
20 00 00	151	4.5.3	9.4	375	345	324	310	364	310	311	313
	59.74	1 N N N	91.10	44.70	16,39	94.96	95,32	95.49	95.58	95.59	95.61
	9 6	0,00	27,16	31.19	33, 82	34.72	38.53	39.36	34.43	38.51	38.27
417	51 71	13,76	23.46	37.77	33,26	34,09	35.17	35.20	35,27	67.78	35.29
		,	•	:	į		•	346	26.7	346	2.65 AVG
25.06 \@.	156	404	on market and the second secon	300	27.	0 to	4/3	64.27	0 Y Y O	14.95	96.45
	# H C	* * * * * * * * * * * * * * * * * * *	46. 61	10 E C 2	17.75		F 0 - 1	45.52	45.24	45.41	45.09
- r - L - U	0	\$1.5 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	25.06	31.74	36.11	37,70	45,57	40.75	40.79	40.79	40.81
• :			,	•							5.37 AVE
30.60 \0.		154		347	(H )	271	250	239	241	239	239
		7, 90	•	69*26	95.15	ð. 14	96.52	96.77	46.04		90.74
111	<b>4</b> 0	B. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	27.41	(H)	59.16	14.4	46.58 50.58	47.87	47 AB	E	47.88
. 1 . 7		on • • • •	r		•	77.		•	•	) •	5.47 AVG
35.00 .0.	745	ياحر	410	341	292	247	220	206	203	200	196
		04.16	φ. υ.	63.63	95.56	9.4.	96.91	97.19			76.24
1- 1 3 1	+4 t	D in	27.41	34,55	40.4	4 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	37,44	54.12	56.56	0 1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	54.61
٠,٠		1	0	0	301/5	7	7. 100				5.57 AVG
46.00 %.	247	1,0	4:7	342	244	237	297	193	187	193	
	57.53	25.23	91.19	97.19	45.67	96. AI	97,14	97,43	97.46	97,79	97.93
۲,	5. 75	61.70	27.37	34.47	42,21		13.00 10.00	63.25	65.45	9.40	76.74
	17,34	14,33	D	14.55	37.42	Cc	13.00	5.0	, I p	1	5.65 AVG
0. 96 24	745		7.5.7	342	279	528	195	160	174	149	
. E.Ga	55,54	66.23	51.12	54.13	65.77	24,38	97,28	97.57	97.42	57.04	98.12
, L.4	52.5	7	27.48	(4°4)	W	57.92	62.51	67.42	711.44 64 44	20.77	65.37
:	17. VC		٠, ٢	1		?				•	5.69 AVG
50.00 AB.	144		<b>6.</b> 6	342	277	221	186	149	159	152	146
p. 1.3.	50.57	45.30		54.20	95.35	94,93	97.49		4 c c c c c c c c c c c c c c c c c c c	ar c	98.40
i		.,	27,35	46.54	4 6 6 4	, 4 , 4	67.75 F. A. R. F.	00 14	66.77	67.93	76.36
.: .: 		<b>3</b> , • c. 1		10.75	7,*,6	•	/ L				5.75 AVG
1.11		2,5	5 <b>. y</b>	343	<u>.</u>	219	176		12		#
		54.55	ţ.	٧	*.	97.55	96.22		P 1	, ,	26.66
,	27.6	22.13	27, 48	4 to 10 to 1	4 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	55.3	64.63	60,23	70.72	47.44	798.41
•		•	1	١.	•	•			•		6.35 AVG
٠. الم	A ê	2.0	2, t6	14.5	7.91	7,11	3.26	1,38	14,51	3,59	4.16
	:r : r : u : .										

B-25

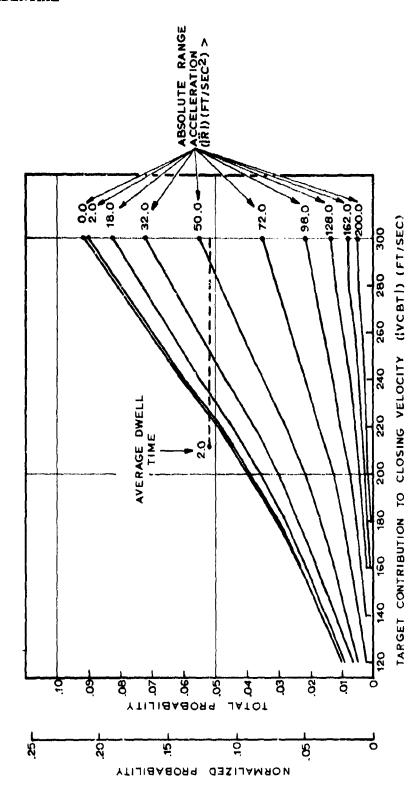
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# 4. Clutter Track Through Requirements

(C) As with the tracking study, the figure given in this section will be for the forward  $\pm60^\circ$  coverage and for the full sphere coverage. The rearward  $\pm60^\circ$  coverage and the necessary source data are contained in Section 3 of Appendix B.

## a. Pulse Doppler Main Beam Clutter (PDMBC)

- (C) Figure B-10 represents the probability of occurrence of the target signal within the PDMBC notch and the range acceleration greater than the indicated value as a function of this notch width. The top most curve labelled "0.0" for range acceleration thus contains all occurrences of the target signal entering the PDMBC notch. This curve therefore gives the probability of the target being within PDMBC notch as a function of the notch width. Using a typical value for notch width in present AI radars (±200 ft/sec), it can be seen that for AI radar coverage, the probability that the target return is within the notch is 0.09 for an average duration of 1.8 seconds. For full sphere coverage (Fig. 17) the probability that the target is within the notch is 0.35 for an average duration of 6.5 seconds. The same interpretation holds for all the graphs from the "Clutter Track Through Requirements" portion of this report (Fig. 16, 39).
- (U) Knowing the distribution of the clutter and knowing the average dwell time, the probabilities that the radar can track through this clutter may now be determined. The ability to track through this clutter is highly dependent upon the accelerations experienced during loss of signal. An acceleration over a long period of time, would prevent the radar from coasting through the clutter. This happens because the "memory" for coast through is an extrapolation of the last known velocity. Thus a change in velocity over a period of time would invalidate this extrapolation. The maximum acceleration/time combination a radar can handle depends on the particular radar in question. For that reason, the summary of the data presented herein will show the 0.05 probability that a given acceleration was exceeded while in the clutter and the associated average duration it was exceeded.
- i. Range acceleration (Fig. B-10, AI coverage; Fig. B-11, Full coverage.)
- (C) In the case of AI radar coverage, the range acceleration exceeded 50 ft/sec<sup>2</sup> while in PDMBC 5% of the time in gimbal limits for a duration of 1.5 seconds.
- (C) In the case of full coverage, the range acceleration exceeded 180 ft/sec<sup>2</sup> while in PDMBC 5% of the total time for an average duration of 1.2 seconds.



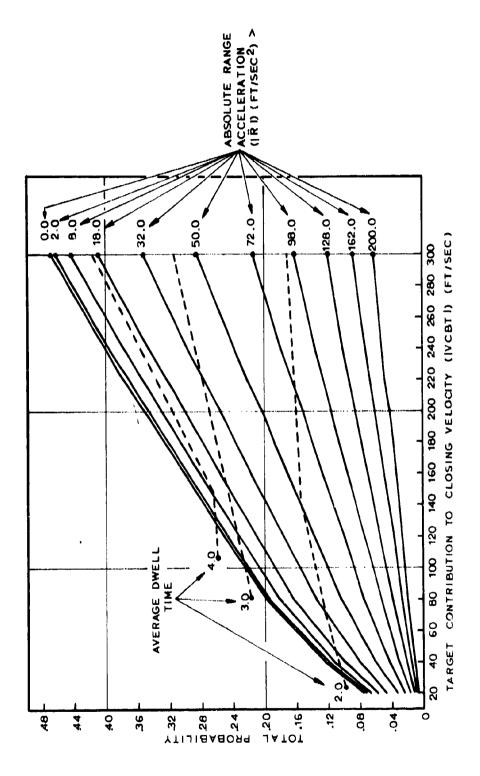
CUMULATIVE PROBABILITY DISTRIBUTION OF TARGET CONTRIBUTION TO CLOSING VELOCITY FOR SEVERAL VALUES OF RANGE ACCELERATION FOR AI RADAR COVERAGE AND MINIMUM RANGE - 225 FT FIG. B-10 -

- ii. Azimuth line of sight acceleration (Fig. B-12,
  AI coverage; Fig. B-13, full coverage.)
- (C) In the case of AI radar coverage, the azimuth line of sight acceleration exceeded 0.30/sec<sup>2</sup> while in PDMBC 5% of the time target was in gimbal limits for an average duration of 1.2 seconds.
- (C) In the case of full sphere coverage, the azimuth line of sight acceleration exceeded 4.9°/sec<sup>2</sup> while in PDMBC 5% of the time the target was in gimbal limits for an average duration of 1.5 seconds.
- iii. Elevation line of sight acceleration (Fig. B-14, AI coverage; Fig. B-15, Full coverage.)
- (C) In the case of the AI radar coverage, the elevation line of sight acceleration exceeded 0.250/sec<sup>2</sup> while in PDMBC 5% of the time the target was in gimbal limits for an average duration of 1.1 seconds.
- (C) In the case of total coverage, the elevation line of sight acceleration exceeded  $4.9^{\circ}/\text{sec}^2$  while in PDMBC 5% of the time the target was in gimbal limits for an average duration of 1.3 seconds.

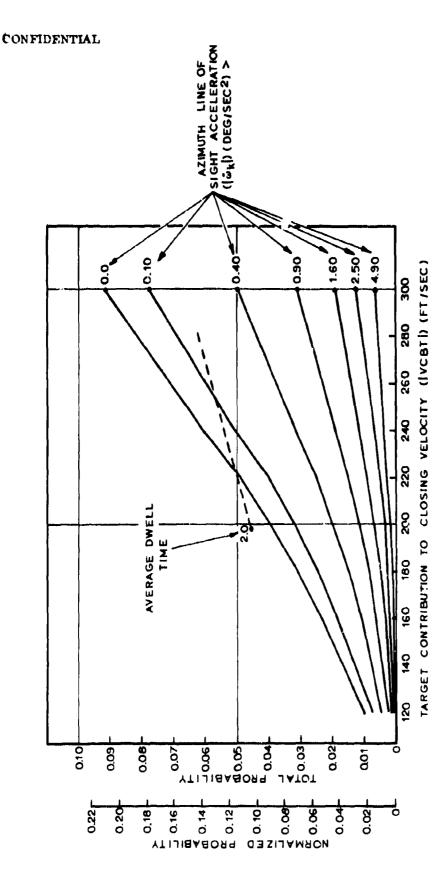
# b. Pulse Doppler fo Notch

- (C) For this study, the  $f_{\rm O}$  notch is shown as a notch of varying widths to account for the difference in notch width among the present AI radars. The notch width used in this report is 150 ft/sec. By use of the graphs and tables, other size notches may be examined.
- (C) The top line on each graph shows the probability that the target is in  $f_0$  notch as a function of the notch width. Using a notch width of 150 ft/sec. it can be seen that, in the case of the AI radar coverage (Fig. 22) the probability that the target is in the  $f_0$  notch is 0.235 for an average duration of 3.8 seconds.
- i. Range acceleration (Fig. B-16, AI coverage; Fig. B-17, Full coverage.)
- (C) In the case of the AI radar coverage, the range acceleration exceeded 38 ft/sec $^2$  while in  $f_o$  notch 5% of the time the target was in gimbal limits for an average duration of 1.6 seconds.

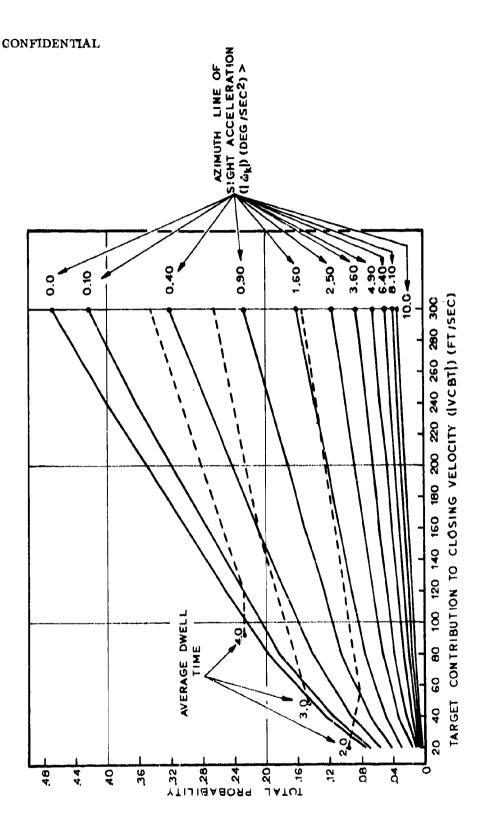
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CUMULATIVE PROBABILITY DISTRIBUTION OF TARGET CONTRIBUTION TO CLOSING VELOCITY FOR SEVERAL VALUES OF RANGE ACCELERATION FOR FULL SPHERE COVERAGE AND MINIMUM RANGE - 225 FT ŀ FIG. B-11

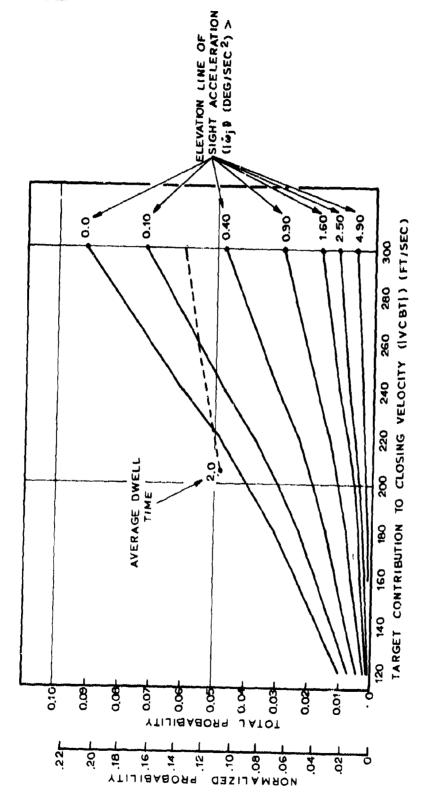


CUMULATIVE PROBABILITY DISTRIBUTION OF TARGET CONTRIBUTION TO CLOSING VELOCITY FOR SEVERAL VALUES OF AZIMUTH LINE OF SIGHT ACCELERATION FOR AI RADAR COVERAGE AND MINIMUM RANGE - 225FT ì FIG. B-12

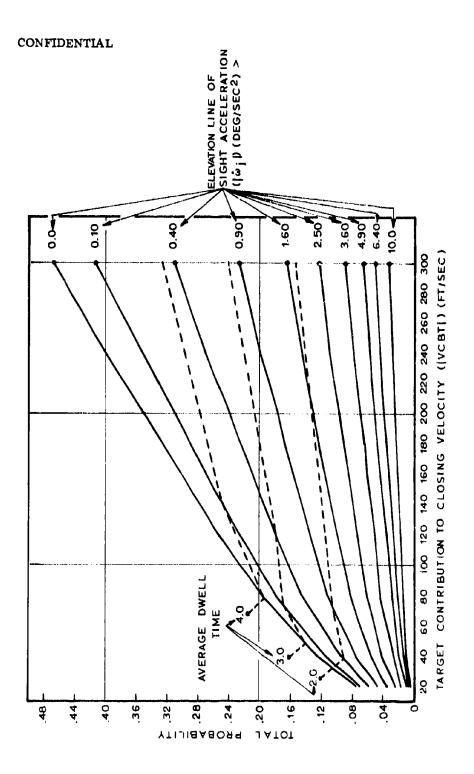


CUMULATIVE PROBABILLITY DISTRIBUTION OF TARGET CONTRIBUTION TO CLOSING VELOCITY FOR SEVERAL VALUES OF AZIMUTH LINE OF SIGKT ACCELERATION FOR FULL SPHERE COYERAGE AND MINIMUM RANGE = 225 FT FIG. B-13 -

Marine State Property

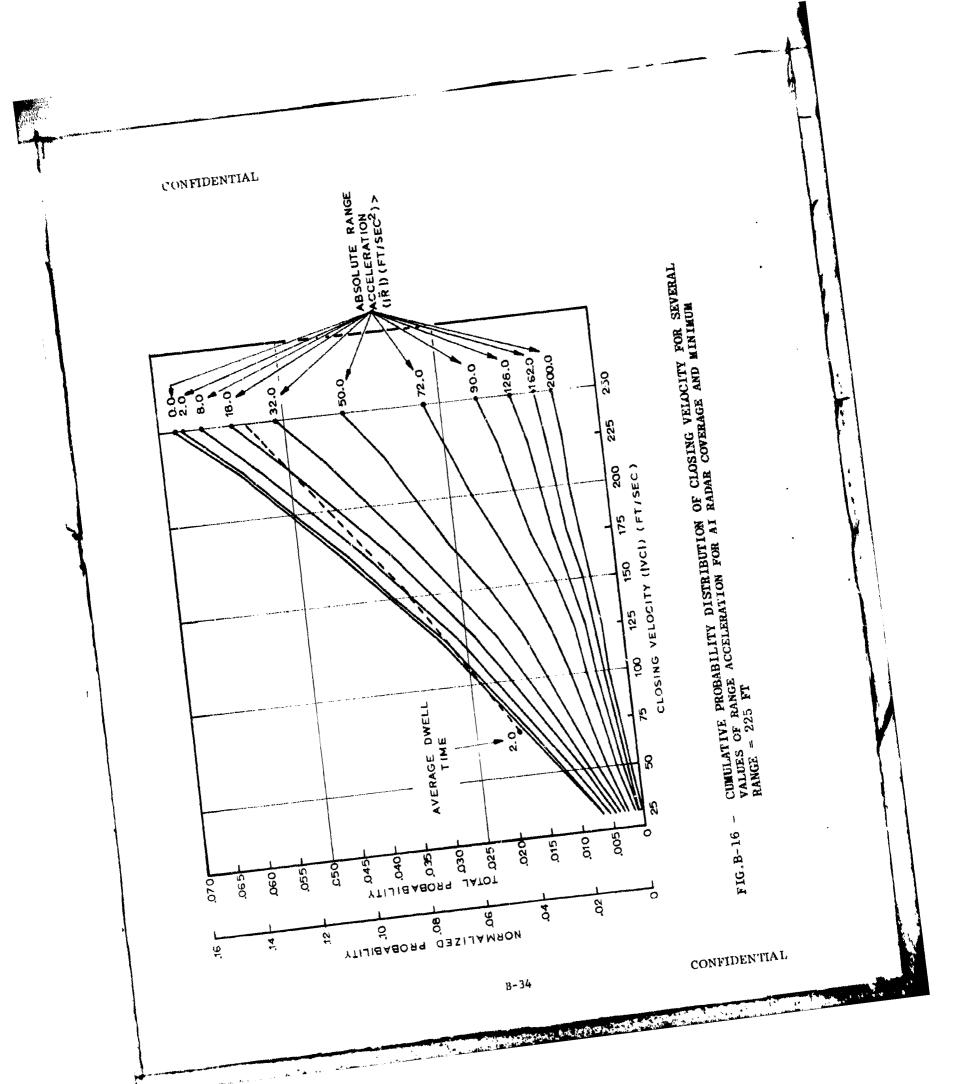


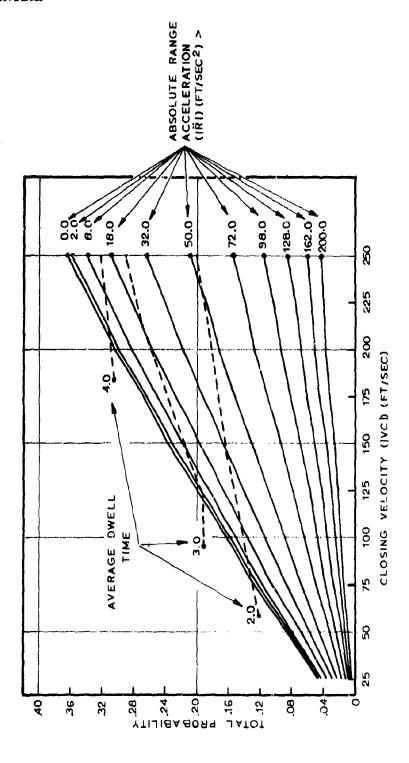
CUMULATIVE PROBABILITY DISTRIBUTION OF TARGET CONTRIBUTION TO CLOSING VELOCITY FOR SEVERAL VALUES OF ELEVATION LINE OF SIGHT ACCELERATION FOR AI RADAR COVERAGE AND MINIMUM RANGE = 225 FT FIG. B-14 -



CUMULATIVE PROBABILITY DISTRIBUTION OF TARGET CONTRIBUTION TO CLOSING VELOCITY FOR SEVERAL VALUES OF ELEVATION LINE OF SIGHT ACCELERATION FOR FULL SPHERE COVERAGE AND MINIMUM RANGE = 225 FT ı FIG.B-15

B = 33



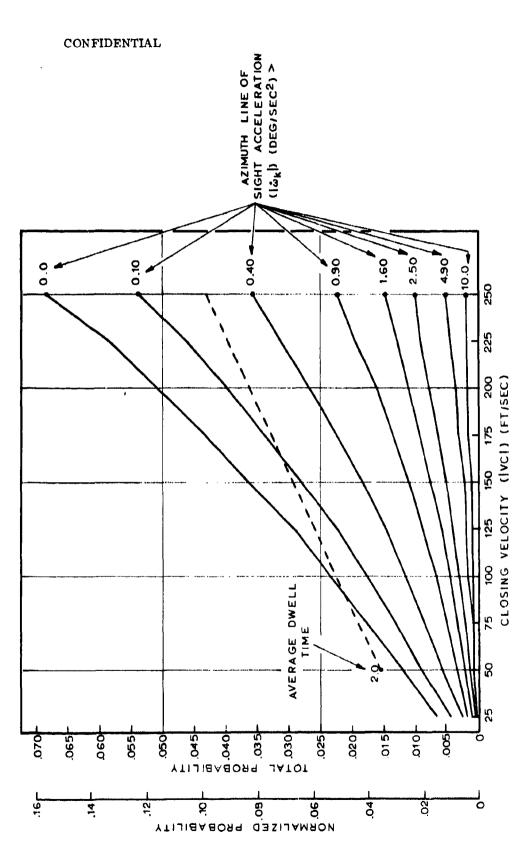


CUMULATIVE FROBABILITY DISTRIBUTION OF CLOSING VELOCITY FOR SEVERAL VALUES OF RANGE ACCELERATION FOR FULL SPHERE COVERAGE AND MINIMUM RANGE = 225 FT FIG. B-17 -

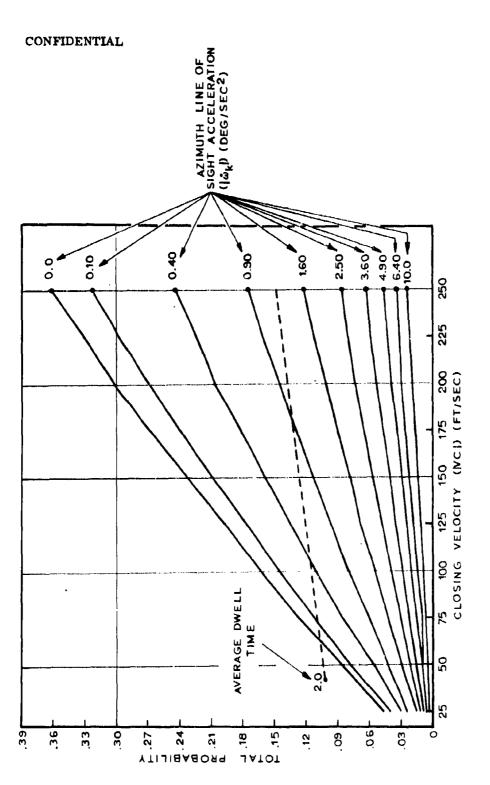
- (C) In the case of full coverage, the range acceleration exceeded 128 ft/sec<sup>2</sup> while in fo notch of 5% of the total time for an average duration of 1.2 seconds.
- ii. Azimuth line of sight acceleration (Fig. B-18, AI coverage; Fig. B-19, Full coverage.)
- (C) In the case of the AI radar coverage, the azimuth line of sight acceleration exceeded  $0.3^{\circ}/\text{sec}^2$  while in  $f_{\circ}$  notch 5% of time target was in gimbal limits for an average duration of 1.5 seconds.
- iii. Elevations line of sight acceleration (Fig. B-20, AI coverage; Fig. B-21, Full coverage.)
- (C) In the case of AI radar coverage, the elevations line of sight acceleration exceeded .3 $^{\rm O}/{\rm sec^2}$  while in founcth 5% of the time the target was in gimbal limits for an average duration of 1.7 seconds.
- (C) In the case of full coverage, the elevations line of sight acceleration exceeded  $3^{\circ}/\sec^2$  while in  $f_0$  notch 5% of the total time for an average duration of 1.3 seconds.

## c. Pulse Main Beam Clutter (PMBC)

- (C) For analysis in this section, the range gate width is taken as 300 ft. This means that PMBC is defined as occurring if the target is within 300 ft. of the leading edge of the ground return.
- (C) For AI radar coverage, the probability that the target is in PMBC is .005 for an average duration of 1.12 seconds. In terms of normalized probability (normalized to the AI radar coverage), the probability of the target in PMBC is .0117. This probability is less than the .05 criterion used in the previous analyses.
- (C) For full sphere coverage, the probability of the target being in PMBC is again less than the 0.05 criterion, that is, 0.015 for an average duration of 1.31 seconds.
- (C) Analysis of the tracking accelerations for PMBC in the same manner as the PDMBC and  $f_{\rm O}$  notch is not possible. Analysis using a more stringent criterion could be made. In order to keep the comparison on pulse and pulse doppler clutter on the same level, the PMBC tracking accelerations evaluated with the 5% criteria are zero. The application of  $\epsilon$  more stringent criterion is left up to the reader and, for that purpose, the graphs of the accelerations are given in Figs. B-22 through B-27.

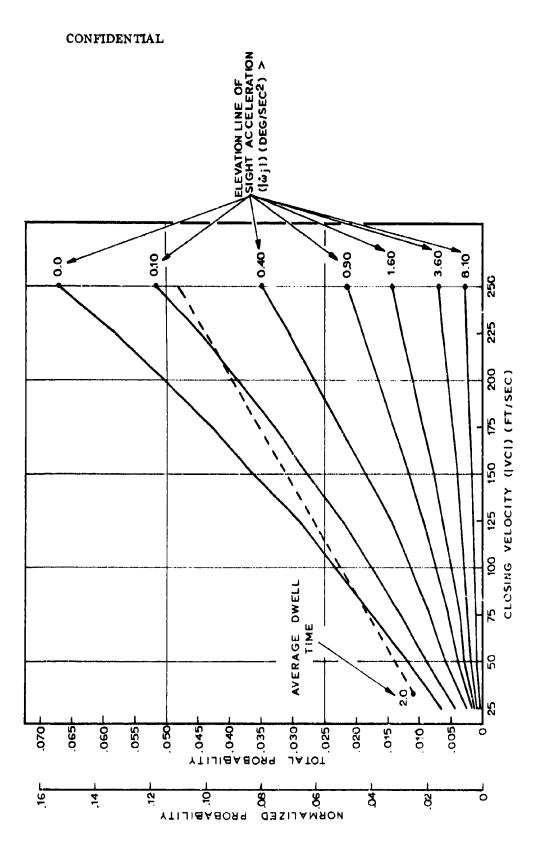


CUMULATIVE PROBABILITY DISTRIBUTION OF CLOSING VELOCITY FOR SEVERAL VALUES OF AZIMUTH LINE OF SIGHT ACCELERATION FOR AI RADAR COVERAGE AND MINIMUM RANGE - 225FT FIG. B-18 -

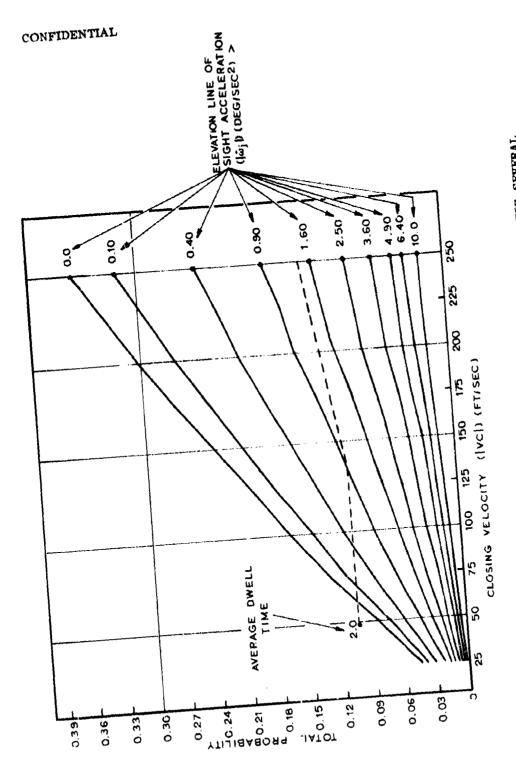


CUMULATIVE PROBABILITY DISTRIBUTION OF CLOSING VELOCITY FOR SEVERAL VALUES OF AZIMUTH LINE OF SIGHT ACCELERATION FOR FULL SPHERE COVERAGE AND MINIMUM RANGE - 225 FT FIG. B-19-

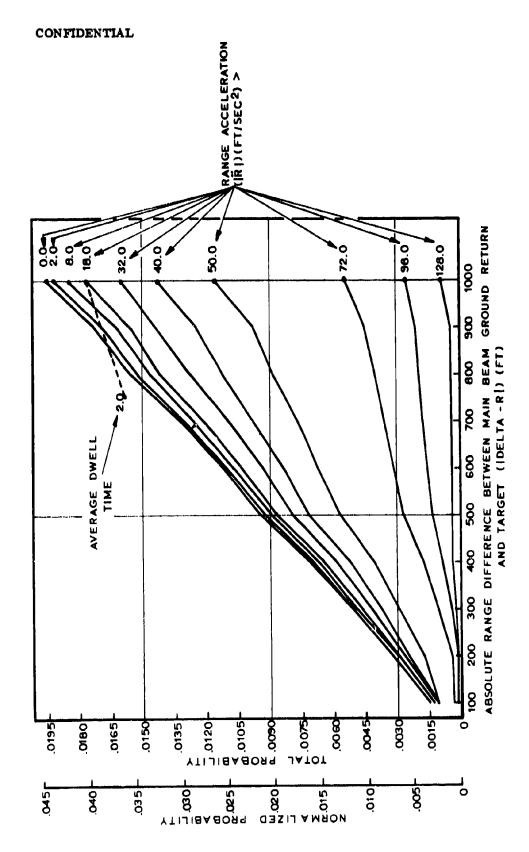
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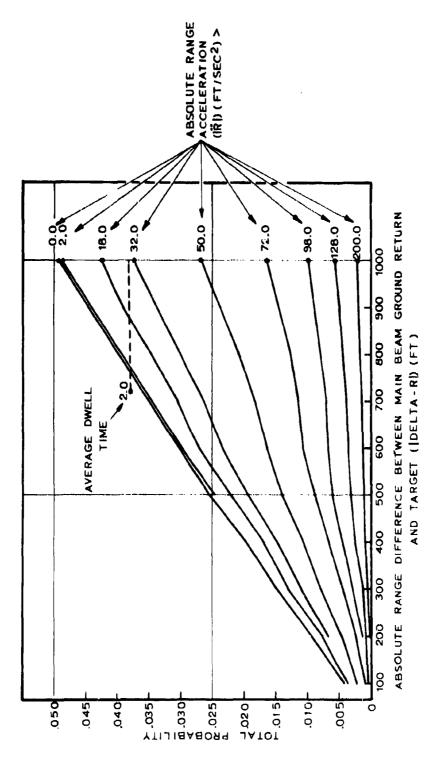
CUMULATIVE PROBABILITY DISTRIBUTION OF CLOSING VELOCITY FOR SKVERAL VALUES OF ELEVATION LINE OF SIGHT ACCELERATION FOR AI RADAR COVERAGE AND MINIMUM RANGE = 225 FT FIG, B-20 -



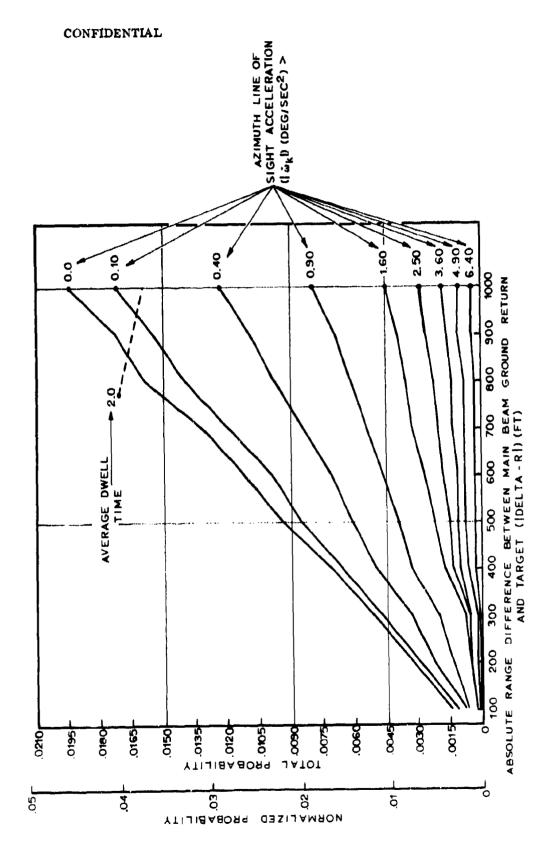
CUMULATIVE PROBABILITY DISTRIBUTION OF CLOSING VELOCITY FOR SEVERAL VALUES OF RIEVATION LINE OF SIGHT ACCELERATION FOR FULL SPHERE COVERAGE AND MINIMUM RANGE = 225 FT FIG. B-21-



CUMULATIVE PROBABILITY DISTRIBUTION OF RANGE DIFFERENCE BETWERN MAIN BEAN GROUND RETURN AND TARGET FOR SEVERAL VALUES OF RANGE ACCELERATION FOR AI RADAR COVERAGE AND MINIMUM RANGE = 225 FT FIG. B-22 -



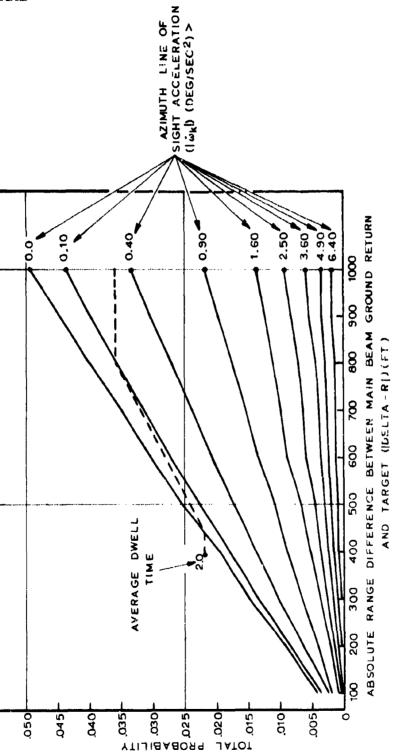
BEAN GROUND RETURN AND TARGET FOR SEVERAL VALUES OF RANGE ACCELERATION FOR FULL SPHERE COVERAGE AND MINIMUM RANGE = 225 FT CUMULATIVE PROBABILITY DISTRIBUTION OF RANGE DIFFERENCE BETWEEN MAIN FIG.B-23 -



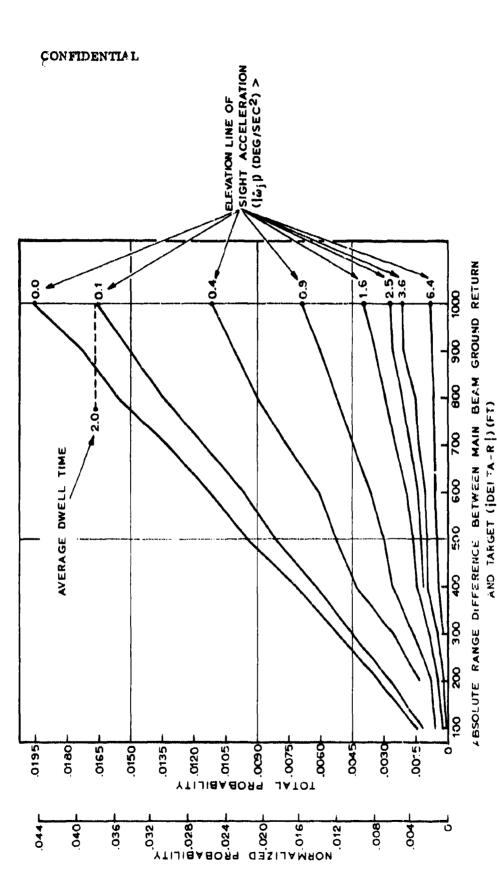
CUMULATIVE PROBABILITY DISTRIBUTION OF RANGE DIFFERENCE BETWEEN MAIN BEAM GROUND RETURN AND TARGET FOR SEVERAL VALUES OF AZIMUTH LINE OF SIGHT ACCELERATION FOR AI RADAR COVERAGE AND MINIMUM RANGE = 225 FT ì FIG.B-24

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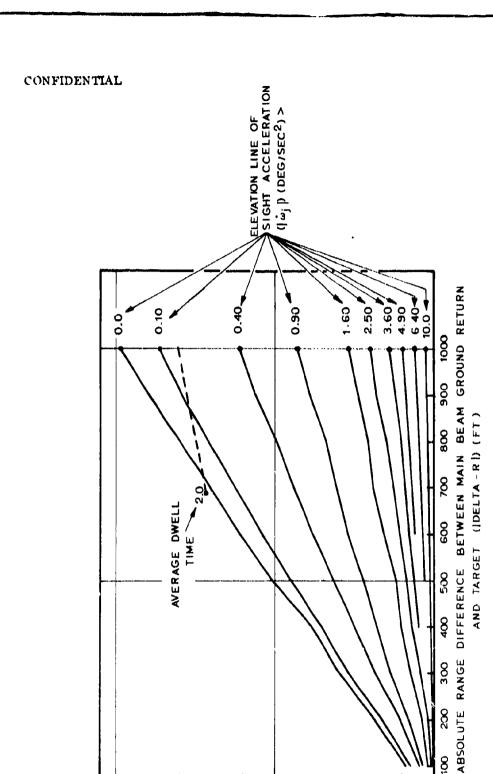




BEAM GROUND RETURN AND TARGET FOR SEVERAL VALUES OF AZIMUTH LINE OF SIGHT ACCELERATION FOR FULL SPHERE COVERAGE AND MINIMUM RANGE - 225 FT CUMULATIVE PROBABILITY DISTRIBUTION OF RANGE DIFFERENCE BETWEEN MAIN FIG. B-25 -



CUMULATIVE PROBABILITY DISTRIBUTION OF RANGE DIFFERENCE BETWEEN WAIN BEAM GROUND RETURN AND TARGET FOR SEVERAL VALUES OF ELEVATION LINE OF SIGHT ACCELERATION FOR AI RADAR COVERAGE AND MINIMUM RANGE = 225 FT FIG. B-26



CUMULATIVE PROBABILITY DISTRIBUTION OF RANGE DIFFERENCE BETWEEN MAIN BEAM GROUND RETURN AND TARGET FOR SEVERAL VALUES OF ELEVATION LINE OF SIGHT ACCELERATION FOR FULL SPHERE COVERAGE AND MINIMUM RANGE = 225 FT FIG. B-27-

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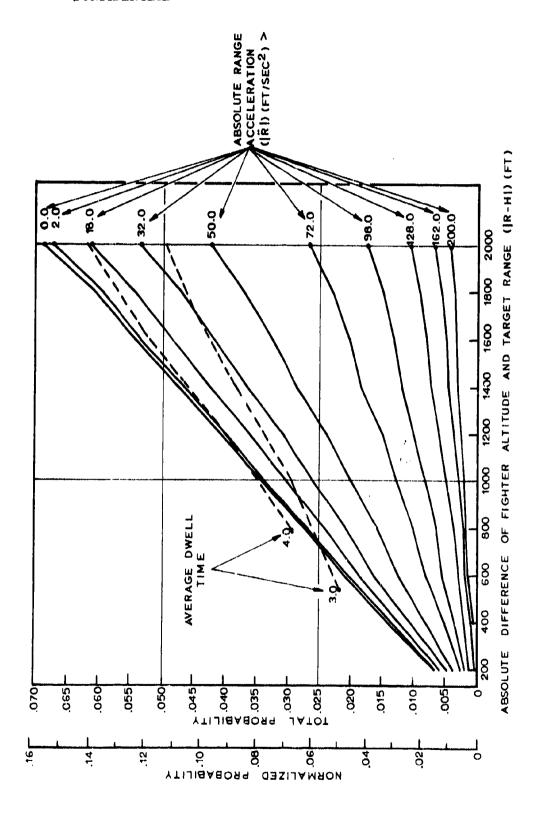
0.40

### d. Pulse Altitude Line (PAL)

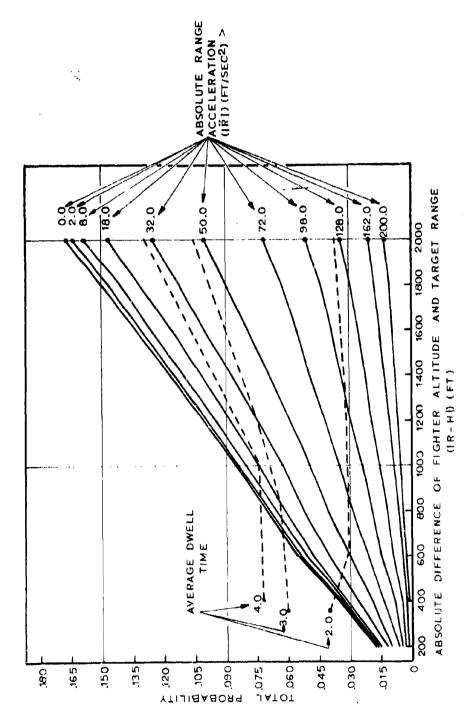
- (C) For the purpose of this discussion, the PAL will be taken as having a width of 11000 ft, which is typical of the clutter return from the ground below the aircraft. This 1000 ft. altitude return further assumes that the strength of the target return is less than the altitude return. The width and strength of the altitude return is dependent upon the altitude of the fighter, the antenna pattern, the look down angle, and the ground reflectivity. For a given width of the altitudes return calculated by the preceding parameters Fig. B-28 through B-33 are still valid and can be used to calculate the track through capability of a particular radar.
- (C) For AI radar coverage, the probability that the target is in PAL is 0.078 for an average duration of 3.9 seconds.
- (C) For full coverage, the probability that the target is in PAL is 0.086 for an average duration of 4.8 seconds.
- i. Range Acceleration (Fig. B-28, AI coverage;
  Fig. B-29, Full Coverage.)
- (C) In the case of AI radar coverage, the range acceleration exceeded 40 ft/sec<sup>2</sup> while in PAL, 5% of the time the target was in gimbal limits for an average duration of 2.4 seconds.
- (C) In the case of full coverage, the range accelerations exceeded 50 ft/sec $^2$  while in PAL, 5% of the total time for an average duration of 2.4 seconds.
- ii. Azimuth Line of sight Acceleration (Fig. B-30, Al coverage, Fig. B-31, Full Coverage.)
- (C) In the case of AI radar coverage, the azimuth line of sight acceleration exceeded  $.4^{\circ}/\text{sec}^2$  while in PAL, 5% of the time the target was in gimbal limits for an average duration of 2.8 seconds.
- (C) In the full coverage case, the azimuth line of sight acceleration exceeded  $0.65^{\circ}/\text{sec}^2$  while in PAL, 5% of the total time for an average duration of 2.3 seconds.
- iii. Elevation Line of Sight Acceleration (Fig. B-32. AI coverage; Fig. B-33, Full Coverage.)
- (C) In the case of AI radar coverage, the elevation line of sight acceleration exceeds 0.350/sec<sup>2</sup> while in PAL,

5% of the time the target was in gimbal limits for an average duration of 2.5 seconds.

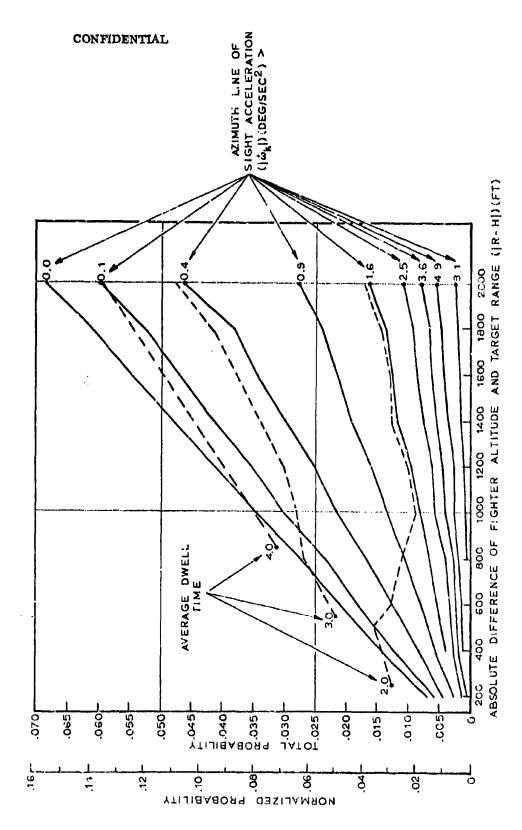
(C) In the full coverage case, the elevation line of sight acceleration exceeded 0.70/sec<sup>2</sup> while in PAL, 5% of the total time for an average duration of 2.4 seconds.



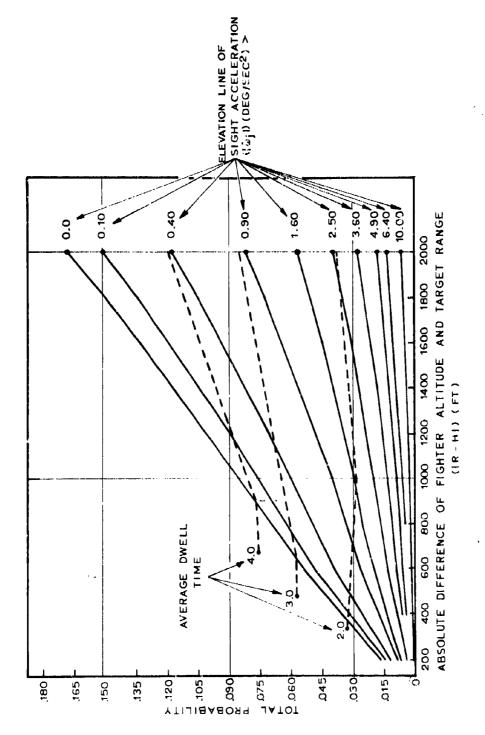
CUMULATIVE PROBABILITY DISTRIBUTION OF DIFFERENCE OF FIGHTER ALTITUDE AND TARGET RANGE FOR SEVERAL VALUES OF RANGE ACCELERATION FOR AI RADAR COVERAGE AND MINIMUM RANGE ~ 225 FT FIG. B-28 -



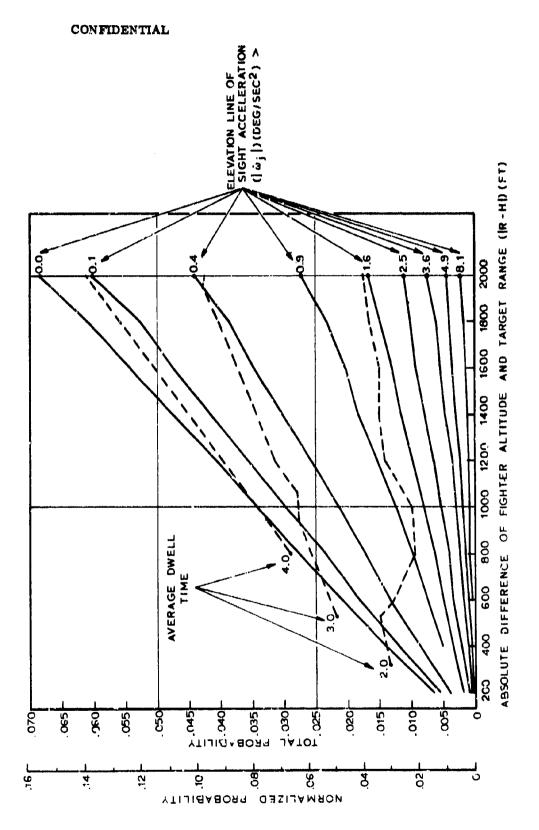
CUMULATIVE PROBABILITY DISTRIBUTION OF DIFFERENCE OF FIGHTER ALTITUDE AND TARGET RANGE FOR SEVERAL VALUES OF RANGE ACCELERATION FOR FULL 225 FT SPHERE COVERAGE AND MINIMUM RANGE -Fac. B-29 -



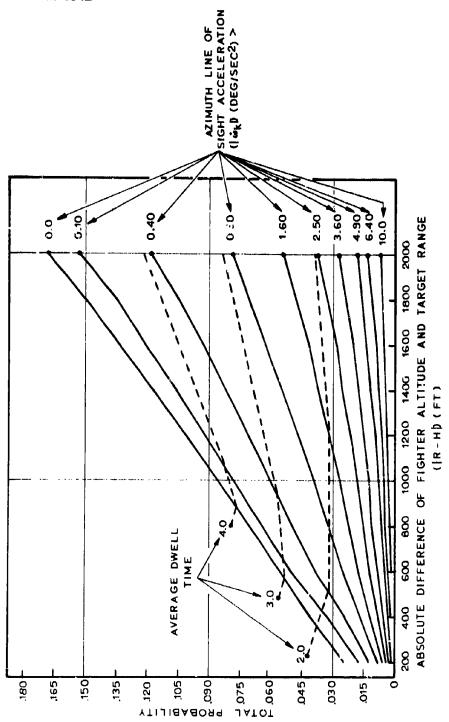
CUBULATIVE PROBABILITY DISTRIBUTION OF ABSOLUTE DIFFERENCE OF FIGHTER ALTITUDE AND TARGET RANGE FOR SEVERAL VALUES OF AZIMUTH LINE OF SIGHT ACCELERATION FOR AI RADAR COVERAGE AND MINIMUM RANGE - 225 FT FIG.B-30 -



CUMULATIVE PROBABILITY DISTRIBUTION OF DIFFERENCE OF FIGHTER ALTITUDE AND TARGET RANGE FOR SEVERAL VALUES OF ELEVATION LINE OF SIGHT ACCELERATION FOR FULL SPHERE COVERAGE AND MINIMUM RANGE = 225 FT ı FIG. B-31



CUMULATIVE PROBABILITY DISTRIBUTION OF ABSOLUTE DIFFERENCE OF FIGHTER ALTITUDE AND TARGET RANGE FOR SEVERAL VALUES OF ELEVATION LINE OF SIGHT ACCELERATION FOR AI RADAR COVERAGE AND MINIKUM RANGE = 225 FT FIG, B-32



CUMULATIVE PROBABILITY DISTRIBUTION OF DIFFERENCE OF FIGHTER ALLITUDE AND TARGET RANGE FOR SEVERAL VALUES OF AZIMUTH LINE OF SIGHT ACCELERATION FOR FULL SPHERE COVERAGE AND MINIMUM RANGE = 225 FT FIG. B-33-

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- 5. Tables for clutter track-through requirements
  - a. Pulse doppler main beam clutter A VCBT
    - i. Range Acceleration (ARDDOT)
      - (a) Nose sector (AI Radar coverage) Table B-10
      - (b) Tail sector Table B-11
      - (c) Full sphere Table B-12
    - ii. Azimuth line of sight acceleration (AWKDF)
      - (a) Nose sector (AI radar coverage) Table B-13
      - (b) Tail sector Table B-14
      - (c) Full sphere Table B-15
    - iii. Elevations line of sight acceleration (AWJDF)
      - (a) Nose sector (AI radar coverage) Table B-16
      - (b) Tail sector Table B-17
      - (c) Full sphere Table B-18

	Tanga and and and		LINIT	- :		0.00	0.00 AVG		9 6	9 6	O. GO AVE	_	90.0	*; ;	28.37 Ave	77	9.34	£.3		52.28 AVG	9	1.55	16.0	58.48 AVE	123			66.22 AVG		2.20	<b>9</b> .	AN AL AVE		2.98	1.76	1.22	246 AV5	3,95	2.01		60.54 AVG	6.62	2,57	1,06	75.05 AVG	12.	*2 6*	96.0	92,44 AVG	*****
		A STATE OF THE STA	2, 00	•	00.0	9,00	•	•			,	•	90°D	1.17	\? <b>.</b>	31	9,34	¥.	75.0	;	7	1.93	0.0		123	1.52		•	164	2,15	50.	7	212	2.03	1,73	1,16	244	06.0	1.07	1.44	194	1.36	2.94	1,89	;			7,20		70 °076
			00.4	- (		.0.0	•	9				•	90.	1,17	2.0	90	0.33	1.37	6.33	3	90				120		A M	;	291	2.06			210	2.79	4.67	1.04 1.04	251	9.70	90.5	1.20	136	6.27	20.5	1,61	717	***	70.4			339,66
	60.00		16.00	9		9.0	. (	<b>*</b>			<b>.</b>	•	9.0	1.17	75.0	27	0.30	1.37		:	7.0	. 4.		,	117	1.37		•	155	1.63	 		205	2.66	1.62	1.04	247	3,90	1.77	1.14	***	9.6	2.22	1,50	į	11.		4.27		24.286
u 6	. DO LAMBA.		32,00	9 (		00.0	•	5		3 6	•	~	0.02	B	9.0	20	0,20	1,25	0.43	;	14.0	1.28	3		201		,,,		139	1.51	40°4		188	2.14	1,43		.1.0	2.07	1.35	6.7	161	2.5	1.1	10.1	į	926	78. K	1.29		900,000
ì	22	7	50,00	•		60.0	•	- ;	) e		;	~	9.02	7. d	9	21	21.0	1.33	6.47	;	. 4	1.67	6.65		2	2.2	1.10	:	103	1.02			145	1.92	1.32	0.63	185	2.03	1.39	0.67	240	2. 65 2. 65	1	0.0	Ţ	210		2,43		300.00
TABLE B-10	SCOURCE TO CONDITIONS AREN &	TAPE NO	72,90	•		0.0	•	9	9 6			•	0		•	^	90.0	5,14	60.00	;	0.24	67.1	0.47		4;	<b>0</b>	14	•	22	e .	<b>7</b>	*	62	98.0	1.24	0.55	415	1.17	1.27	0 · 3		2.25	1.47	94.0	;	267	20.00			241,14
TA	TENON 64		98.00	- (		30.0	•		3 C	, 6		•	0.0	9 0	2	m	90 0	1,00	0.00	•		1.00	0.00		5. 5. 6.	72.0			N	3,32		\ <b>3</b> * 0	23	0,52	1,14	44.0	**	9.0	1,16	9.0	***	1.27	1.29	96 0	į		10.0	7		234, 62
	SUBJECT		128,30	- C	200	00.0	•	<b>-</b>		) c	•	9	0.0	9 0	2	~	0,62	1.00	00.0	;	10.0	1.00	0.0		# :	2 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	) C	•	23	93.0	4, c	3	*	0.28	1,03	0,17	7	9.0	104	9.20	=	0.73	1.17	4,41	3			1,14		324 35
			162,00	<b>-</b> 6		00.0	•	9 6	) C			0	9			~	0,02	1,00	8,50	•	9,80	1.80	00.0		# 6	60.	9 5	•	91	0.14	H 6	•	\$5	0,21	404	0.20	42	0.27	1,00	9.24	•	9.00	1.13	90,0	;		7.00	9		62,566
			200,00	- t		00.0	•	9			3	6	5.0		2	14	9,02	1,00	0 0	•	9,04	1.00	00.0		•	9 6	3 6		12	0,16	, d	•	70	0.14	1.06	\$2°0	**	0.10	1,09	0.29	91	41.0	E F	0.38		707	7	10.0		242,37
	707 A 54734494			1 Par 20.07	 	STD.						80.00 NB.	֓֞֞֝֞֝֞֞֝֞֓֓֓֓֓֞֓֓֓֓֓֓֞֝֞֓֓֓֓֓֞֓֞֓֓֓֓֞֓֞֓֞֓֞֓֞֓֡֞֞֓֞֓֡֓֞֓֡	- F	40.0	120.00 %8,			510.	44 60 57.	100.00	מ	STD.		180.06 %6.		- E	3	200,00 NG.		Ė		220.00 he.		ä.	STD.	240 08 148	-	E	sto.	40 00	-	i	STB.				sto,		9 A C

**はないないというないというないまままでは、** 

		-					9 4 6				9				AVE				¥v6				AVG				AVG				AVG				Ave				AVG				AVG				AvG	
		PARAMETER ARDDOT	LIMIT	0.01	1.10	2.5	70.00	0.03	1.00	6.6	32.49	0.26	1.43	0.71	43,31	0.86	1.57	0.05	56.10	261	1 76	1.24	68.25	167	2.52	4.4	69.72	200	2.53		68.01	231		2.07	71.22	250	20.0	2.24	74.31	321		2.80	78.09	349	82.70 R 17	7.55	95.87	76.9
		X PARAME	2,00	0.61	1,00	0.0 0	•	0,03	1,00	9	6	52,5	1,41	0.72	•	48.0	1,50	0,47	į	901	9	1 14	. !	168	2,46	90,4	. ;	202	\ I	79.1	•	233	9 6	4.6		792	2.18	1.99		331		2.41	. ;	980	7.22	6.02		11,000
			8,80	0.01	1,00	9.0	•	0.03	0.	e .	00	3,75	4	0.72	9	0	3 7 6	96.0	į	60 F		0.0	. •	171	22.22	1.23		207	7	4		240	7	9		273				747		2.09	, !	40 C	70.5			943.00
	60.00		19,50	0.61	1.00	6. 6	•	80.9	4, 7 <b>0</b>	e.	ě	6.20	1.25	0.34	•	0.73	1.36	6,65	į	134	77	0.0	ĺ	171	0 T	9.0		211	9 . 2 .	. G		549	9.0	1.07		281	96.	1.21		368	9.0	1.45	.	552		3.45		//* 0
	225, de Landa e		32,00	0.01	1,00	<b>96</b> .	97	0,02	1,00	00,0	;	1	1.19	0,53	13	2,54	1,28	96.0	;	911	77	0.71	. !	154		90	,	199	2.13			224	, . , .	6.0		264	75.	96.0		355		1.15	. ;	265	10 7 0 T	2,81		12.011
B-11			30,60	10.0	1.90	9 .	~	20.0	9	00.5	•	90.0	N	6.15	A M	70.0	11.1	6,93	:	2		0.97	į	121	1.23	6.67		150				591	26.	6.65		227	70.7	0.71		316		0.82	į	000	20,00	2.26		920
TABLE B.	INTERACTORS OF THE PARTY	4400	72.00	90.0	0.00	90.0	-	10.0	9.0	90.0	•	0.02	4 . 5 . 6 .	0.57	36	0.22	1,13	9.0	•	è		*	;	•	91.	9		110	7	4		57	100	0		179	1.20	0.54		262	10.1	0.67	•	296	20.7	1,65	454 11	10,00
	PARAMETER INTERACTION TE.COMBITTONS BRIN H	•	30.84	e .	0.0	e	a	60.0	0.0	<b>.</b>	•	0,02	1.00	0.0	¥.	9.11	20.7	0.27	3	200	2	11		7.	9 4	0,20	;	*;	No.	0,16		***		0,24		145	1.0	10.0		210	10.	0,50		9,	7 9	1,40	46.5	10 20
	SUBJECT		128,00	00.0	0.00	00.0	a	00 0	0	00.0	•	0.01	1,00	30.0	•	0.07	1,00	00.0	•	, e		0		•	2 C	***	;	6		27.0		2	) M	<b>91</b> 0			90.	0.23	,	150	S	0,42	į	205	3,64	1,16	454 30	421,00
			162,00	00.0	0.00	o •	٠	00,0	0	0 ° 0	+	10,0	1,00	9 2 2	4	0.03	1,00	90.0	ť	è		0	•	9 :	1 2 2	98.0		et d PO F		0			9 5	000		6 7		00.0		9	60 E	H	. ;	290	7 W	83.0	96 747	, , , , , , , , , , , , , , , , , , ,
			200,00	900	0	0	۰	00 0	0,00	9	-	10'0	1,00	00°0	M	17	1,00	0.03	,	3 5		9	•		100	0		O 4	10	0		27	¥ C	6		7 9	1.00	0.0		20 4 20 4	3 tr	30		P) 6	75	90		CT*7/*
		ARAMETER A VORT	6 6		i.	STD,	40.00 %6.			STD,	4 00 0 a		in the second	STD	120 DB NG.	90.	10	STB,		10 to 10 10 10 10 10 10 10 10 10 10 10 10 10		STD.		190.061		STB.		200,00		570,		220,00 NB.		or the		246.00 %9.	 	STR		300.00	 	STD.		100	; ; ;	87.0	•	.7

The second secon

		N PARAMETER ARDDRY	6,09 2,00 LIMIT	533	,- \	1,74 1,72 1,77 p 04 4 48 4 34	•	437 621	12,25		\$	94.16 AVG		00.44 KU.44 GP.654		•	770 668 627	24,59 2		4,01 4,77				4,28 7,27 7,18 W TR 92		929	30,48 32,84 32,55		4.66				2,00 9,00 6,25		۵.	_	5,07 6,09 7,01 1 66 R Te A A		740 626	47,86 49,66 40,15	A4.71 17.44 19.40	•	670		60.4 00.4 01.4	02"6 92"6 90"	SA CE TO TO THE TOTAL TO	=	61,6824 96,86 86,93	798.41	3VA -04 242 115 243 63.
	66.00		16,00	517	5.72	4.30		786	10.00	1,77	1.09			16.45		1.	868	21.07	2.99	2,22	į	977	23.00	2.0	76'3	:	27.02	3.49	2.47		1027	10.05	2.5		1690	32.34	9 6	Z	1879	34,48	70.4 1	3.10	1133	40.79	4.91	3,51		1011 1011	, A	•.	74n 47
	DEGS GO LAMBA =		32.00	453	4.56	1.26	66.0	157	11.0	1.56	0.89	-	125	10,03		7.1	940	17.58	2,34	1.64		1047	21.72	0 ·		1084	23.67	2.74	1,99	10	1121	22,20	2.03	•	1154	27.61	, c		1206	29,75	, s	2.32	5 282	15,29	3,45	2,63		74 47	6,23	6,10	440 20
B-12	25 25 25 25 25 25 25 25 25 25 25 25 25 2	•	. R	340	3,42	61.1		553	6,15	1.30	<b>*</b> 6 0	i	769	4		11.1	248	13,73	1.93	1.30	,	7201	17.17	11.7	C .	1361	10.79	2,12	1.92		1111	20.07		•	1145	22,15	7.		1196	23, 92	2,51	7.80	1283	28.37	2,73	2,04	-14			21'5	16. 97
TABLE B-	RAMETER INTERACTION BADITIONS RMIN H	2011	72,00	267	2,43			432	4,40	1.28	0.64	ļ	624			•	767	19,03	1.64	1.04		868	12.09		***	770	13.96	1.86	1,1			17.1	1.27		1691	16.62	2.62	7	1983	17.95			1183	21,41	2.27	1,62	74.97	77	3,58	\$.00	357.74
TA	16.2		96.00	201	1,73		40.0	958	3,15	1,17	6.43		TO S	*n*	7 4		651	7.38	1,42	0.77	į	44,	B .	7.0		828	10.4	1 30	•	. ;	878	::		•	<b>914</b>	12,56	1.71	-	963	13.68	1,77	1.11	1864	16,16	1,92	1,25	***	14 67	2.98	2,40	397.46
	SUBJECT		126,00	. 47		4 C	•	258	2,28	11,11	0,37	;	413	70		***	533	5,43	1,20	24.0	. ,	9	ri i	7	•	F2.9	7.73	100	6.7	. ;	02/	2	1.42	•	762	0r.	1,5		862	10,04	1,57	0,92	26.7	11,99	1.69	1.04	****	26 26	2.39	2, 61	355.64
			162,50	601	06.0			168	1,60	1,07	0,33		315	Z 7V	77.1		416	98.5	1,16	0,53	. !	005	76.	5 T	90.4	* Y Y	5.47	1,29	7.0	.	926	9 .	100	•	620	4.77	) H		692	7,29	1,66	6,75	121	9.74	1,50	d. <b>0</b> 5	•	1960	2,30	1,67	357.42
		•	200,00	81	67	, i	6710	147	1,23	1,05	0,32	į	238	26.	1	0 · 1	31.7	2.74	1, 9	0 0		200 j	9 7	***		<b>6</b> 07	3,00	1,17	26,0		•	-	10	•	19		1.26		516	5,24	1,29	-	775	6.34	1,36	0,72			2.08		359.07
		**************************************		23.00 Ve.	្ត់	- E	- - -	40.00 199.		, La	STD.					.a.c	120.00 NB.	Į.		STD.		160.00 160.			100	180 00 00		5	STD,		200.48 NB.				\$20.08 NB.				240.00 58.	PCT.		STD,	100 00 20			STD.				sta.	AVG

		A PARAMETER A VIDE	0.10 LIMIT	00-0	000			•••	:··	::		***	1017 1010	BAY 96°0	21	4.24 0.34 		1,41 AV6	2	9.67 1.96	10-0 00-0	1-40 AVE		1.47	6.62 1.00	1,26 AV6	1.43 2.20	90.1	-	212	2.47 2.48	1.61 1.76			1.63 2.03	1.20		321 323	•	1.70 1.95	_	733 421		5.05	2031 AVE
			÷.	•	2	•	•	•••	:	:	•		00.0	•	15	e.13		}	7	in :	7.0	: 1	2;		6.73	1	1,13	4		133	1.59			150 150 150	94-1	1.01		235		1.49		870	3.69	2.93	
	;		3°	•	•	:	•	:	:	:	m	20.0			2			}	1	* :	14.0	}			£.	2	0.73	1.26		44	1.63	6.57		77	1.63	0.74	;	181		1.07	i	18.51	2.62	2.18	
	253-66 LANGAE		#.	•			•	•••	:	:	-				<b>s</b>	:		}	ĸ	6.5	0110	; ;		10.1	9.32	ē	94.0	***		70	0.67	1.20	; ;		2		:			0.76	į	10.01	2.15	1.65	
		-		•	2:		•	0.00	9.0	:	-				2			•	11		0.24		2		0.22	2	<b>9</b> 2.0	1.67		24	6.37			2	111	6.39	•	9 4	7	19.0	į	\$25¢	1.83	1:10	
TABLE B-13	IN INTERAC	TAPE NO.	3,		9.0		Đ	00.0	0.0	•	•	•		•	۳;				<b>:</b>			:			<b>0</b>	23	6.18			50	ار ا	6,23	;		1.00	02*0	ě	0 - 4.3	71.1	0.97	į	5.62	1.60	98.0	
T/	PARAMETER INTERACTION SUBJECT TO CONDITIONS MAIN =		Ĭ,	• • •	•		•	00.0	•	•	•	0.0	9 0	1			0.0		•		90.	•	***	:	0.0	*	0.11	7.00		52	0*50	0.00	;		1.00	00.0	2	0.40		6.31	į	6.03 4.03	1-41	0.65	
	SUBJECT		•••	•••	* • •		•	00.0			•						•	,	,	1,00	0	٠	90-0	1.00	•	13	0.10	1.00 .30		12:	1.			6,22	1.00	0.0	7	6,39	1.07	0.25	294	3.60	1.27	0.52	
			<b>6.1</b>	9.30			•	0		•	•	0.0	0		-1 ×		•	•	* :		•	•	- 0	1.00	•	σ.	10.0		)    -	#1	71.0			0.15	1.00	0.00	ŗ	2	1.03	6.17	ě	65.5	1.20	0.42	
			10.00	•		•	•	•			u3	•	, -	,	-:		•	•	• :	7 6	0	•	10.0	1.00	•	Φ	0.05	0 to	•	25		9		0,10	1.90	90.0	*	0.23	1.04	0.10	***	1.61	1.13	۴,٠٥	
		ANAME SEE A VUBIT	20.00 MG.		. D.		40.84 MO.	į ž			56.80 AC.	, to	sto.		120.05 MO.	6	STO.			5	STD.	186.00		01.	<b>\$</b> T0.	POR PRO NO.		310		220.08 MO.		<b>3</b> 02	246.80 20.	1	.T0	តំ ភ	366.30 40.	ָּבְיָּבְיּבְיּבְיּבְיּבְיּבְיּבְיּבְיּבְיּבְי	07.	STD.	THE MO.	į	•	sto.	1

B-14	
TABLE	

			SUBJECT		PARAMETER INTERACTION TO CONSITIONS RRIN #		OFF TAIL				
PANAMETER A VCBT					·				_	X PARAMETER	ETER A WILLY
	10.00	A.10	4		TAPE #0	0.		,			
26.00 40.					-	2,50	•	n 6 • 6	***	0.10	LIMIT
	9	•	9		•	•	•	-	~	4	red
DT.	9 6						9.00	0.0	0,01	10°C	0.01
2	9			0000		•••		1.00	1.00	1.00	1.0
						9.	0.0	0.00	90.9	90.9	::
48,60 NO.	•	•	G	•	•	•					1.16 AVG
	0.00	90-0	6.4		•	•	• ;		-	~	•
DT.	00.0		0.69					10.0	0.0	0.02	0.03
510 <b>.</b>	0.0	0.0	0.0	0	90.0			-		7 ° ° °	<b>1.</b>
				•						•	9.0
80. PO NO.	6	•	•	•	•	•	•	•	•	:	BAY AVE
ָבָּי מ	9.0	0.0	0.00	0-0	90.0	0.0	•	9	•		3
. DT.	9.00	0.0	0.00	0.0	9						47.0
STD.	0	•••	00.0	0.0	00.0	9.0			10.0		
130.00	,	•	•			1	}				11.00
	- 6	•			M	S	80	16	37	3	
	00.0			0.0	0.12	4.0	9.0	er.	*	.72	1
<b>C1</b> 0.			1	1.00	00.1	1.0	1.00		1,16	1.45	1.57
•				•	-	•••	90.0	•••	6.37	1	26.0
160.60 MO.	•	•	•	•	:	i	i	į			0.62 AVG
	0.03	0.63	90.0		17	21	Ħ	5	9	Ž,	132
.10	1.90	1.00	1.17			07.0		<b>M</b>		:	1.05
ST0.	9.0	00·3	0.37	4			919	n : 1	1.24	1.0	1.76
						A 7	7	T+ : E	70.0		7.54
180.06	•	^	9	•1	19	-	**	-	711	17.	1.16 AVG
	50.0	90.0	<b>0</b>	0-13	0.17	2	£ <b>7</b> • •	0.73	1.27	2,22	
			4.10	7-14	1.11	1.16	1.17	1.36	1.37	1.7	1.15
				2,3	.31	6,37	<b>97.</b>	15.9	9.0	1.29	1.47
200,000 40.	•	•	75	1.1	*	•	;		•		1.24 AVB
	6.05	94.0	\$1.0	. T	22	,	1	7 :		161	102
	1.00	1.00	1.00	213	10.1	1 1 1	10.0	10.1	1.72	Z.E.	3,23
<b>.</b>	0.0	•	0.29	0.32	0.27	7.	96		1		7° 67
	(	,	,			) )		!	:		76
	9 6	21 6	<u>-</u>	<b>1</b> -1	8	*	1	127	184	522	231
		7.0		52.	100	95.0	0.82	1,35	2.23	3,46	3.5
1015				-		1-1	2:1	 E:1	1-49	:	<b>5.</b> 14
			77.0	92.0	22.0	.43	100	6,63	. 80	1.56	2.67
240.09 MC.	11	15	ź	**	3	8		-	***	ì	1.44 AVE
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, 0	90.1	1,00	<b>1</b>	1.06	1.68	1.17	72.1		7.5		20.0
3	•		97.0	23.	6.27	6.41	7.4.0	•	0.97	1.0	2.26
300.00 MC.	1.7	:	*	•	i	1	•			1	1.55 AVE
PCT.	\$1.°	9.16	0.33		12.0	2 %	<b>!</b> :	ָ הַלְּי	7 .	728	125
94	1.96	1.16	1.14	1015	1.21		100			9 9	7.1
sas.	92.0	0.36	0.35	3		19.3			1.23	7.1.4	Z.72
LIMIT NO.	138	166	217	, e ,	***	•	•				1.65 AVG
	1.23	1.5	2.08	2,93	9	17.5		1			ž
, o	1.12	1.5	1.20	1.97	5			7454		19.00	22.76
STD.	0.34	0.30	0.42	***		9	1.21	1.72	2.44		7.55
AVG	548.20	12.6.27	568.17	***	26. 244	70 157		•	,		3.12 AVG
,	}		1	7	463413	65.9	452.44	437,42	431.07	458.84	

		្នាក់កក់កក់ស្លើកក់ក្នុងកក់ក្ <sub>លើ</sub> លើងកំកក្លើសលើកក់ស្លើងថា ស្លឹងថា រ	. รู้ "หล่อกัญพอกัญจักกัญตั้งกัญตั้งกัญตั้งกัญตั้งกัญตั้งกัญ ว่า		
438 515 438 515 1.60 11.69 1.00 11.69 565 11.66 2.02 2.34 668 6.25 64.57 18.46 2.65 3.54 2.13 2.98 2.13 2.98 2.13 2.98 2.13 2.98 2.13 2.98 2.13 2.98					
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TABLE B-16

PARAMETER A WIDF			b 6		96	B. BO AVG	•	9.60	90.0		1.08 AVG	`*	1	. 25	3.90 AVG	<b>5</b>	***	. 66	0,83 AVG	*	9 %		1,25 AVG	123	96	\$ C.	TT VAC	194	. 20	7 · 00	1.64 AVE		9	1,76	86 AVG		50.	19	94 TO 1	323	, 62		76 AVG		. 49	( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( )	7.50 AVE
ETER ,	•		Ī	•	_			_			_	•	•			•	-	-	•	•	- •	-	-		-	•••	•	,		~ •	•	•	~	~ ~	1 41	,	<b>P</b> 7 (	~ •	4 64		•	) 1 <b>4</b>		,	<b>4</b>	7	
X PARAN		0110	9			•	-	00.0	0	00.0	•			0,40		<b>6</b> 1		19.0	•	77	12	19.0	•	103		70.	•	138	() () ()			185	2.23	4 C		223	80 m	10	1111	316	5,19	N P P P	4717	715	34,00	20.0	
	47-4		-		900	•	-	ę	000	2	•	70.0		7	•	3	PH P	0.42	•			0.43	}	69	6,72		•	T.	21.	26.0		124	1,40	1,45	•	196	<b>7</b>	1175	3	546	65 'S	1,41		783	24 545	4 5 M	76 16
90.09	ć	- ·	) C		9		0	0,0	0.0	90.0	c	, C	1.50	0.50	•	•		32.0	,	22	46.4		•	<b>17</b>	<b>;</b>	12 · 1	•	•	ę١	9 6	2	29	6.0	10°C	•	101	1,22	70.0	5	174	2,12	1,00		669	16.63	20.0	4313
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VORLEGT TO CONDITIONS AND E	TAPE NG.	9	9 69 69		0			0.00	200	9.6	•	9.00	0	000	1	~ ;	70.0	00.0	,	# 5	A 4	00.0	•	<b>.</b>	0.11			25	01°		•	25	0,27	1.00	<u>.</u>	2	0,57	1001	<b>:</b>	3	***	1,10		624	6.3		***
ilianca ai	4	-	90.0	0.00	000		<b>.</b>	e .		5		0.00	90	90.0	•	۰ ا		0	,	•		90.0	•	25	ij.		•	# ;			-	<b>5</b>	27.0	0.17	-	33	60.0	ä	<u>:</u>	57	2610	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	-	579	9		) i
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	6	-	ם.	9.00	0,0	,	<b>3</b>		)     	2	•	, C	0	0,00		e :	90	20.0	,	- i		0	•	2 5	Y 6	201	•	<b>ب</b>	* E		•	•	670	9 0 3 U	) 	#		# E		5.	4110	100		22.3	2,23	1160	1.10
<u> 4804 € 53:34¥5</u>		70.00		i.i	STE.		40,60 AE,	5 1	1 1		.50 %6.	2	11	STE		120.00 he,		STE		TOU.DG NE.		STE		150,00 Ne.		: 63 - 63 - 63 - 63		.00.00 NE.	- •	515		220,00 he,	i i	14 E 1		40.00 NG		215		300.00 NE.	֓֞֞֞֜֜֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֡֓֓֓֓֓֡֓֓֡֓֡֓֡֓	715	•	LIMIT NE		2 0	-

		X PARANETER A WIDE	.4C D.10 LIMIT	-	100 61 0.01	300		W.	,U1 0,82 0,03	1.10	90.0	ţ	20	1.39	0,68 0,71	;	27 64	26. 4 .38			77 123 132	179 1,52	173	en'i oni	156 167	2,10	90° H 99° H 90° H	7 1 6 4	155 200	,52 2,67	139 1,78	,86 1,53 1,86	227	.93 3,36	,43 1.62	1,58 2,07		3,95	1,51 1,86 2,25	1,59 2,24	272	4,02 4,19 7,14	2,26	2,83		20.06	Va.02 20.00	4,12 7,55	3,24 AVG 447,24 438,82 444,41	
	90.09		-		6.00		•		00.00		<b>a</b>		C, 33			•	•					0 121	4 6	•		•	1,25	•		. 95	1,24	.61		24 1	•	G 99.			1,31			2,66				Ī	2,44		449,27 447	
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B-17		9	•	5	96		<u>:</u>	5	90.0	00.5	90.0	•	10.0	1,00	00.0	•	•		00.0		30	62.2	2 4	B	38	45.4	## #	7240	21	£,45	31.0	3,30	89	0,61	1,12	0,32	55	8.75	1;11	0,31	124	1,23	1,24	6,73	427	5.87	1,72	P 4 2	471,53	• !
TABLE I	PARAMETER INTERACTION COMPITIONS RRIN R	3017	N 60	5	<b>0</b>		3	•	r. 90	20,2	93.0	c	0,00	00.0	30.0	•	• 1	20,0	00.0			61.0	-	•		-	10 to	•		-	80 T	-			-	6	44	-	A 0.4	-			-	-	32E	55	4	59*0	479,45	
	18		16°7	3					9	5	5	٥		10.0	-	•	3 (		0	•		41.0	•	•	26	0,2%	# 6 6 4 1	417	33	. 0 . 2E	1,06	0,24	3	0 34	1,07	-	4	0.41	1,00	0,24		9 0			345	10.5	(A)	26.0	494,64	
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			8,10	<b>C</b>	200	96.0	3	-	000	0	_	62	00.0	00'0	00.0	•	r+ ;	3 6	200,20	•	#	01.0	100		13	6,11	40,00	111	15	C, 13	1,07	42÷D	45	6,15	1,06	6,23	**		1,04	•	5	6,25	1,03	6,27	216	( ) ( )	1,23	C 1 42	527,62	•
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		PASAMETER A VCBT		20.00 he,				40,70 NE.	ב ב	5	STE	10.01	104	13	STC		134 00 021	รับ เ	STE	•	160,00 NE.			13.5	180,00 NE			i n	200,00 %6,		<b>.</b>	STL	225.00 %6.	PCT	Lij	STE	240.00 NE.		5	1255	20 002		<u>.</u>	Siri	102		I	1112	) 3 <b>4</b>	

	R A WJDF		520	7,30	1.75	i.24		12.49	2,52	1.96	3,78 AVG	70.	2004	7 C N	3,62 AVG	627	29.00	9.6	77. CY 2	969	20.08	3.76	5.72	3.68 AVG	67 61 55 61	6.22		3,68 AVG	667	25,00		3.89 AVG	671	57,53	7,01	SA KO'E		40.19	:. ::	7,57		46.94	9,76		3000	19.92	1138,16	798,41	363,63	
	X PARAMETER	•	506	68.4	1,71	1,16	849	11,55	2,34	1,82	,		77 2	40.6	•	722	22,59	2,92	40.00	795	26.93	4,24	3,84	;	28.80	4.45	4.02		848	31,09	4.4	•	684	33,25	1,71		616	39,46	20.		984	41,35	5,27	5,19	8.83	· ••		14:70	358,56	
		;	7.64	5,83	1,61	1,00	577	9.62	2,09	1,90	į	673		2.18	•	745	17,86	24.00	C 1 2	536	25.09	3116	2165	į	87 G	76.50	217		910	23,89	2180	-	941	25,43	2000	-	978	27,106	2167	21.5	1072	31,24	16 to 10	3439	13.72	65,80	6118	9	353,82	
6		;	000	4.65	1,53	96.0	4	7.53	1.67	1,29	;	200	61.17	1.62	•	740	13,45	2,28	7,17	836	15,79	2,37	1,86	•	100	2.43	1,90	•	404	17.68	10.	•	940	16,79	15.0		\$ to	19,96	2,54	40 ° 7	1077	22,41	2,65	2,20	1463	47,58	4,00	3, 7)	348,71	
360 DEGS		,	0 F	44.8	1,45	0,83	4.82	5.68	1,65	56.0				100		682	10,03	9 C	1160	767	11.67	16.1	1,39	į	147	1.04	1,42		829	12,98	44.	-	866	13,72	2,01	;	916	14,75	Z, U1	1,21	990	16,05	2,11	1,60	43.65	35.09	5,22	21,2	349,55	
ÚO.		••	Z, 5U	2,52	1,29	1210	345	4.0	1.42	0.74	9	554		10.0		585	7.37	1,58	7.01	662	6.65	1,64	1,11		0 0 0 0 1 0 0	4.67	1,15		719	60.0	9 F.		756	10 to 1	1,72	111.	161	10,96	1,74	1,73	949	12.36	1.82	1,31	1222	26.52	2.72	2:13	354,73	
TABLE B-1		TAPE NO.	3 4 6 °	1,72	1,17	0,42	204	2.91	1.24	6,51	•	904		99	•	477	5,21	10 10 10 10 10 10 10 10 10 10 10 10 10 1	2,42	542	6.17	1,43	0.79		700	A 40	0,82		592		· ()		929	7,54	2. c		929	7,93	2,22	<b>A9.</b> 0	711	9,11	1.61	95.0	700	20.34	2,44	1,73	364,64	
I SASHTERA			- C.	50.4	1,00	0,27	200	2.02	11.	0,36	•	* C C	200	3 6 6	•	200	3,70	2.5 2.5	\r * 0	428	4.51	1,32	0,0	į	, e	90	0,73		468	21	74	•	693	9,26	4.	<b>1</b>	513		4 6	* K.	558	6,76	25.0	0,80	45	15.83	2,32	7,52	376,89	
		;	0 4 0 5 4	. E. C.	1.07	9210	24.	, .	1114	0,38		יי יי יי	, ,	96.0	-	283	2,79	1,24	2	335	3.38	1,27	0,57		5 4 E		3,62		364	10 m	* * * * * * * * * * * * * * * * * * *	2	2000	4,23	1,37	, ,	485	97.7	() () () () () () () () () () () () () (	49.5	448	5.19	4.45	97.0	326	19.01	2,20	1,33	£2. 75£	
				19.3	1,10	G 30	121	1111	1112	07.3	•	10 10 10 14 14 14		7 4 5	: •	224	64.4	1,22	n L +	27.0	. 68	1,24	2530		6/2	1.26	0513		294	90,	) to to		310	1,37	# t	) 0 4	335	55.5	45°	2913	372	4.14	1 43	59.3	263		ž.12	114	343,56	
			10 T	411	1,11	25.0	11.2	4.0	1 10	かれてつ		111		44.		158	1,63	27 C	,	228	2.55	1,24	8 ¥ E	,	7 1	9 10 10	4		246	C. F	) I	•	264	13 14 14 14 14 14 14 14 14 14 14 14 14 14	*) ( [기년 대기	2	278	2,56	en i	/ 6 1 0	100 E-1	3,42	) N	49.0	£ 1.5	40 M	2 67	זונפ	395,60	
	PAGAMETER A VCBT		- 9% 50 30	100	• •	STE	40.00 35.			STE		1 1 1 DO 1 DO 1		  		120'0C NE.		in the	) . C	160.0C NE.		L	STC		180,00 NE	 	STE		200.00 he,			1	220,00 NE.		in the	<b>1</b> 1 . C	240,00 NE,	P.17	ត់	3.1.S	. 24		13	*** V1	6 4 4 4 4		) : 1	215	10 .3 48	

- b. fo Notch (ABS VC)
  - Range acceleration (ARDDOT)
    - (a) Nose sector (AI radar coverage) Table B-19
    - (b) Tail sector Table B-20
    - (c) Full sphere Table B-21
  - ii. Azimuth line of sight acceleration (AWKDF)
    - (a) Nose sector (AI radar coverage) Table B-22
    - (b) Tail sector Table B-23
    - (c) Full sphere Table 8-24
  - iii. Elevation line of sight acceleration (AWJDF)
    - (a) Nose sector (AI radar coverage) Table B-25
    - (b) Tail sector Table B-26
    - (c) Full sphere Table B-27

	,	<u>-</u>				AVG				AVG				AVE					<b>5</b>				24				1	<b>8</b>				Ā									<b>▼</b> < G				AVG				27	
	1	PARAMETER ARDDOT		0.57	1.67	7.23	72	20.1	11.70	20,000		7.48	20.2			5.93	2.18			121	25.3	76			2.91	2,49			100		30,00	104.06	201	0D. *	2.4	10.00	25.7	4.62	2.67	4.24	98.45	7	. 64	4.15		421	40.49	14.67	_	639.33
		X PARAME	2,96	56.9	1		75	10.1	0 T T	•	*	7.7	2.20	•	114	1,89	2,08	2,23		223	12.2	70.7	•	190	2,86	2,39	2.36		7/1	4	2.53		204	10°0	2.42	3,16	221	4,55	2,58	3,12	•		2,62	3,07	•	967	9. 60		9	638,98
			<b>.</b>	6 2	1,24	•	2	0.4	7.70	•	2	£,2	10	•	121	1.71	1.77	1,24	:	2 6	10.2		:	159	2.63	2°08	1,60	•	201	2.14	4	•	215	3.69	213	77 7	233	4,29	2.31	2,28	•		2 36	2,27	,	*24	37.80		,	641,36
	60.00		9. 9. 9.	9,0	4. 4. 6. 4. 6. 6.	•	7.			!	2	1.87		•	117	1.47	1.97	•.	•	97		0 5	•	181	2,31		1.26	•	781	1.02	90.		216	5.32	)) ( 	1.1	256	3,05	2.08	9.68	;	107	2.16	1,68	•	811		10.0		642,38
	, 00 LANDAR		<b>35</b> .90	0.33	4.08 2.08	•	*			?	<b>S</b>	20.0	1,00	•	101	1.27	<b>3</b>	<b>9</b>	***			10.0		947-	2.04	1.72	<b>2</b> 0.4	•	, T		22	•	208	9,00	1.73 1.64	7717	230	3,41	90.	1,33	786		200	4.34		124	28.69	20.0		643,78
B-19	22	•		12.0	D 0		2:	2 4		•	2	£ .	40	•	<b>•</b>	71.	, se	1.0	***				•	134	17 d	1.32	•	***	•	1.92	0.0		168	2.32	e e	•	202	2,67	29°	1.02	210			1,63	,	27 C	7.0		?	648.37
TABLE ]	SUBJECT 10 CONDITIONS MAIN B	TAPE NO.	2,00	0.20	90.0		2	4 C	91.0	•	3	76.0	90	•	*	0.76	1,22	**	*		7		•	121	۲.۲. در	1.37	10.0	17.	97	10	9.0		154	2,40	90		169	1,92	70 1	0.70	184			0.80		797	10.00		:	671,82
	PARAMETE			27.5	9 0		W (		0		200	29.0	90		ņ	\$ 0	21.	42.0		1 1		4.0	•	63	60 C	1,23	\ • • • •			1.22	4	,	125	1,21	77.1		136	1,33	1,25	, o	146		1,28	66 0	!	**************************************	A 2 10 10 10 10 10 10 10 10 10 10 10 10 10	. T	•	732,59
	SUBJECT	;	99' <b>821</b>	60.0		. ;	O T		0	;	<b>~</b> [	7.		•	ic C	<b>5</b>		* I .	•			20	•	<b>.</b>	4	21.	3	-		1.16	40		9	24.0	1	;	106	50° #		C .	116		25	0.51	į	7 ,		4	<u>:</u>	726,35
			192,06	0.07	9.0	. ;	P 4	10	0		<b>5</b>		00.0	•	;	98.0	26.1	6113	9	9	200	4		200	e i	) i	975	**	46.0	24	52.0	•	(7) ( <b>43</b> )	5,73	) (P		99	0,78	# i	ت <u>.</u> ک	20		1,15	C. 41	;	7 A C	0.00		-	728,76
		;	30 00Z	90'0	90	. ;	2	000	2	. ;	5	77.0	90		<b>S</b> R	2	3 0	) )	88	e e	00.	0	•	9	Br.		<b>7</b>		4,4	1.03	91.0	•	•	20,0		<u>•</u>	•	96.0	p (	<b>1</b>	22	3	90	5, 2 <b>8</b>		700			•	732,56
	77 <b>98</b> 4 086384040		25.00 NB.	Į.	STD			ā	970		75.86 MB.		STo.		100.00 %6.	į	- 6	20.6	125 05 MR.			\$ 10		150.00 Ne.		3 (	-0.0	175 66 1.4.		i i	STC.		200.00 148,		3 0	,	225.00 NB.	<b>P</b> C7.	D		250 at NA.		13	sts.	:		 		5	446,
	240		25			•	2			ì					10				125					3				175					200				\$22				365				:					

	<u>.</u>		•		•	1 440		<b>.</b>	4 و	AVG	•	- ي		DAY 6				AVG	<b>.</b>	• •		T AVE	. س			8 A 40	<b>.</b>			B/4 1	• •		<u>.</u>	Y VE		_		9 V				5 AVG				<b>3</b>
	•	EN AND	Ltair	0	<u>ج</u>	72	7				7		 	72.6			2	73.31	3	•		73.51	2,		10	70.28	7		2.5	72.3		R	20	24.88	9	2.2	5	71.0	7.63	, S	3.9	72.96	22.7			443.87
	1	N PARAMETER ANDDO	2,00	17.0	1,24		100	7	1.27	•	122	2.5	2	į	161	2.2	1.0	•	178	96.5	700		207	200	200	. ;	228	200	2.62	. ;	C 2 3	2,94	26.33	240	6.78	3,16	2,93	284	7.69	3,35	3,34	180	22,40	7,22	6,62	444,87
			.04	.01	1.22		101	2.	1,1		851		10	. ;		7.00	10.4	•	12	200	00.1	. !	220		9 6			9,4	2,11		4 4 4 A	200	2,19	261	6+9	2,70	2,42	24.2	40.6	2,96	2,69	787	21.92	5,91	<b>1</b> 0.7	446,36
	<b>6</b> 0 '09		18.99		다. 다.	7.0	104	P.		•	Tr.				*		10.1	•	104	70.0	,		273	9 6	100		262 7		1.47	1		2.20	1.93	187	5.76	2,35	1.72	143	40.4	2.47	1,92	583	10.44	4	8.43	451,80
	AIL ANDA 5		95.56	9	0 1	12.0	*	# C	, <del>,</del>	•	123	10.4	0.78		157	. Y	8		184	<b>A</b>	100	• 1	214	7	90	1 1	242	9 4	1.29		111	1.93	1,23	203	4.62	2,60	1,37	113	5.47	2,07	1,46	101	16.81	3,93	2,81	460,92
B-20	PARAMETER INTERSCTION GRE PAIS. CONDITIONS RMIN : 229,00 LANDA	9	20,00	6	9	<b>3</b>	2,5	0.67		•	109		0.97	. ;	140		9		267	0 <u>1</u>	0.72	. :	900	67.7	0.0		***	10.4	34.0			1.1	0,01	274	30.00	1.64	6. B	4	4.12	1.69	4.09		20.0	2,83	2.26	460,26
TABLE	ER INTERIC	TAPE HB.	72.06	12.0	8		<b>3</b>	, c.	0.14	•	2		0,37	. ;	707	20.	4.0		131	97:1	100	, ,	3	7	0.62	! !			6	į	700	1,42		226	2,59	1.56	0.76	247	2.97	1, 51	06.0	195	16.43	2,32	1,85	494,18
	PARAKET TO CONDIT		98.00	; <del>;</del>	4, 00 1, 00	9	7	20,0	96		3		0.27	. ;	71 S		0.83		201		17.0	. !	ri,		7		en e	, c	7	. ;		1,25	0,92	36	1.73	1,24	0,52	183	2.00	1,31	99.0	1	7.00	1,96	7,7	516,56
	SUBJECT TO		128,60	¥ 7.	2		7.	9		•	4		25.7	. 1	100	7 C	# # S		3				45	0.4	60	; ;			200	. ;		) el	0.37	110	1 02	1,14	<b>9</b>	195	17.5	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.49	4	3	7.1	4 56	549,15
			162,00	90'0	1,00	<b>9</b>	17	e .	90	•	25	9 E	0	. ;	S	) C	0	•	40	62.0	- C	•	о ·		0.27	•	7.		22	, (	70 4		0.27	4	G.98	1,67	0,26	ŕ	0.67	1,1	0,35	200	3,63	4 7 7	96.0	593,55
		<b>.</b>	200,00	9.0	96	<b>*</b> • •	D T		90		<b>S</b>	7.5	00	. !	ro 9	10	0	•	7	) i i	96.		:	2	30.	;	7		0.47	, ;		1.0	0.16	17	0.35	1,02	6,15	3	9.0	40	0,20	24.3	2.28	90 11	9.0	612,58
		767 20	3	FCT.	Ė	-	9	5	STD.		9		STD.		2		STD.		2				2		10 to	;	į		STD	,		; =	sto.	9		-	570.	9	F. T.		STD.	ď			្សា	AVG.
		PAHAME . WA	50.50				50.06				75.00				100.00				125.00				150.00				175,62			;	99.09			225.00				25.0				1				

	PARAMETER ARDDOT		407	4.97		94.69 AVG	609	70.		40 40	683	12.82	2.35		181.82 AVG	16.41	2.83	2.87	101.30 AVG	747	10.91	2 10 10	190,88 AVG	_	23,50	20.0	184 K7 AUE	795	26.89	4.24		105.29 AVG	No. N.	7.7		105.46 AVG	14.	20.00	40.10	106.45 AVE	004		• • •	106-80 Av6	_	99.92	1138.18	119.44 AVG	452.48
	X PARAMET	2.00	414	4, 45	1. 0.45	•	618		7.4	30.1	705	12,99	2,24	1.09	756	16.15	2,60	2,44		783	16.01	2 4	•	912	24,12	76.57	9, 10	<b>541</b>	26,49	8,05	3,63		20.60	36	4.20		**	7	4.70	ı	998				103	98.41	62,59	67.1	452,01
		90.0	420	4.15	2.5	•	<b>434</b>	<b>1</b>	76	-	746	14.86	6 . 6 .	1,48	•	15.24	2.35	1,85		926	16,52	7.7	•	<b>406</b>	21.90	, i	7	951	25, 13	3,34	2,7	•	28.48	29.50	80.8	1	284	100	80.0	, ,	101	7.27			303	94,10	13,68	66.33	453,59
	<b>9</b> 0.0 <b>9</b>	18,00	410	3,62	4 C	•	579	76.9	4		179	10.52	1.69	1.02	444	48.84	4.96	1,32	į	020	16.64		· •	1.58	19.69		1.07	1055	22.66	2.6	1.97	• • • •	25.67	2.88	2,18	•	1131		2,41	•	1173	i i i		2.30	1101	80°00		•	456.11
EGS	. BC LAMBA .	32.00	269	3,04	9 G T	}	949	<b>7</b>	12.5		756	\$. B4	4	0°20	1	11.54	1.68	0.99		637	14.14	30.5		1014	16,74	2,07	1	1102	19.34	2,25	1,46		1700	2.33	400	4	1217	60.00	1,75	, ,	1279	, c		0 E .	2492	74.13	6,23		158,88
21	123	•			9 6		513	5	9 0 6 C		688	<b>93.</b> <del>9</del>	1.25		784	99.	4	0,68	į	177	10.94	(4 G)		177	13,72	2 4		1070	15,20	1.76	1,01	,	7.75	20,1	1.17		1202	101	1.27		1265	A 11 . C		1.37	1698	59.31		7115	463,09
TABLE B-	SNS SNS	72.00	208	1.66	4 C	•	440	2.50	100	•	557	54.4	2 m	# C # D	774	6.41	1.23	0.49	i	250		# 45 C	•	821	4.47		D .	016	11,21	1,51	6.79	4	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1,59	98.0	,	1000		20,0	. !	1124	26.61		70.1	1574	44,92	10 E		472.96
PARAMETE	TE CONDITI	30.89	155	1.24	 		316	2.32	3 60	•	455	5,76	*0 ·	. T	67.5		1,12	10 E		<b>9</b>	9.70	4 9 0		676	9	12.1		787	8,30	1,32	₽ <b>.</b> 3	***	0	1.38	99.0	į	916		6.0		970	- T			1430	33,97	2,98		483,37
	SUBLECT	128,50	113	0 <b>.</b> 0			233	0 C	) () () ()		374	2,78	다. 나	# !! 	4,1	3.57	1,07	97.0	į	643	6,29	9 6		544	9,15	4 1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	***	636	9,20	1,22	6,45	146		1.27	0.51	į	734		10 m	•	780	7 N N		5	1223	29,24	85.24 ************************************	4	194,98
		162.50	13	5 <b>9</b> " 0	2 0 2 0 2 0	•	165	1 32	20		242	1,93	1.00 0.00	90.0	<b>C</b>	2.51	1,02	9,14	;	260	2	0.20	•	417	20,0	) c	6280	867	4.49	26,1	0.34	178	2	1.16	35	•			0.42	. '	621	100	í		1020	18.74	2.30	) I	508,84
		200.00	89	9 2 E	4 to		132	601	) E	• •	061	1 32	90	<b>00</b> • 0	328	1,82	1.00	30,0	;	270	2,17	1 6		314	51.30	7	B T 6 O	382	3,23	1,06	92.0	•	7.76	1,09	0.30	į	7 C		I CO	. :	482			000	170	14,91	2.36	\$5 T	517,30
	764 ABS VC			۳۲.	ST:			֓֞֞֝֞֜֝֞֝֓֞֝֓֞֝֓֓֓֓֞֝֓֓֓֞֝֓֓֓֞֝֓֡֓֞֝֓֓֞֝֞֡֓֡֓֡֓֞֡֓֡֓֞֡֓֡֡֡֡֡֓֡֓֡֡֡֡֡֡֓֡֡֡֡֡֡֡֡	3 (c) 31- V	5		, L.	ra (	51D:		•	G	sto.		•	- 10 A		'		F I				-		sto.		-		STB.				570,					a n	, 49·	į,		i .	446,
	. Sere		35.00				20.06				75.06				100 00					125.00				150.00				175.00				90 000	•			į	225.00			į	250.06				, ,				

		<u></u>						AVG				224				:	9				AVB				AVA	•			97.0	2			-	\$ *				2				AVG				4				AVE	
		X PARAMETER A WKDF		LIMIT	7	1.67	3	3.65	22			<b>:</b> :		1.5	20.2	3.16	3	100	2.0	3,19	52.2	121	7.	70.5	2.15	3	2.91	\$	7.0	3	3.41	2.54	90°0	2.20		2.49	4.61	2:19	4.62	2.67	4.24		246	2,73	4.15		421			2.31	630,83
		X PARANE	,	• 1 •		1.37	1.22	,	3			1.13	2	1.0	1,59	1.12	100		7	1.18	;	117	::			1.59	2.24	2002	7•:1	3	2.67	2.0	1.51	į	3.12	2.01	1.50	212	7	2,15	1.63		157	2.2	5	į				•	645.17
			•	9.40	0.22	1.17	4.37		25	*	1.1		•	69.0	1.25	0.55	:	9		0.72	1	6		4		115	9.		•	139	1.79	1.61	1.01	***	201	1.60	1.01	•	2-43	1,73	1.10	•	198	2	1.17	į	970	12.45		?	647.90
	99-09			96.	1.15	1.19	0.39	į	*!	2000	P		4	1.42	1.15	3.42	3	19.7	1.23	0.55	į	F			•	15	86.0			100	1.17	1-46	19.0		1,39	1.43	9.90	•	1.67	1.49	6.91	Ş	1.07	1.53	0.0	i	3	25.5	2.18		643.73
	OFF MOSE 225ces Labbam		;	-		1.25	E+*+		£.	77.		12.0		9.30	1.06	9.23	•		1.23	6.33	į	25		27.	•	\$	69.0	10.74	704.	H	18.6	1.36	0.10	8		1,35	9.68	100	1.17	1.38	0.72	:	1.28	1-30	18.0	;	169	18.01	1.68		650.80
77				<b>.</b>	59.0	1.20	94.0	;	2 :		•	4.63	<b>5</b> 2	12.4	*	92*	;	1	5	5.5	į	e i	1.15			7	<b>?</b> :	7.4		8	95.0	2. 2.	9.50	;	0.70	1.21	9.55	2	0.81	1,28	0.61	i	7.0	1.30	0.67	į	125		41.	•	655.38
TABLE B-22	INTERACT.		TAPE NO.	9	50.0	1.20	•••	:	9 :			•	2	1.16	1.05	7		Į.	1.07	9.26	;	7 .	1.10	0.30	1	96	[F 6	1.28		;	•	***		5	0.50	1.11	0.36	1	0.56	1.14	6.39	,	3	1-14	<b>6.</b> 39	į		1.60	9.0		663.05
	SUBJECT TO CONDITIONS ROWN =		;	•	6.63	1.50	•••	:			D 0 0		E.	9.10	1.00	•	2	9.16	1.60	04.	;	F	06.1	0	;	8 F	22.0			*	0.30	00°	0.37	67	96.0	1.07	0.34	7	0.42	1.08	6. ¥	1		1.00	0.35	į	9 F		99.0		965.50
	SUBJECT T		•	, m	0.02	1.00	0.0	•	9	000			•	90.9		•	15	6.12	1.1	•••	:	71 0		0		02				12	9.22	•		#	0.28	1.03	0.17	99	0,31	1.03	0.16	2	#. #.	1.02	9.15	ģ	2,00	1.27	0.52		8Z*8/9
				<b>.</b>	0.02	1:1		•	<b>9</b>				-	9.0	P * C	•	12	91.0	1.60	00.0		<u>.</u>	1.00	0		51.	71.0			22	<b>9.18</b>	1.63	17.0	7.0	0,22	1.04	0.19	30	52.0	1.03	0.18		6.27	1.03	0.17	ý	֓֞֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	1.20	0.42		982.58
			10.00	~	20.0	1,00	•	•	7	-		:	•	<b>6.0</b> 5			11	0.00	1.00	9.00	:	21.	1.00	00.0		12			•	0.1	0.16	50.0	77.0	5	0.18	1.05	6.21	23	9.10	1.04	0.20	K	0.21	1.04	0.50		***	1.1	0.33		681.78
	,	PARAMETER ABS VC		25.00 to.	ŗ.	<b>.</b>	<b>.</b>	50.05 ED.		.10	<b>.</b>		75.00 140.			•	160.00 40.	•	10	sto.	07 44 3c1			STD.		150.00 MO.	֓֞֞֞֞֞֓֞֓֞֓֓֞֓֞֓֓֓֓֞֓֞֓֓֓֞֞֓	370	•	175.00 NO.	ָּבֶּי בּי	ָ פֿל	• 0.6	200.00 140.	T.	Ţ,	<b>\$</b> 10•	225.00 NO.	_	ָב בַּ	STD.	040.60	ביב	0T.	sto.	11111		94	sto.		904
		7															_				-	•				~				~				~	•			N				^	ł			•					

		PARAMETER A WILLY	****		.7.	1.20	11.	2.14 AVG	<b>:</b>	7007		1.74 AVE	_	2.12	2.24	2.53 1.58 AVE	168 168	2.73	2.36	200	1.78 AVE	3,5	2.57	2.07	102 102	***	2.75	1.54 Ave	223	5.16	2.9	1.57 AVE		<b>1</b>		1.55 AV6	262			1.55 AVG	2;		M. 94	1.54 AVG		65.10 8.17		3.12 AV6 443.67
		X PARAMET	:	•		1.27	.7.	į	• •		7-12	77.1	115	1.62	1.90	1.94	3	2.39	5.00		17.	3.00	2.16	2.00	204	3.71	2°2	•	236	4.41	* ° °		552	5.24	Z C		201	5.62	2.36	į	Ž,	2		<b>A.B.</b> 2		5.14	3.68	451.57
			•		0	1.26	0.65	;	9 :				26	3.25	1.70	1.07	110	1.68	1.76	•	141	2.04	1.62	1.67	174	2.55	<b>1</b> .		102	3.65		9	231	3.67	79-1		548	4-15 2-16	ET.I		192	20.0	3.1	3		. F.	2.44	465.78
	60.09			<b>Y</b> .	0.37	1.28	9.0	i	ī ;				11	0.90	1.59	•	2	1.23	1.57	9 .	211	1.45	1.63	7.46	135	1.70	50	7	159	2,12	1001		182	2.51	1-36		26	1.80	1.37		בוז בוז'ר	1.00	1.48	637	3	2.48	1.72	474.53
	0FF TAIL 225-00 LAMDA •		•	7047	•24	1.25	0.52	}	8		6-1		94	96.9	1901	1039	5	19:0	1-57	1.26	ŗ	25.0	1.60	1.21	6	1.13	96	1 4 4	106	1.33	1.95	1111	126	2°88	1.55		<b>9</b>		1.05	:	2:	1.41	1.16	469	4	1	1.21	497.60
			7	200	0.18	1.15	0.36	į	3 0	1000	1	:	33	9.40	1.52	•	*	45.0	94-1		4	9.0	1.48	6.73	3	0.75	1.42		76	5.0	1.39		96	1,05	1 . 4 6 . 6		111	1.27	40.0	:	921	1.37	3	<b>619</b>		1.63	0.00	531.42
TABLE B	PARAMETER INTERACTION CONDITIONS RMIN #		TAPE NO.	12	0.10	1.06	0.2B	7.	2 -				22	6.23	25.1	000	30	16.9	7-30		•	0+0	<b>2:</b>	0	<b>\$</b>	<b>:</b>	22.1		23	g.	15-1	?	63	•	15.0	<u> </u>	ž;	1.29	6.49	*		1.20		9			29.0	577.37
-	PARAMETER IN' SUBJECT TO CONDITIONS		4.00	-	0.0	1.10	<b>8.30</b>	:		80.1	12.0		11	0.15	21.1	26.30	23	9.25	-1-1		95	0.27	1.13	* n = 0	*	0£-3	1.12	7	38	40.0	11.1		9.	0.42	96.0	. :		1.13	0.33	:	70	1.13	9.34	203	2.6		6.49	598.55
	SUBJECT		6.40	æ	90.0	1.17	0.37	•	90-0	1.14	0.35		7	0-10	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		51	41.0	07-7	•	20	0.18	1.15	9	22	0.20	4 M 0		52	0.22	0.32	•	16	77-0	0.00	ì	4 6	1.09	92.0	7	9 6	1:11	0.31	712	2.08	1.20	***	630.07
			8.10	•	0.03	1.00	00.0	•	0.0	1.00	0.0		•	90.0	00.0	;	11	6.10	1.09		13	6.11	900	•	13		0.27		<b>4</b> !	6.12	97-0		11	40°F	0.24	1	2:	1.05	0.22	2	9,18	1.05	0.21	\$	45.	1:19	<b>Φ</b> Ε • α	649,23
			10.00	•	0.03	1.00	0.0	•	60.0	1.06	0.0		in ,	40.0	00.0	:	•••	6.01	1.13	•	*0	0.01	1.13	66.0	•	6.07	1 E C		• ;	e -	0.31		11	01.0	62.0	:	£1 :	1.03	0.27	ž	0.13	1.07	0.25	138	1.23	1.12	¥	714.33
		AMETER ABS VC		25.00 NO.	L.J.		STD.	50.00 MO.	PCT	nT.	STD.		75.00 NO.	•	e de		100.60 MG.	בָּי בּי	<b>.</b> C.	• • •	125.00 NO.	į.	1	• •	150.00 NG.	į.	510.		175.00 140.		STD.		200.00 NO.		sto.		TOUR BETT	· -	STD.	250.05 NO.	_	10	<b>5</b> T0.	LIMIT NO.	PCT.	į,	STD.	AVG.

						ABLE	-24					
				SUBJECT	TO COMPITION OF	TOWN THIENTY - P.	a Š	44 LANA -	**			
PANAMETER ABS VC	20 SE					Tase and	-				X PARAMETER	TEK A VZOP
		10.01		6,44	;	3.5	2.50	1.66	:	***	0.10	LINIT
25.0	9	<b>#</b>	7	ŝ	3	£	121	3	22	303	ž	199
	֓֞֜֞֜֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֓֓֡֓֡֓֡֓֡		10.0	10 ·	ŗ	1	1-12	1.51	2.31	3.67	70.4	4.57
	į	= ;			= :		2	1-10	Q.	1.27	7	7
	•	•						Ĭ			į	3.10 Ave
=======================================	\$	3	2	<b>1</b>	111	173	112	202	į	=	115	\$
	į	Si.	Ş.		<b>!</b> !	3.	2	2.2	12.	S.8.	7:1	31
					1-12	::	2.1	r:				2:
						<u> </u>	ž	*			1967	1.12 AM
7. E	9	=	3	27	7,	231	787	Lik	;	619	576	3
	į	ř:	<b>.</b>	1.13	\$: -i,		ų.	r:	I.	3	1; 1;	2; 2;
	e de		20.0			31		1001	F	2 %		5.5
		•	•			}				}	}	3.26 AVE
100.	9	1	7.	7	218	Z	361	į	543	2	į	2
	į		ĸ:	r.	2.03	Z.	E.		20.0	11.21	14.70	16.41
	ě	7 7	1017	1201		7.7	ž:		::	21	<b>7</b> .	2; 2;
	;					:			•	200	****	1.13 AVE
125.11	<b>Š</b>	130	961	192	ž	200	<b>9</b> 17	*	ş	776	2	747
		X:	3. 1.	3	2.53		6.83	6.61	9.70	13-61	17.62	10.01
		27.0		5 % T		10.36		2:		2.21	20.2	# # m r
	;	;			•		24.	7101		•		3.42 446
150.8	<b>ş</b>	<u>\$</u>	178	022	162	376	473	;	ş	137	93	3
		7	7-1	2.19	2.05	<b>5</b> ;	29.62	7.92	2.1	16.66	20.97	25.52
	<b>5</b>		17.1	95.0				17				2 2
		1						•	•	•		3.36 AVE
175.	ž,	<u>.</u>	212	85°	Ħ,	5	3	22	*	2	3	£;
		1:16	1.22	1.26	7.1	7	3	9		2.49		4-24
	STO.	9.10	96"0	15.0			5	1.21	1.5	21.2	3.14	4.22
	•	3	1	ş	į	į	;	i	į		į	3,52 AVE
		3	2.30	3.63	7.0.5	j			2	20°	27-16	12.47
	07.	1.21	d.	1.30	1:30	<b>F</b>	1.53		2.00	2.65	3	17
	<b>\$</b> T0.	4.47	45.0	1.	8.72	.66	=	1.27	1-11	2,33	1.5	20.5
225.00	0	220	560	313	104	512	:	Š	632	1903	926	3.57 AV6
	7.	2.16	2.61	3.28	4.33	5	9.0	11.27	16.15	53:22	82.62	33,36
	. e	22.5	9 Y C	10.0	 		6 4 6 4	2.48 5.48	2.17	2.2	**************************************	
		•			•	•		}		}	•	3.56 AVG
250.69	ĝ	235	278	339	669	<b>1</b> 55	169	3	166	1053	951	i
		<b>6.3</b> 1	: X	1.33		# :		12.25	17.61	24.67	32.50	3.5
	Ę	95.0	95.0	50,				1.37	1.92	2.7	1.67	
								•				3.46 AVG
LIHIT	NO.	472	3	637	962	2	1157	1352	1520	1458	2	11
	ŕ	20.0	7.01	11-03	14.21	18.70	24.53	33-15	700	65.83	87.93	26.66
	STD.	1.00	1.22	1.33	1.50	1.75	2.5	2.50	7 S	58.6	16.61	798.41
												4.05 AVG
	9×6.	513.20	511.23	494.89	484.61	474.88	458.82	447.14	440.02	445.21	449.50	_

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		X PASSANETER A MJDF	LIMIT	P (		1.60	2,98 AVG	72	1,53	***	3,18 AVG	26	 	20.2	N. R. AVE		1,0	2,16	3.14		2,32	2,40		2.58 AVG		2,49		2,33 AVB	207	2.54	3,39	2,38 AVG	7a2 •	54.6		2,25 AVG	(S)	2.67	4.24	2,14 AVG	252	2.6	51.5	2.88 AVG		\$ . C	12.12	2,50 AVB	639,83
		X PASAME	6,10	32	2	1,04	!	<b>S</b>	6.75	***	•	2	60.4	00.	111	105	1,44	1,71	1,31	***	1.76	\$ . \$	1,36	,	141	1.96	1,40		192	2.02	4.4			7	<b>5 P D E</b>	į	212	2.83	1.55		235		19.5		715	34,58	70.4		659.88
			07.	24	77.	, r , o	ı	<b>T</b>	96.	18.0	•	70	24	1,27	46.40	*	0.57	1,939		3	1.15	1,53	9,64	;	117	44	8.65		242	19.5	0.07		101		1,82	į	111	1.74	1 1 1	•	7.	61,17	12.21	,	783	24,61		•	680.84
	60°09		0.0	15		0,40		<b>S</b>	1,35	9,50	•	49		1,24	66.0	63	C. 65	1,30	69,8	94	0.77	1,41	6,87	1	2 0	1.51	0.50		961	1.50	20.0		117	9	90.0	į	123		12.1	1	120	7,17	1.21	•	669	16,63	2,38		601.09
	GFF NBSE 225,00 LAMDA=		1,60	13		0,42		27	62.0	6.6		32	0,57	101	70	45	D. 4 d	1,03	81.3		.00	1.40	96,0	į	1 0 1 0	1 0	76.0	. •	9 9	4	6,95	1	9 6	7011	6.	ì		15	10.1		102	21.	1.91	•	289	11,60	2,67	:	664,79
B-25			2,50	55	3 6	, 4 9		25	4.25	169.0	•	90	10.0	200	A C	37	5,3 <b>6</b>	1.30	500	,	0.46	80.4	0,0	•	D 4	1 2 2	68.0	, ;	D 4	0 P	0.05	,	67	2	90.0	;	7.5	1.43	9,97	,	77		96.	•	503	67.40	2,12	7	692,05
TABLE	R INTERACT		3,50	<b>o</b> ;	5,	: # C		67	67.0	10.5	•	\$2	0.24	7,7	,,,,	30	0,30	1,23	29.0	2	33	17.7	86.0	;	# # *	2.20	0.56				9		52	,	0.0	;	3 :		69.0	,	M (	7910	***	•	429	6,37	1,46		694,13
	PARAMETER INTERACTION SOCIETY OF THE SACTION SOCIETY OF THE SACTIONS AND A SACTION SOCIETY OF THE SACTION SOCIETY		4,06		<b>0</b> ,	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	•	ü	۵,	0.57	;	<b>39</b>	9 t 0	77.1	20.00	25	0,22	1,22	16.51	ŧ	6.24	1,20	0,49		9 C	1,20	9	•	7	100	25.0	ı	3	7 6	120		4,	7	15.0	•	9		1,52		379	<b>6</b>			696,12
	Jud JECT		9,46	<b>,</b>	y (	2 6 6 6 6 6 7		9	31.0	1000	•	er i	21	n i	2010	17	910	118	0,51		4 80 1 91 10	9	67	;	N 60	1700	6		3 S	# T T	15.0	•	# F	3 d	0 53	;	6	70.4	15.0	•	9 i	***	1101	•	331	3,68	4	1	716,29
			F, 10	<b>**</b>	,	20.0		0	60,	1.63		12	111	1111	.,33	51	414	1,20	70	:	4 67	7	6,51		5 5	1 t 1 t 1 t 1 t 1 t 1 t 1 t 1 t 1 t 1 t	4	•	*	2 .	7	•	33	3.	94.0	!	27	21.	54.0	•	28	6,26	10.00	; ;	271	2,98		2	724,59
			13,00	;	H 1	3 ts		0		3 C	•	*		D 6	7 1 2	12	01,0	1,50	01.0	ï	7 L7	100	00.0		7 .	16.	80	•		7 6	100	•	77	, i	14		<b>9</b>	21.	10	  - 	19	916	617		22.5	2,23	1,25	7:10	742,66
		DA SHE FR. SHENE		25, CC NE,		+ 12 -1		50,00 AE,	<b>.</b>	L V		75,00 NE.	• 1		- i.i.	160.66 N.E.	1 Ja	, ,	311		122 00 221 PCT.	14	STE		150,63 76,		STE		175,00 AE,		211.5	•	200,90 AE.	֧֓֞֞֞֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	STE		225,00 NE,		217.		250,00 NE.	֓֞֝֝֓֞֝֓֞֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֞֓֓֓֓֞	1 L	,	LIMIT NE.		<b>1</b>	9119	PAG.

	PARAMETER A WIDE	LIMIT		. 22	N	2.48 AVB	2	1,53	1.7		1,93 AVG	41	2.56		1.65 AVB		2.79	2,56		1.64 AVB		***	2.47	1.61 AVG		4,41	2.73		1,59 AV	91.5	2.9	3,26	1.64 AVG	2.		5,35	1.63 AVG	292	<b>5</b> , <b>2</b>	200	3,70	276	1,83	3.55	3.97	1.64 AVG	349	22,76	, T	7.22 ASE	443,87
	X PARAMET	j.	3	190	77.	-	*	NT T	7.	1:1	,,,		10.0			;;	1,4	\$ 0 i	2,1	•	177		2.53	;	204	2,79	2,33	/612	226	4.48	2.4	2,63	į	2	1216	2.69	•	277	5,92	2 6 6 6		287	1.74	2.65	3,12	•	488	20,06	5,15	71.	453,82
		9.4	•	6,42	1115	7.	3	0,75	1,42	0,76	:	•	9717			116	1130	1,72	1125	į	127	99-7	1437		141	2,64	110	10.1	***	2	9	1,92	,	221		1,54	•	231	3,82	2.07	784	240	4.35	2.19	10.00		553	14,67	3,42	J# 5	418.94
	00 i 09	9.6	23	0,26	1,14		;	0.49	1,35	0,76	;	•				2	1111	1,56	1,17		607	76.7	1.16	1	756	1,64	7,63	7110	9	20.2	1,68	1,19	į	174	35.	1.16	;	189	2,61	1.73	1164	202	2,95	1.79	1,32		542	10,57	2.4		432,55
OFF TAIL	E LAMBA	7.60	13	0,16	91	7712	33	0.32	1,21	66.9	;	•		79.0	•	3	99.0	£ 1	6,71	;			7.4	•	16	2.00	2.5	7/10	484	1.23	10	8,76	•	921		10.0	-	142	99 7		101	150	1.86	1.55	0.00		466	7,75	2,08	7,15	516,71
9		1 2.58	<b>6</b>	0.16	110	7710	2	92.0	1,14	0,35	į	-		1	;	-	67.0	1,24	50.0	•		2 10	1.55	•	73	0.73	1,25	***	•	06.9	1.27	9,26		104	A C	1.0	•	118	1,26	40	70.5	76.	9.1	1.61	6.72	,	427	5.67	1,72	0	531,19
TABLE B-2	Sub	TAPE NO.	9	41.0 0.14	0 7 3 1 61		2	0,23	1.89	0,28	:	5		1	•	H	6,35	61.4	9,0	:	1		100	•	38	0,53	92.5	1.	7	6-6	1 18	0.42	i	2	ָב בּיַב	1,22	•	14	8 °	1,21		*	0.97	1.26	-0.58		378	4.55	1,0		551,49
PARAMETE	Te cexpit			110	D F	,,,,,	11	9,14	40,4	0,24	ł	7 7	1 ×		<u>;</u>	27	6,22	40 H	9 T		, ,	7 .	27.0	1	42	۲, a	4. 5.	7210	7	0.42	1,00	0,27	ı	4	2	9 10	•	9.0	0,61	4		13	0.65	1.14	6.35	•	316	3,51	0 P	(	586,45
	SUBJECT	9.4	<b>*</b>	0,07	31	7	•	80°2	1,11	0,51	,					16		1,06	-	;	177	, ,	2.5	•	52	0,21	4 C	7 1 5	96	0.26	1,10	0,30		9 6	700	E 27	•	•	0,42	4 4 5 6 6 6	3710	2		11.1	25.0		241	2,72	H (	3	415,00
	i	6,18		90.0	1 1		•	6,67	1,13	0,33	•	0 7		100	-	13	-	2° 00	6.27	ţ	2 :		12.0	•	19	2,16	4. 0.	77.0	24	5.20	1.04	0.20		27	77.9	P (5- 	•	35	6,30	1,30	,,,,,	4	C.32	40	121		216	2,12	1,23	7.1	531,61
		10.00	in.	S. S.	D T T	7	\$	5310	1,920	D * 5	¥	n 4	- C	1 17	•	•0	93.0	1,17	7510	٠	4 1	~ * * * * * * * * * * * * * * * * * * *	11.0	-	36	63.0	## F	37.60	:		1,07	92.0			1	1 C		21	0,18	C2 1	7,10	2.2	111	1	6.2	•	174	1,60	A	7	051779
	PARAMETER ABS VC		25,00 NE,	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	. R . P	<b>4</b>	50,00 N.E.		1.3	51E		12 DD 1C/		115	,	100,00 NB,		1	ועוני	40 200	123,00 NE,	֓֞֞֞֝֞֞֝֞֝֓֓֓֞֝֓֓֓֓֞֝֞֓֓֓֓֞֞֞֓	7 1 2	1	150,00 %2,		<u>.</u>	110	176 SR NO.		L	5712		200,00	- 3 (	1 Li	•	225,00 NE,	ū	· • • • • • • • • • • • • • • • • • • •		250 30 15			L .				• •	.,	•

		IDF					AVG				•	7				AVG				A.48	•				AVG				AVG				5					•				<b>Y</b>				AVG				AVG	
		PARAMETER A WJD!	LINIT	407	4.57	7 6 7	3.67	609	79.0	7.7	4.	60.0	12.82	2,35	2,33	5,47	126	16.41		10°2	747	19,91	3,84	3,36	95.5	766	BC'C7	3.82	3.56	795	26.00	7,5	77.	200	30,37	4,71	3.02		33.36	5.27	5.64	はん。ウ	77 72	5 77	6.43	3.66	# 5	26.00	798.41	4.16	452,48
		X PARANE	0,16	374	9	10 m	•	572	7,63	4:0	1,21	189	11.30	2.07	1.76		748	14,50		717	798	17,61	2,77	2,46	!	78 46	40 L	2.74	•	968	23,72	5, 51 5, 51	79.00	945	24,98	10.00	3,39	653	29,33	3,86	8,74	685	50.62	4.08	4.16		633	60.70	14,70	:	457,73
			9149	900 1000	2119	9 4 5		787	215	1,93	1,01	707	61.87	11,04	1,36		920		( i i	1	742	17.564	2.36	1,86	į	200	2.40	2 95	•	199	18,29	2 c	2017	076	20,96	2,74	2,41	996	22,36	2,90	2,58	1843	24.97	00.0	2,69		1332	02160	9190		460,97
	90.00		06.0	225	7.25	0.66	•	187	4	9	0.65	č	9	1,63	1 0 E	į	1				929	66.4	1,91	1,42		11,54	2.03	1.57	•	845	13,34	20.5	707	699	15.02	2,17	1,70	914	16,32	2,24	1,83	966	17.44	2,29	1.53		1463	000	3,7	. !	460,47
	340 DEGS 225,00 LAMBA =		1,60	175	2,1	196	•	306	3,27	70.	0	• 67		1,1	19'0	:	26,		10	•	567	7,29	1,61	90 º 7	į	0 K	99.	**	•	707	9,73	1,72		761	11,06	1,77	1,26	926	12,55	1,82	1,32	26.6	12.94	1.87	1,35		1565	7 T	2,72		464,24
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			<b>6</b> ,10	•	2 0	2.28		<b>40</b> (		91:4	6.0	117	1,62	1,09	0,32	:	9		07.0		£97	1,57	1,17	77.0	9	1.89	64.4	64.0		235	6212	0.50		÷92	2.55	1,25	5,50	292	2.83	1,26	64.9	391	3.04	1,27	6,69		ລຸ ເສົາ	1 · ·	574	,	26.92
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- c. Pulse main beam clutter (DELTAR)
  - i. Range acceleration (ARDDOT)
    - (a) Nose sector (AI radar coverage) Table B-28
    - (b) Tail sector Table B-29
    - (c) Full sphere Table B-30
  - ii. Azimuth line of sight acceleration (AWKDF)
    - (a) Nose sector (AI radar coverage) Table B-31
    - (b) Tail sector Table B-32
    - (c) Full sphere Table B-33
  - iii. Elevation line of sight acceleration (AWJDF)
    - (a) Nose sector (AI radar coverage) Table B-34
    - (b) Tail sector Table B-35
    - (c) Full sphere Table B-36

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TABLE
Εď

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	*E* 256.7A	n				404					H PARAME	TER ARDDOT
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State   Stat		•	e.	1,60	1,00	٠.	1.06	1.68	1,07	1.07	1.07	1.07
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Fig.		11,02	0,02	0.02	90.0	0.14	90.0	200	. S.	0.57	0.59	09.0
STD	1.23	1,00		1.00	1,14	1,13	11,1	1,15	1,15	1,15	1,14	1.15
No.   1	STD.	9	00.0	00.0	0,35	0.48	6.42	6.52	0,51	0.50	6,49	
No.   Color			,		,	į	;			į	i	63.68 AVG
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Oct	, T			)   	97.0	BC*0	.03	n, 7c	u.,u	<b>9</b> . 0	0.73	2.5
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STO	:	•	9,82	6.22	0.16	0.30	•	0	1.08	11.1	1.16	1.17
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Sign	)  - 	•		9.4	12,27	25.	1.52	1,71	1.70	1.77	1.86	1.30
Dect.   Dect	sin.	-	Ľ.	a.	16.5	• •	10.1	4,05	1.03	1.04		
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00 \( \begin{array}{c ccccccccccccccccccccccccccccccccccc	510.		90.0	0	5	65.0	1.04	1.06	1.04	1.07	1.12	1.25
10   10   10   10   10   10   10   10		•	•	,	•	. :	, '		,	,	. !	58.63 AVG
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ET,         1,50         1,64         1,54         1,54         1,73         1,86         1,94         1,97         2,14           STD,         0,50         0,49         0,66         0,84         1,69         1,25         1,21         1,24         1,32         1,42         1,43         1,41         66         60         65         60         63         60         40 <td< td=""><td>בוב מ</td><td>•</td><td>1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1</td><td>90.0</td><td>2 0</td><td>7</td><td>10.1</td><td>1.61</td><td>1.36</td><td>7.05</td><td>1,70</td><td>1.72</td></td<>	בוב מ	•	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	90.0	2 0	7	10.1	1.61	1.36	7.05	1,70	1.72
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TABLE

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X PARAME	6		3, 43	1.3	0.39		44	6.03	1,20	0,62	1	142	*1*	70.0	*1.	174	1,04	1,40	1,18	,	7	10,2		•	220	3,03	1,73	<b>8</b>	***	44 7		1.67	•	231	3,94	2,14	, o ,	237	4.42	2,34	2,06		242	4 c	20,0	0,1,	103	98.41	68,89	71.25
	e e	45	0.40	111	0.31		20	6,85	1.15	67.0		191 1	4.6	7 0		173	96	1,35	6,32	,	137	7.		•	221	۶. <del>د</del>	1.67	1,17	9	71 1	) (C	07.	•	234	3,77	2,02	90.1	243	£5.4	2,18	1,72	;	242	•	70	)	593	94,10	20.03	cc*22
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	82 00	* * * * * * * * * * * * * * * * * * *	27.0	1.11	0.31		78	0,68	1,09	6,33		116	7,17			140	1,49	1,26	6,63	į	17.	н . С. 4	) () 		197	2,35	1,50	0.88	6	644	0 0	1.12	:	213	3,02	1,7	: :	228	3,39	1.86	1,40	į	223	×,72		0.11	1491	74.13	8	e .
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	162.50	3 M7	0.02	1,00	00.0	•	'n	40	1,03	0.00		1 : e	۵. مارو	. d 2 ft 4 ft	,	13	9,17	1 1 1	0,31	ŗ	77	) () ) •	- d - d - d	,	59	0.24	1.67	0,26	ć	9 40	7 5 6	0.26	<u>;</u>	3.0	0,2B	/ ·	18.5	**	(n)	1.24	65.0	, i	97	7,53	0 4 5 G	o n o	1020	19,74	0£.	1,6,1
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	7 DEL 187					7/86 MD.	-				X PARAMET	PARAMETER A VXDF
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404,00	€	~	•	-	•	•	13	71	<b>,</b>	=	7	
ķ		0.05	0.02	10.05	•	0		***		197	3	3
	٠ <u>.</u>	1.00	1.00	7.00	1.00	1.10	1.00	1.13	1.16	1-10	1.17	1.15
	sto.	00.0	0.0	00.0	•••	0.30	.28	0 + 8	50	90.0	9.82	4.30
***	1	•	•	•		;						1.68 AVE
	•	7 (	P (	7	~ ;	2:	<b>:</b>	X.	*		2	2
			75.0	· ·			E1.	6.20	r.	96.	0.75	2 ·
						1000	2:	1:14	7201	1.19	F.	26.1
	<u>.</u>						7			7	\c.	
604,00	Q	~	m	~	-	10	36	2	7	3	*	40
	•	20.0	0.03	0.02	90.0	0.10	1.15	***	1.42	1	4.87	
	i d	00.1	9:	000	<b>1</b> -1	1.20	1.19	1:25	1.37	1:31	1.47	*:
	•		•		.35	•	9.30	. 52	.53	6.93	:	0.10
760.00	ě.	^	P	•	•	22	:	*	3	1	:	1-40 AV
		0.02	0.02	0.02		11.0	6.10				***	
	10	1.00	1.00	7.00	1.13	1.17	1.22	2.1	10.11	1		•
	£10.	0.0	•••	0.00	0.33	0.37	0.53	9.70	.10	2.0	1.90	1.01
**	•	•	,	•								1.36 AVB
		~ 6	7 (	٦ (	<b>.</b>	£1;	ຂ	E .	41	2		5
	<u> </u>	20.0	2000	700		21.4	9.19	9.32	, i		5:13	7
	STD.		0	90.0	25.0			100	1.01	7001		
						}						1. 11 AWA
400,00	ç	~	• ;	*	9	1	2	33	15	7	3	
	֓֞֜֞֜֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֡֓֡֓֓֓֓֡֓֡֓֡֓֡֓	20.0	Fp.0	M (0 )	0.10	<b>71.</b>	6.23	9,36	9.65	1.01	 3.	1.52
		200	000		1.20	1.29	1.32	1.36	.59	3.		2.02
	•		20.5	•	9.0	54.0	0.55	0.85		7.06	1.26	
1600.00	, Q.	•	•	•	:	1	ž	;	2	ī	:	I.36 AV6
•		0.02	0.03	0.03	0,10	9	97 Y	. A. A.	74.0			
	oT.	1.00	1.00	1.00	1.60	1.25	1.27	36.	7.7	1.74	0	11.6
	\$10.	0.00	04.0	00.0	04.0	64.0	0.52	0.87	0.05	1.09	1.42	1001
	;		į									1.35 AYB
	° E	<b>507</b>	152	296	350	430	125	631	2	870	733	129
		1991		00.5		20.62	7.64	10.81	15,35	24.21	34.35	40.49
	570	1110	0.47	25.0	7.0	9 4 6	1.63	2.15	Z.62	# 6 # 6		12.05
		•	!			1		2			2	3-31 449
	AVG. 3245	96.95 326	823.86 335	25. 20°191	126.10 324	4VG. 224599.95 326823.86 335197.02 335126.10 324697.72 321476.25 324613.61 316026.61 313682.56 307961.74 325394.09	176.25 324	613.61 316	026.61 313	682,56 39	7961.74 32	

B-32	
TABLE	

156.00 NO. PCT. DT. STD.											
PCT. DT.	:	;	4,	:			•	•	•	01.0	1 7 10 7 7
STO.	00.01	2 °	) C	9.	3,00	) (*)	•	•	•		12
10 S	<b>-</b>	•	•	- (	?	n ;	n (				4.12
STÖ.	00.0	0.0			V .		, i	0 0	- C		
STG.				00.	200	9 0	9 0	9 6		2	9
	00.0	9		000		0	00.0	•		•	1.70 AVA
	-	-	•		¥	•	đ	17	12	54	
2	10.0	ָרָיץ.	0.02	. 6	0-04	- 0-0	P. 0.7	41.0	0.18	97.0	2.0
	100	100.	1000	1.00	1.00		900	7-06	1-10		95 e I
100	0	90.0	0.00	6	00-0	00.0	9	0.24	67.0	0.65	38.0
	•			•	}						2.15 AVB
<b>%</b>	gard	_	~	•	•	13	2	31	ţ	;	7
CT.	10.0	0.02	0,02	90.0	96.0	0.11	0.15	4.27	0.38	0.49	1.0
7.	1.00	2.00	1.56	1-17	1.11	1.08	1.66	1.10	1.13	1.39	1,42
<b>ST</b> 9.	00.0	9.00	0.50	0.37	0.31	0.27	0.23	0.30	6F.0	1.48	
;	•	•	•	,	:	;		į	*	ď	1.96 AVE
2		→ !	٠,	- 1	2 :	<b>S</b>	2	\$ ;	9	200	ñ
• •	10.0	20.0	20.0	90-0	01.0	4T-0			n :		
ė	1.00 000	2.00	200	1014	02-1	1.20	1-15		12.0		
<b>8</b> 10.	9.0	00.0	96.9	6 T P	•	•	97.0	7000	n e		24 AVE
9	•	•	•	•	;	7.	:	7	1	ů	
		- 5	9.0		1.	0 1		0.11		9-18	
					1.27	25	3	1.21	1.33	1.59	3.5
			9.10		A . 0	7			1.12	59-1	1.67
5				7			161		:	:	1.72 AVE
9	~	M	<b>U</b> D	12	91	22	30	47	3	29	~
J	6.02	0.03	0.05	0.10	0.16	0.22	0.30	94.0	9.6	0.87	3.0
1	1.00	1,33	1.20	1.08	1.25	1.27	1.27	1,23	1,35	1,63	1.73
STO.	00.0	14.0	0.0	0.28	95.0	0,62	0.57	9.55	90.0	7. 3.	
			i		ļ	ı		;	;	;	1.96 AVG
9	~	, (1)	en j	13	17	42	2	25	31	2 8	2:
<u>.</u>	0.02	60.0	50.0	0.11	0.17	0.24	0.33	96.0	6,73	54.0	60.1
<b>1</b> .	1.00	1,33	1.20	1.08	1.24	1.25	1.24	1.24	6F.	1.67	2
STD.	0.00	0.47	0	0.27	0.55	9.60	0.55	9.00	86.0	1.66	
								į	,		1.56 AV
Š	2	• ;	•	*	61,	72	37	in i	9	23	2:
֖֖֖֖֖֖֖֖֖֖֖֓֞֡	20.0	0.0	91	0.12	91.0	12.0	7 P P	, i	9.0		
	1.00	5.1 5.1	~ * * * * * * * * * * * * * * * * * * *	1.07	1:2	1.26	1.24	7.0		1001	100
STD.	00.0	500	7	02.0	7E • 0		<b>1</b> 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	•			97 140
5	•	•	•	•	2	2	9	\$	12	7.5	
1	0.0	0.0	0.06	9.14	0.20	9-29	0.40	0.61	69.0	1.12	1.26
	1.00	1.25	1.14	1.06	1.19	1.29	1.28	1.38	1.56	1.87	2.03
STD.	0.0	0.43	0.35	0.24	0.50	0.50	0.55	0.67	1.03	1.81	
					i			į		ì	1.95 AVG
9	~ ;	• ;	- 6	11	នុ	E :	P* •	20	5 2	2 =	
į	70.0	5 .			7.	700	7				
	800	1.25 62.1		# 6	77.1	1.26	1.20	74.0	70.7	9	P. D.
n		,	•	)	:	•		}			1.94 AVE
Š	138	166	217	<b>5</b>	349	614	694	537	7	483	97
Ċ.	1,23	1.5	2.08	2.05	## n	5.47	7.45	10.62	14.94	19-86	92.22
70	1.12	1.16	1.20	1.27	1. 0.4 0.4	100		2°48	EE.	4.0°	
570.	_	d. 39	24.0	0.49	0.62		0.39 U.42 0.69 U.62 U.81 L.72 Z.44 3.98 7.939	1.72	× × ×	30.5	7.00

						TABLE B-33	-33					
				SUBJECT	PARAME TO COMOI	PARAMETER INTERACTION SUBJECT TO CONDITIONS RMIN #		366 DE65 225-00 LANDA	•0.09			
JARAMETER DELTAR	4 DELTA	œ				TABE NO.	-				X PARA	PARAMETER A
		10.00	8.10	04.9	4.90	3.60	2.50	1.60	9.30	0.40	0.10	Ŝ
106.00	8	0	0	9 (	~	NO.		13	2	35	2	ı
					20-0	***	10.0	01.0	67.	92.0	9.50	<b>.</b>
	<b>3</b> 70		9.00		97.0	00.0		0000	0.20	0.17	97.0	
200-00	Š	-	^	•	•	Ç	2	*	5	¥	9	
	Ų	0.0	0.02	0.03		0.10	6-15	22	0.43	0.65	4	•
	D.		1.00	1.00	1.00		1.00	1.00	1.08	1.08	1.38	
	ST0.	0	0	00.0	•	0.00	•	•••	4.0	0.32	0.E	•
300,00		m	•	•	12	19	8		76	114	132	•
	, . , .	0.05	0.0	90.0	0-11	0.17	0.26		19.0	1.04	1.0	
	i E	- 0	61.5	1,75	1.17	1.11	1.10	1.07	1.01 4.0	1.14	1.20	-
				•	<u> </u>				9			
400,00		S.	Φ	•	<b>6</b>	27	7	55	z	141	163	_
	į	5 · 0 ·	90.0	0.10	0.18	0.26	6 .	<b>1</b> 6.	6.0	1.39	7.50	<b>.</b>
		07*1	10.53	7.4	91.0	61.1	1.17	<b>1.</b>	07.	1.23		
	Š				•	•			20.0	000		: -
500.00	Š	<b>W</b>	•	11	25	36	45	69	110	163	187	-
	į	50.0	- 0 · 0	11.0	0.21	0.30		9.68		1.7	2.28	Ä.
	, d	07.0	47-0	29.0		22	1.56	1.23	1.25		1.533	
	,							16.5	7			-
900,009	2	~ ;	21	<b>4</b>	2	76	9	2	126	181	285	~
		90.0	01.0	0 T	9.56	FE .		60	7.36	2.07	2.73	'n.
	9	56.9	04.0	65.0	1.10	95-9	1.58 0.68	6.53	100	( 0 · 0	24.1	-
				1	•	•			;	:		
704.60	ÿ	•	2	<b>*</b> :	96	45	9	65	137	193	<b>*</b> 2	~,
	į	9	90,1	00	0.26	•	9.0	1.00	1.56	2.37	48°E	-i -
	10.	5	0	65.0	94.0	95.0	9.0	0.70	0.71	10.1		•
	,	1	,	,	,			•	•	•	•	-
	2	۲,	=======================================	2	<b>F</b>	<b>L</b>	21	103	152	248	554	Α,
		1.14		1.27	1.16	100	1.29	1-12	10.0	1.63		Š
	570	6.35	0.39	0.57	0,45	0.53	99.0	0.74	0.74	1.1	1.69	
606.80	Š	•	2	20	7	š	74	-	191	217	233	
•	2	0.08	4.0	0-20	0.37	3	. 6	1.26	2.00	3.04	-	•
	10	1.25	1.23	1.25	1.21	1.24	1.39	1.4	1.56	1.17	2.15	÷
	£10.	9.6	98.0	0.62	0.42	0.57	0.71	0.0	•	1.20	7	₽.
1000.00	Š	•	*	21	9	8	9	121	166	335	737	^
	Ļ	0.06	0.14	0.21	05.0	6.50	*	1.40	2.20	3.34	4.37	٠.;
	70	1.25	1.23	1.24	1.20	1.25	1.37	1.45	1.6	1.69	2.31	~
	570.	99.0	95.0	19.0	6.5	0.57	0.68	0.82	00.0	1.30	 9	'n.
LIMIT	9	472	*	637	798	693	1157	1352	1520	1456	795	•
	בַּ	7,53	10.6	11.03	14.21	18.70	24.53	33.15	46.41	65,83	87.93	3
	10	2.00	5.09	2.17	2.23	2.43	2.66	3.07	6 m	90	13.86	1130
	STO.	1 . 09	1.22	1.33	1.50	1.75	2.01	2,59	3.65	5.65	16.51	198
	AVG. 42	. 18.3724	415075.90 4	02475,79 3	87834.31	AVG. 424575.81 415075.90 402475.79 387834.31 376537.15 355493.06 348421.07 319932.60 308431.45 297701.02 302288	55493.06	340421.07	19932,60 3	108431.45 2	97701.02	302288

	BEE KASE
B-34	
TABLE B	THATOLOGIA
TA	DADAMORD
	4

						5	•				9	*				4	•				8	,				5					9				Š						9				ZAT	ì				AVG					5 2
PARAMETER A WJDF		- ;	1		20.1	87.0				1	7 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	1.20	? ?			4 4 4		3	1.15	0.50	1.53 A		9.82	1,32	0.63	1.36 A	9	0.98	1,46	0.76	1,32 A	87	1.17	60.1	10:1	I'de ve	<b>:</b> :	?		10.		2	-			101	1,72	2.14	1,41	1.48	421	40.49	12,05	200	
X PARAME!	•	2			, de	42°0	ř	•	7	D F	216	;		,	1 2 2	2	G		4.1	0.52		29	0.70	1,31	0.58	•	74	0.84	1.42	99.0		77	1,01	4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1.03	;	2	910	717	1,05	9	, T				ĕ	1,47	2.02	1.36		715	34,38	6,83	4, 50	4772,45 3
		•	٠,	10.0	7817	1536	ij	7	21.		0 1 6 2	;	•	1010	7 0	4140			1.18	0.45	•	4	0.46	1,71	0.45	•	20	9.50	1,25	0,51		66	0,000	1,47	0,61	•			1,50	99.0	**	9 6		7 6	1011	9	66.0	1.80	1,25		783	24.61	3.04	25 4 5	1523.40 34
00.00		)  -	,	6	1.2P	0.40	•	•		7	10.0	;	7	7 7	7 .	7.663	36		1.26	0,40	•	30	0.27	1,17	97.0	•	35	0.34	1,20	0.47		9	0.42	1,32	0,69		* :	**	A 7 1	9,78		* * *		0 0	24.10	40	9,0	1,63	0.94		669	16.63	2.98	62*2	75.07.14
225,00 LAMDA=	;	7 0 0	N (	70.0	1,00	0.00		٠,	* * *	-	00.0	;	2	2 .	2 4	91.0	•	4		0.56		46	0.15	1.19	6.53		1.0	97,0	1,28	96.0		25	0.24	1,36	0,71		300	97.0	100	90.0	į	97		1.00	/c 10	13	0,38	1.50	59,0	•	589	11,66	2,47	1,83	FE 98. 740+
225,0		12	<b>→</b> ;	7 0		99.0	•	• ;	200	30	10.0	•	•	9 6	2 6	33.60	:	1;		6.57	-	19	1.12	1.15	N. C	•	14	97.0	1.21	0,56		172	0,16	1,33	0,79		44	200	1,52	0,73	ţ	2 6	9 4		11 4 0 4	33	3,26	1.50	60	•	503	9.49	2,12	1,48	CAST RR TA
SEE SEE	TAPE NB.	2017	<b>5</b>	9	0000	0,00	•	N (	2010	1.00	00.0	•	•	0 C	200	20.7	•	•		i d	•	=	11.0		00.0		11	0.43	1.18	0,39		13	0,13	 K	0,58		<b>*</b>	1.0	1,29	85.0	,	14 to	6114	1.20	66.10	50	6,20	1,25	2	•	459	6,37	1,86	1,14	ACTS CALLER DE FORTACE DE CONTRA DE L'AUGUST DE AGUSTA DE AFFORT CO 4-FAZES (Y GRACIE) CE FOSITIF DE STITUTE DE
TO CONDITI	•	3 * •	9	000	50.0	70 0	,	rt ;	10,	20.4	36. 3	,	• ;	2 .	200	3030	•	<b>.</b>	, c		-	4	9	1.00		3	.6	0.07	113	35	Ī	•	<b>6</b> 0 0	1,2%	6,42		0.	010	1,30	0.46	;	#} \ #4 \ 6	210	2:	7.67	:	44.0		G 4.5	•	379	56° <b>T</b>	1,65	181	1
SUFUECT	,	3	13	20.0	000	00"0	•	<b>+</b>	10.0	20.4	000	•	7	70 ° 0	10 10 10 10 10 10 10 10 10 10 10 10 10 1	30.00	k	,			2	•	o et	200		3	•	90'5	1117	0,37		9	90,0	1,33	0,47		•	Ø :	1,33	U . 47	,	٠,	70":		C . 1 .	4	0 C. C		W **	•	331	3,88	1:47	1240	4 64 66 6:
	;	01.5	6	50.0		00°3	•	H ;	16.3	1,00	c • 00	,	<b>~</b>	70.0	3 + 1	ត្ត រ ្	•	?	70.0	) E	2	•	2			•	•	60.03	1.00	000	•	4	40.0	1,25	6,43		•	* 0 * u	1,25	£,43		4	÷ .	2,53	6,43	ц	20.0		4.0		271	2,88	1,33	5,58	**
	*		0	9	ວ ເຄື່ອ	0,10	,	-4	Į,	1,10	0,10			13.0	1,10	נים	•	<b>→</b> ,	12	9 ti	<b>3</b> 7 7 7	-	1 2	1 5		3 4 5	-	ם.נו	100	0.0	•	N	23 0	1, 00	0,10		:\4	E .	1,60	010		<b>~</b> ;	7 to 10 to 1	D	ن ت	•	7 N		3 C	-	22.3	2,23	1,25	1410	
CELTAF			<b>L</b>		• 1	57.E		w.	• • •	# - 1	215	•	u (	ا را ا را ا:	٠ ا	SIL		u U			<b>a</b> 1 . 0	4			1 1 1	11.0	ų.			STE.	•			1,1	STE		, E			STE		, KE	֡֝֜֝֜֜֜֝֜֝֜֜֜֝֓֓֓֓֓֜֜֜֜֝֓֓֓֓֓֓֜֜֜֜֓֓֓֜֜֜֜֓֓֓֜֜֜֡֓֜֜֜֜֡֓֡֡֜֜֜֡֡֡֡֓֜֜֜֡֡֡֜֜֜֡֡֡֡֜֜֡֡֡֡֡֜֝֡֡֡֜֜֝֡֡֡֜֜֝֡֡֡֡֜֝֜֜֡֡֡ ֓֓֓֓֓֓֓֓֓֓		51E.		היים היים		- 1 1	•	,	1		SIE .	
PARAMETER DELTAR			() () () () ()					200.002				;	300 005					440					30.00				999					750,00					20 * 848					00.006					1000.00				1111				

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	TER A WJDF	LIMIT	27	27.	67.5	97.4		0.29	1.38		1.79 AVB	<b>.</b>		1.47	1,81 AVG		99.0	0 th	1.89 AVG		0.83	# ! # !		71	0.98	1,73	1.74	1,50 ATG	1,05	1,76		1.92 AVG	1.17	1.92		1,94 AVG	2,40	2.03	1.94	1,91 AVG	90	200	2.00	2.02 AVG		22.76	
	X PARANETER	0,10	7	RC 0	200		52	Š	1,29	4	;	•	٠,	2.70		r.	ŭ.	1,70		3	0,71	1,39	9/10	72	0.84	1,46	96.0	**	n. 91	1,50	96,0	•	1.01	1.57	1.03	;	7 7	***	1,13			1,10	91.		488	20,00	7.1
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- d. Pulse Altitude Line (R-H)
  - i. Range acceleration (ARDDOT)
    - (a) Nose sector (AI radar coverage) Table B-37
    - (b) Tail sector Table B-38
    - (c) Full sphere Table B-39
  - ii. Azimuth line of sight acceleration (AWKDF)
    - (a) Nose sector (AI radar coverage) Table B-40
    - (b) Tail sector Table B-41
    - (c) Full sphere Table B-42
  - iii. Elevation line of sight acceleration (AWJDF)
    - (a) Nose sector (AI radar coverage) Table B-43
      - (b) Tail sector Table B-44
    - (c) Full sphere Table B-45

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1400.00 NB.	22	58	43	3	97	140	150	134	121	122	~
	0.26	0,34	96.5	0.99	1.52	2.49	3,21	3,76	4,05	4,17	4.27
<b>1</b>	1,50	1,62	1,70	1,82	1.07	2,23	2.68	16° N	80.00	<b>4</b> . 24	4,73
STD,	99.0	0,85		1,10	1.24	1.54	1.80	2,79	3.07	3,20	in.
						,				ļ	74.68 AVG
1400.00 NB.	23	31	<b>L</b> 3	*	107	136	165	190	971	134	
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מל	1,57	39.1	1,72	N .	20.1	2.25	2.76	66.2	1	70.	2.12
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Ė	7.5	**		*	9.0	7.47		•	45.4	5.14	5.63
- E	72	40	10	1.10	2	5.65	2.02	3,08	4.00	3,72	4.11
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LIMIT NB.	302	393	467	631	782	913	954	119	169	967	421
	3,77	5,38	78.7	10,39	15,08	21.80	28.89	34.48	84, 60	29.76	40.49
Ed.	1,57	1,72	1,87	2.00	2,42	2.99	3,92	5, 31	7.24	80°0	12.05
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	9444	DANA MATERIAL	LIMIT	7 :	7.0	0.42	76.47	7	0.77	1.50	 		2 2		46.0	74.55	<b>:</b>	1,72	2,63	Z.3	75.5	200	N. D.	2.37	79.01	87	2.41	8.47			27.4		2.6			3.21	N.	2.69	40.4	3.40	4,30	2.93	82,58	104	7		61.17		22.76	8.17 4.55		6942.96
			2,00	7 !		45	•	•	0.77	1.50	1.16	ŗ			. 4.3	•	82	1,70	2,00	50°Z	3	1.97	2.94	2,17	,	68	2,59	90,0		:	2,71	17			103	3,17	8 . BS	2,57	404	3,56	4.09	2,84	į	10 E				389	22,40	7,72		6928,47
				9 :	0	0.42	•	<b>8</b> 6	1.75		1,09		76		170	•	18	9.0	2,2	7 · 1	**	4.02	2.86	2,67		0	2,31	3,22	Z 2 3	585	2 4 6		7.57		106	3,09	90° P	2.46	***	84.0	3,80	2,66	•	977	4 15	7.0	7017	456	21,52	10.0		6916,54
	40.00		18.00	22		0.41	•	s S	9.0		0.45	:	12		100	•	ž		2.2	1.	:	7.7	2.61	1,53		<b>1</b>	21.2	2.77	1.69						118	2.78	2.95	2,61	4.20	3,13	3.94	2.13	ļ	139		20.0		552	10.44			6F35.78
į	ATL 10 LAMBA .		32.09	ä	A		•	7	75.0	1.30	U. W.	9	, v				Έ.	1.26	2.15	4.3	ä	1	2.30	1,47		6	1.62	7.	1.80		200	7 7	1.76	•	115	2,40	2.62	1.87	121	2.69	2,63	1,93	ļ	Cri c	27.6			593	16.81	2	10'3	6734,37
œ .	225.	4	50.60	22	¥.5	. <del>C</del> 3		6.5	5,6	200		2	7.0		1.22	  -	3	¥ ;		10.1	22	1.20	2.68	1.39		25	4	12.2	9	6	4.96	-	99.4		106	. 98	2,23	3,75	132	2,12	2,18	1,70	į	127	200		•	909	13.53	2	4.	6631,39
TABLE B-38	TO CONDITIONS WIN A	TAPE NO.	72,08	A .	1.	0.4		tin i	e c	1,32	20.5	2	19		1.26	•	S.	6.0	2 :	1011	95	96.0	2,63	1.40		Ç. ;	4	10.2	1,10	76	1.24	2.04	4	•	9	7.7	7.07	1.41	136	1,65	1,95	1,39		A01.	200	25		553	10.43	7,00	•	6612,39
L	TO CONDITI		98,00	15		0,28		12	6.20	1,19	<b>60.</b> 0	N.	0.38	4	6.0		44	0.57	20.0		5	0.65	1.59	0.97		20	<b>9</b> /40		0	6.3	6.65	1.68	66.0	•	72	96.0	1.7	<b>6</b> 0 <sup>6</sup> 1	8.5	4.54	1,68	1,67	;		1 T	1.23	,	566	7,63			6704,25
	SUBJECT		128,65	• •		00.0		•	19 19 19 19 19 19 19 19 19 19 19 19 19 1		2	4.7	0.18	. 35			32	57.0	1	7	9	40.0	30	0,85		32		76.1		9	0.40	66	6		;	0.56	9	* D * H	87	0,72	1,58	6.05	•	:	1.66	0 1 1	:	402	5,2G	* ·	•	6926,55
			162,00		- C	00.0		Cu i	(V C	-	2	7	90.0	***	ري د د د	,	01	9 6	9 4		11	0.12	1,36			91	1	7	000	2	0.21	24	50.00	•	24	6.25	1.29	•	O.E.	5,32	1,33	04.		4 6	9		•	240	9	, d		7325,85
			200,08	•		00.0		9	9,0	3.0	2	2	6.02	1,00	0.00	,	,	20.0	9 C	•	•	6,05	1,20	0,40		<b>.</b>	9 4	671		9.	0.10	1.20	0.0	•	12	0,12	123	0 °	15	91 0	1,33	0,60	•	1	1.31	96.0	<u> </u>	213	25	# C	•	7713,02
	ARANETER AR BOX	1				STD,		400.00 NG.			100	600.00 MB.		1	STB.			1	. E	3	1500.00 NB.		1.5	STD.		1200.00 48.			<u>.</u>	1456.00 he.			STD.		160G.00 NB.	ב פ	<u>.</u>		1800.00 NB.	PCT,	E3	, U			L L	578	<b>.</b>	LIMIT NE.	֖֭֡֞֞֝֞֜֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֡֓֓֓֓֓֡֓֡֓֡֓֡֓֡	֝֞֞֝֝֞֝֞֝֞֝֓֓֓֓֓֓֓֓֞֝֞֓֓֓֓֞֡֓֓֡֓֞֝֞֓֓֡֞֞֡֓֡֓֡֞֡֓֡֓֡֞֡֓֡֡֡֞֡֡֓֡֡֡֡֡֡֡֡		AVG.
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11 14 14	0			SUBJECT	TE CBNDIT	IEN INTERAC	116% 360 225	DEGS LAMBA :	00.09		2	
	r i i i					TAPR	+				Ę	TEN ANDON!
		200,00	162,00	128,10	98.00	72,00	56,30	32,00	18.00	00.4	2,08	LIMIT
	• •	40	17	28	47	65	96	118	137	147	153	156
-	زز	80 g	đ.	9,26	0.45	e. 65	96.1	17.7	1.48	4 0 62	1,67	1.72
		1.25	1,12	***	1,21	1,25	1,25	1.28	1.35	. 30 . 30	1,37	1.38
-	# T	99.0	0.47	44.0	0.62	0.61	1.58	0.61	0.88	1.05	1.03	1.03
00.00		1.2	28	53	87	125	160	188	263	205	210	211
		12	5		6					1.37	N. 47	
		1.25	111	94.4	1.28	80° 1	1.56	1.72	10	2.36	2.07	2.11
٠,	STD,	9	0 41	9,0	77.	0.97	40.4	1.27	1,72	1,69	1.89	2.08
		,	•		•		•	•			. 1	72,94 AVG
00.00	9	<b>5</b> 0	€3	4	117	153	192	234	237	227	526	225
••		0,28	/ <b>*</b> a	ದ ಕ್ರಿ	1,46	2,18	60 60 60	4.02	4.78	5,17	5,39	5.51
•		5 F 3 F	F 647	F 4 5	1,58	1,78	2,01	2,15	2,53	2.00	50.0	3.07
		80°D	7.61	1,10	1,00	1,24	EC.1	1.63	2,34	2,73	20.0	27.5
6	5	72	i			•	, 20	376	,	346	136	78.27 AVG
3		0 5		? ;	907	701	107	607	107		65	679
-				1911	1,93	A ( )	21.0	7,4	6.17		1 A A	† P. 1
•	. C	1 . 5 V	0 K	) O	1.01	4 4	K.13	9 4 · v		3 P	n e	2 M
		• •	•	5	7	7	7017	1:03	2019	2	1	
00.00	e d	4.4	æ	112	163	201	296	285	273	252	237	224 AVG
	Ž.	0.53	4	5.5	2,43	3.50	76.7		1 2	. 26	<b>8</b> .40	1 60
		100			7 4	1.0	100	2.2		4	7	200
•	STD.	0.00	26.5	1.01	1.18	1,50	1.00	2.10	90	2.67	4.34	4.70
		•	•	•	•	•	7	-	•	•		32.56 AVG
90.00	, ₩	5.4	4	137	190	232	293	316	266	260	238	
-	ن	69 0	1,10	1,92	2,97	5.3	5. 9d	7,55	8,85	9,55	6	10.11
		1,29		1,75	96.1	2,29	2,04	2.0	10 H	4.00	2.2	2.7
			1.0	1.10	1,31	1,04	. A . 4	9217	5.37	70.		
0	9	13		1	216	255	131	110	101	234	241	65,66 AVE
	,	) M	101	2.30	1	0		200	10.24	76.87		24 25
			**							4.42		4 4 5
•	STD.	0	100	1,22	14.1	1,73	2.00	2.42	3.92	4.29	5,35	.0.0
		•			1			)				86-93 AvG
690.00	•0∗	72	114	169	240	290	342	376	336	291	549	227
-	מיי	, 6° D	1,55	2,60	90.0	20,00	7, 92	10.04	11.66	12,61	13,12	13,36
•		200	2, 2	2 .	76.37	7,	2,0	٠ د د د د د د د د	67.			· ·
			20°E	1,24	1,40	1.1	21.2	2.02	44.0	• 7	16.9	7.52
000	2	44	1	101	240	111	4.82	707	482	200	25.4	024 450
-			2	00 Y	4.46	6.34	4	** 28	13 43	14.14	14 68	1
	ü	9	9 7		2,08	2.40	2	N. 50	4	10	7.33	60.
-	510.	0,97	1,07	1,27	1,48	1.74	2,16	2,61	3,71	4,85	6,78	8,45
							,	1		,		89.18 AVG
90.00	₽9,	100	154	218	300	366	432	428	377	311	524	
-	, ,	1,32	2,10	3,61	5,08	7.17	11,01	12,68	14.70	15,87	16, 47	16.80
	ä	1.65	1,71	40.	2,12	2,46	2,93	3,71	6 . ·	9	6,15	97.00
-	510.	96.	1,56	1,79	1,49	1.78	12.2	2,75	3.93	5,10	7,60	r, 01
	9	273	•	1001	4470	1674	4644	407		707	•	59.93 AVE
- <b>-</b>	1 2 2	14.01	18.74	25.24	100	44.02	100	74.13	86.05	04.10	68.41	00 00
		2,08	2,30	2,59	2 98	5,58		6,23	9.79	19,08	62,89	1138,18
	313	1, 35	1,67	2,01	2,40	3,00	4,12	6.18	74.0	22,55	71,25	798,41
	•			4			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,					119.44 AVG
-	, D A	7194,85	6988,67	6783,98	6659,53	6602,98	997,66	6686,25	5829,62	6952, 37	7027,21	7344.91

1 25.6 LANDA. 225.6 LANDA. 225.6 LANDA. 226 1.256 1.356 1.356 1.356 1.357 1.356 1.35	TABLE B - 40  TABLE B INTERACTION  TABLE  TA	TABLE B-46  SUBJECT TO CONDITIONS PRIN W  6.48	### A Parametria Interaction
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TABLE B-41

				SuBJEC	PARAMETER INTERACTION SUBJECT TO CONDITIONS BRING	TER INTERI TYONS RMI		OFF TAIL	40.07			
PARAMETER AB R-H	- A6 P-	Ŧ				7 307					X PARAK	PARAMETER A WIDE
		10.00	A.10	4	•			;	,			
200,00	ş	~	~		•		<b>7.36</b>			9		LIHIT
	ecT.	0.02	0.02	0.02	. A.	<b>A</b>	,	ָ י	3 :	<b>=</b> {	4	2
	7.	1.00	1.00	1.00						7.0	\$ .	75.0
	STD.	00.0	00.0	000	90.0	00.0		7.00		1.1		
					•			774			7	7.0
400.00	9	M	m	•	•	15	2	*	*	4	\$	9AU 13*7
	į,	0.02	0.82	9.0	90.0	41.0	23		3	9	•	;
	Ð.	1.00	1.00	1.00	1.00	1.26	1.21	00.	76			
	STD.	0.00	0.63	000	0.0	**	95.5	6.70	0.92	1001	1.17	1.18
	!								)		•	2.17 AVA
00.009	₽!	• ;	en i	=	15	<b>X</b> 2	<b>9</b> £	<b>*</b>	51	3	71	
		4 0 0 0		0.10	0.13	9.24	0.37	0.53	3.0	1.02	1.25	1.32
	Ě	1.25	1.20	1.09	1.07	1.20	1.28	1-47	1.57	1.68	2.20	2.26
	9.0	E * 0	0	62.0	6.25	64.	0.51	1.00	1.11	1.35	1.9	2,04
44.044	9	•	•	:	1							2.68 AVB
	2	` .		* !	2	e i	ŝ	*	29	2	16	
	· -	•		71.	B	E.O.	84.0	0.68	4	1.32	1.63	1,72
	STO.	90	0.33	96.0			£6.4	1.57	60.	2.10	2.52	2,65
				1		3			97.1	- T	2.17	
1000.00	ş	1.0	111	11	16	37	4	:	,	:	ł	2.62 AVB
	4	0.00	0.10	0.16	12.0				200	3 2		2 :
	<u>.</u>	1.10	1.18	1.18	1.13	2.7	90	94.1		7 6	9 .	2007
	STO.	<b>6.</b> 30	0.39	0.38	40	6.53		41-1		1.67	7 C	70.0
										9001		2.63 AVE
1200.00	9	E	*:	87	27	7	SS	19	18	26	•	
	: ;		51.0	87.0	• . 26	9.42	9.65		1,21	1	2,25	2.41
-		T .	1.1	27° T	1.22	1.32	1.47	1.78	1.9 1.9	2.54	3.20	3.47
	5	/ -	6.33		29*	15.0	0.73	1.23	1,45	1.76	2.47	2.63
1400,00	ě	13	17	23	=	*	.,	\$	¥	•	•	2.61 AVG
	ŗ.	0.11	4.15	0.21	9		6.72	7-0-1	1,13		73.0	7.
	Ę.	1.08	1.12	1.24	1.19	1,33	1040	1.82	2.02	2	12.5	
•	sto.	0.27	0.32	6.43	9.40	;;	0.72	1.32	1.55	2	2.4	1902
	;	į	,	;						)		2.51 AVS
30.0041	Š	<b>*</b> !	61	2	SE .	3	3	28	\$	107	105	
		2.12		77.0	60.0	n .	0.78	1.19	1.60	2.41	2.98	3.21
_	2	10.0	17.0	77.0				100	Z•11	2-85	3.56	3.0
	•		751		0	A	2.5	1.32	1.048	1.62	2.47	
1860.00	ş	16	21.	52	37	53	*	1	182		9	2038 AVG
-	PCT.	*:.	0.19	9.25	9.36	15.0	9.85	1.36	1.76	2.67		
		1.06	1-14	1.24	1.22	1.36	1.53	1.9	2.17	3.01	6	4.30
	<b>3</b> 10.	9.24	57.3	0.43	11.0	1.62	17.0	1.37	1,59	1.97	2.67	2,93
2000,000	Ş		7	8	•	ż	ł	;	1	,		2.34 AVB
	Į.	0.15	0.22	0.29	0.40	, e	72 0-02		111	121	110	*
	٠.	1.12	1.17	1.24	1.27	*	1-61		2.23	3.4	30.0	
	sto.	0.32	0.38	0.50	0.50	99.0	0.79	1.40	1.63	2.09	2.8	# # M
LIMIT	Ç.	1 28	746	116	i		;	•				2.31 AV6
	7			2.08	147	,			756	563	F84	340
	10	1.12	1.16	1.20	1.27	- T	) * ° C	0 5	79.01	10.0	09.61	22.76
	STD.	0.34	0.39	0.42	0.49	6.62	90.0	1.21	1.72	2.00	-10°E	7.54
•	9	01 0378		***							•	3.12 AVG
•		01.0500	10**158	00.200	748.43	7495.44	7127.42	6768.92	6736.19	6495,72	6626.95	•

B-42
TABLE

		TIT.	1	22.	Į:	200	111	Z.		:	2	194	Ęį		724	ž			A 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		3	.7	LE AVE	22	===		37	2	213	î =	37 AV6	121	Ą		7	*21	261	m,	15 162 Aug	52	į	2	<b>.</b>	11 AY6	2	91.	-	OF AVE
	TEN A	3		~	Ă,		-	Ä	NĬ (	<b>.</b>	• ••	wñ.	eř (	Ť	¥"	, F	m	ň (	Ň"	•	•	4	Ň,	٦;	Į.		•	**	₹,	•	Ñ	14	Ä	-		-	<b>*</b>	•		•	<u></u>	<b>Š</b>	• •	ŭ	8	1138		
ı	A SARANETER A VED	0.10	3	1.55	<b>X</b> :	;	2	3.23	*	1.7	***	40.0	2,2	g.,	747	24-9	3.26	2.81	282		30.0	14.6	•	2		-	•	275	8.0			263	12-11			£	13.52	* :	7706	309	15,28	6.19	<b>66.8</b>	200	87.93	13.86	16,51	4947 67
		*	121	7.1	20	. 10	174	<b>5.</b>	9.4		122	3.85	2.19	C/ • 1	24.5	*	2.56	1.98	36	7	2.65	2.47	•	787	41.0	2.66	•	307	2.2	2 - 7 - 7 - 7 - 7 - 7 - 7 - 7 - 7 - 7 -		328	\$		;	186	10.47	3.74	3.20	385	11.64	3.65	3.43	1456	65.83	2.06	5.85	
***			1	1.0	2		129	1	9		167	2.50	10.		20,	3.24	2.02	1.00	702		2,20	1.1	1	2			•	274	, n	7.15	i	200	E			326	7.68	2.72	26.5	359	9.00	2.79	2.59	1520	46.41	3,63	3.65	
DEES Se Lavor •		1.	3	3.6	**	į	103	1.21	79°	**	132	1.13	3; ;;	7201	14.2	2.24	1.73	1.24	111	2.67	2	1.63	(	***	e de la companya de l			222	3,72	Z-70		723	4.20	22.2		262	4.7	2.27	1661	261	90° 34	2-12	1.48	1342	33.55	70.0	2.50 N	
*** ***.	•	. 52	3	***	1017		ħ	0.0		1	•	1.18	 8		121	1	1.52	6-81	**	1	1.60		į	30	2:19	1.06		166	Z*39			195	- N			516	90°0	24.1	1.39	234	3.70	1.98	1.40	1157	24.53	2.66	2.01	
IN ENTERACI	200	1	Z	N.			3		22.1	;	2	3.	2:	:		1.01	1.20		113	1.26	1.40	9.0	į	*21			}	3				154	50.2	90.		175	2.37		1.50	167	3:6	# 1 m	1.23	663	16.70		1.75	
PARAMETI TO COMPIT		*	13	1.14	2.	•	2	00.0	1.12	3	3	-	1.17	•	1	1900	1.20		*		1.26		į	1			•	100	1.50 L			112				132	19-1		6	**	1.85	1.61	•••	798	14.21	2.23	1.50	70.00
SUBJECT		3.	=	0.14	12.1		2	-15.	1.18	16.5	**	¥.	1.19	X.	1	6.43	1.23	. 52	å	***	1.26	1.52	9	8 4		. T.	1	69				2	9 1	1.62		66	1-1	100	•	105	1.33	1.59	•	637	11-03	2.17	4.33	12 BE 12
		<b>8.1</b>	17	9.10	\$ ! 		*	£1.		Q.	2	1.22	2:	744	2	2.	1.24	6.43	36	<b>6</b> E 4	1.26	;	;	::		1.51		m (	700			9	2.3	7 0 0	•	69	0.00	,		F	00.0	1.61		541	9.03	2.09	77.1	43 OCE
,	*	10.00	•	10.0	*:		71	0.10		82.	15	6.14	1.20		8	6.21	1.18	P	ĕ	X.	1.20	04.4	}	<b>R</b> :	P .	7 - T		7		0.70	}	4 10	ň.	10.0		25	E9"0	2001	•	26	1.0	90.	6.40	472	7.53	2.00	50°T	£444 47
	AMANETER AS Nº		280,80 MO.	<b>.</b>	Ėį	• • • • • • • • • • • • • • • • • • • •	400.00 MO.	į.		.018	600.00 NO.	7.	•	•	996.66 MG.	150		STD.	1000.00 MO.	2	<b>.</b>	<b>\$</b>			į	<b>5</b> 70.		1480.00 MO.				1600.00 NO.		Ė	, ,	1806.30 NO.	ָבֶּילְ מַלְי		• 0.6	2000.00 MG.	֓֞֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	ö	STE.	LIMIT MO.		5	510.	624

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0 0 1 1 1 2			Sigueor	PAZANET TE C3%DIT	TONS BAIN E	9FF 225	vase .00 LAMDA=	60,00			; ; ;
					SH BUY					H W W W	FAXARETER & BOUF
	03'01	F+13	6,40	3°.4	3,63		1,60	06.0	0 + 4 0	9,10	LIMIT
200,00	~	23	₩)	•	^		16	20	ň	<b>4</b>	55
	2,10	20.1	(V) (C) (C) (C) (C) (C) (C) (C) (C) (C) (C	30.0 0	90.0	91.0	91.0	27.0	0.37	1010	A .
	9 C	200	3 i	)	+ i	A 0	1,63	1,23	1,03	1,00	1.55
- - - -	21.0	. n . n	<b>.</b>	30 ° 0	65.0	6210	24.0	5 T T	200	791,0	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
. 34 00'00 <b>9</b>	77	•	ī	٥	12	19	30	39	36	7.8	
	2,5	80°0	No.	0.00	0.11	1,19	0,31	0,40	0.78	1,09	1,26
, T.	C J T	3D 1	1.20	1,17	1,17	1,26	1,30	40	1,75	1,74	4.95
£. []	0,0	00.0	0.40	0,37	0,37	47.0	0,53	06.0	1.12	1,20	1.59
		u	•	;	,	ţ		•	;	:	1.43 676
30 man	n 42	n g		1 7	ED 41	20	* G	9	-	19.	
ָבָּי ביי ביי	) -		4 . 5 . 4		20.5		47.		2,11	2017	2
£ ::		0.4.0	17.0	98.0	0.42	0.89	0.94	1,62	1.89	1,96	2,27
•	•	•	•	•	•	•	•	•	•		1,46 AVG
400,00 NE.	-	٥	i pr	12	23	28	9	55	19	95	6
<u>เ</u>	40.0	0.07	11.	0.13	0,21	800	e 58	06.0	1.53	2,10	رم بع ا
	-	H . H	D 4	1.55		9 6	200	6,5	· ·	2:0	2,25
•. 		76.7		•	0	/ 6 l l:	A 0 8 5	1.22	1140	019%	40 3VE
1000.00	'n	7	15	: N	26	37	48	79	5	104	
		(E)		4	O. Se	1.51	0.75	. 12	1.02	2.65	3,06
• • • • • • • • • • • • • • • • • • •		1,43	1,33	1,35	2	1,73	96.	2,19	2.54	51.	66.10
SIL,	0,0	C * # 3	0.60	95,0	*0 * T	1,43	1,37	1,77	2,10	7.53	2,96
											1.43 AVG
1200,00 SE.	•	<b>3</b> * (	17	21	## i	47	63	18	110	115	101
ູ້ !	٠,٠		80 ( *1 (	0,724	40.	091,		1,39	0 ° °	3,14	3,63
- E	리 c	3,5	V 1	1221	1,55	7. a	1,4	C113	7017	9 6	2
7	•	•	104.			-	7387	9041	7102		1.43 AVS
1400.60 NS.	13	1.5	25	\$	39	57	7.5	95	125	131	
		E. 13	50°C	45.0	****	٦,75	1,09	1,69	2,72	3,72	4,27
<u></u>	1.53	1,23	1,21	1,29	1,41	1,65	1,48	2,23	2.73	3,56	4,73
STE	9319	6,42	0.50	0,76	1.04	1,32	1,29	1,70	2,21	06.0	3,55
											1.57 AVG
1650,05 15.	**	91	27	3.5	47	6.0	78	102	134	141	119
ີ ເ	3 ·	e In	,	7	5° 5		7,7	B +	) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) (	77.	9
- 4 - 3 - 6	-3 ( -4 (	F	32.5	1	o c	300	0 1	4.5			21.6
·		<b>3</b>	164	90.0	1 • •	116/	1,0		100		5. AVG
. 94. CT. DOB	i, t	10	53	35	51	69	80	117	149	154	127
		C.1d	0.30	0,36	0.59	\$6°0	1,38	2,16	3,48	4,74	5.45
• • i	1,15	1,28	1,31	1,37	1,45	1.71	1,97	2,32	2,93	98 %	5,38
		£.5	.55.	0,40	96°0	1,24	1,26	4,58	2.27	2,97	3,73
		ľ	u	î	ů	2	8	124	9	4	1.58 Ave
* # \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	7 1	700	15 de 10 M	2	1 0	90-1	55.	2.43	3.64	1,4.1	9
•		, ,	200	75		2.5	20.0	***	10.00	40.4	100° E
• c.	1 1	0 0	14 2 <b>(</b> )	\$ F	1.47	1.57	1.59	1,93	2,56	3,75	4,11
								į	!		1.56 AVG
		27:	122	¥.5	⊅ ! • ,	503	949	, ,	7 / F.S	(1)	124
	3	D	E C	<b>3</b>	/5.0	, ·	11,43	10,73	19.97	56.30	
•	0 1	9 4		יים יים	1 T	44.	, B.		2	20.4	5,52
•	• · · ·	;	•	•	•	-				•	2.50 AVG
	46 4 17 2 3	4441.93	17,9500	8934,43	5607,95	#383,64	8218,71	7857.98	7508,77	7374,40	7460.22

		<u>1</u> 0					_	AVG			_	!	9 ×				AVG	,		_	;	9			_	94	_			4		_			7 46				AVG		_		946	_			9 A C		_		AVG	
		PARAMETER A WJDF		•	0.37	1.15	0.45	3,31	19	0.77	1.59	51.1	2.58			70.0	2 62	91	1.72	2,65	2.30	CC. N	00'2	10	2,37	2,4	30	7	7 0	200	47	2.74	3,54	2,61	2.40	101	2.01	2.69	2,31	105	9.	4.0	2.29	ğ	* 1	10.4	2.28	349	22,76	4,17	3.5	6042,96
		X PARAME	•		n, 32		98,0		28	99.0	1.43	6,72	ş	,	101	- M	-	82	1,51	2,30	1,00	*	1.75	2.5	1,65		56	7	10.7	7/17	106	2.40	2. B4	1.83	;	114	701/	4.92	•	121	5,17	2128	7142	125	, 50 10 10 10 10 10 10 10 10 10 10 10 10 10	70.0	7.17	488	20,00	5,15		6835,85
			9		0.26	1.07	0,25		5	6,95	1,38	0.66	**	9 6		1.23	•	77	1.25	2.04	1.5	2	44.	2,21	1,61		49 ( 40 (	1,72	12.	,	66	1,96	2,47	1,74	,	113	7 7 7	1.72	•	124	2,53	4,70	7,17	130	2 8	7.7	3001	525	14,67	(N (N)	4	6649,07
	90.09		e c		0.22	4.	91.0		<b>;</b>	0,42	1,29	19.0	r r	2 6	2 4	1.28	1	9	16.0	1.9	1,30	e e	10.0	2,00	1,42		73	1,22	47	1	84	1,36	2,02	1,44	į	9 1	70,1	1.42	•	104	1,72	4.42	7.11	111	1,94	21.7		542	10.57	2.44	) 1	6902.67
	PEF TAIL			200	0,19	1.0.1	0.20		99	9 35	1,22	0,53	44			4	-	4	0,71	1.62	I. ab	ď	60.0	2,00	1,20	ı	4	1	777	•	56	1,97	2,67	1.19	•	n c	21.5	2017	•	*	121	* 4 * 4 * 4	, <del>, , , ,</del>	35	7	12.	1110	446	7,75	2,06	,	6957,98
-44			- T	7	9,12	1.07	0,26		54	0,23	1,21	0,56	1	1		300		Ø.	4,5	40.1	r / 12	42	5.5	1.62	0,79		200		4 0	,	55	0.71	1.62	2, 62	,	9	rt 0	00.0	•	70	en e	10.10		75	er (	) d () f () d		427	5.87	77.72		7263,40
TABLE B-44	PARAMETER INTERACTION SUBJECT OF CONDITIONS RMIN =		יארת הער איני איני	2 0	1 1 1	4.08	0,28	•	12	6,19	1.1	υ, 35	ď	9 00	400	25.0		33	6,36	1.36	2,74	36	C: +	60	0.54		45	D .	H = 0		45	tr.52	**	6,65	Ü	N C	* C * C	10.63	•	5.5	70.0	7 0	9	<b>7</b>	0,74		10.0	375	4,55	4 4 4 4		7463,45
=	PARAMET IR CUNDIT		ð		70.0		900		<b>.</b>	4.15	1.00	0 2 2 4	ê		4 4	1 JA 4 PC 4 CC		22	0,25	1,24	2	č	6.27	1,21	0,41		9 ; P) ;	3	217	•	34	C . 32	1,22	.D Ψ	•	.3 ( <b>7</b> F	2	24.0	•	.7	9 : C	N of	,	4	υ ,		1	21.0	3,5	* F C		7677,35
	SUBJECT			, ~	- 10 th		00.0	,	4	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1,67	7,26		· · ·	) (* * *	1 ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) (		20	G	1.15	49	22	, e.	4	46		<b>9</b>	n (	4 F		<b>10</b>	92.0	41	98.0	;	25.0	3000	0 40 6 P) 6 C	•	155 (P)	5 ° C	N 12 PIFE	,	37	9 (P	77.4		261	2,72	-4 C	2	29696
			1	1 4 4 7	0,0	100.1	00.0		э.	0.07	1, 63	0.00	•	-1 S	) r	3 C		175	01,0	1,00	2	H.	) (*)	10	6,27		0	C 1	e d		tO +·t	5.17	h +1	0,37	į	5	D	5 40 et #0 et 12	;	22	C 21	D 0		23	25.0		† • •	216	2,12	*) c	Y 6,	99,6219
					90.0		20.0	•	'n	* L = 3	(E)	ن ا ا	•	D 4	) (	3 23 2 4 4 4 4		٥	0017	1,17	201	7		, <del>,</del>	۲, نو نو		i-4 (	13 d	U 0	-	12	. 111	7131	62.0	,	<b>.</b>	9 T	• 5 • 6 • 6 • 1	-	41	, 13 V	≯ d ere id .		17	6,17	4.1	7,17	172	1,1	e e e e	2	E415, to
		PARAMETER AT PAR		6.00			1000		400,60 NE	F04		ים. בו גי		* 65 00 000	- • ·	110	,	.34 93,368		<u>.</u>		.04 00 000 +	, ,	• • • • • • • • • • • • • • • • • • •	215		1200,00 %,			7	1402.00 %%		. L.	STE		1606,60 16,	<u>.</u>	# L.	•	194 00 0091	ا د د	-1 5	1	2000,00 % 8	ָרָ מ	- 4 - 4 - 5				- 1	.,	* ()

B-45	
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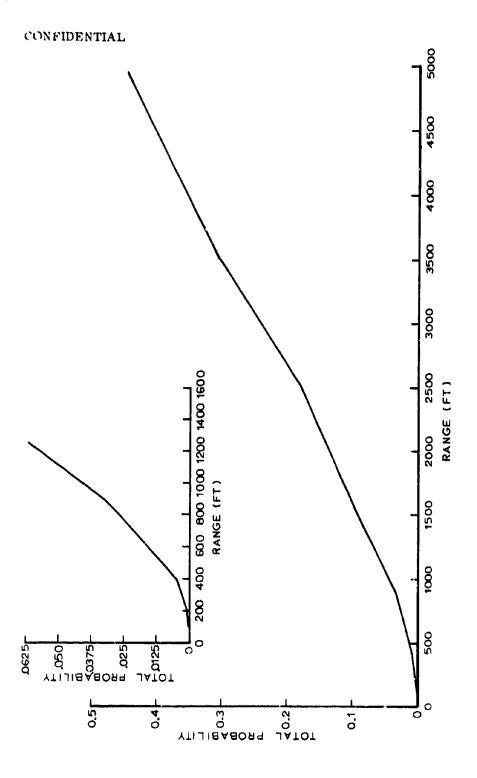
#### 6. Miscellaneous Interactions

#### a. Minimum Range

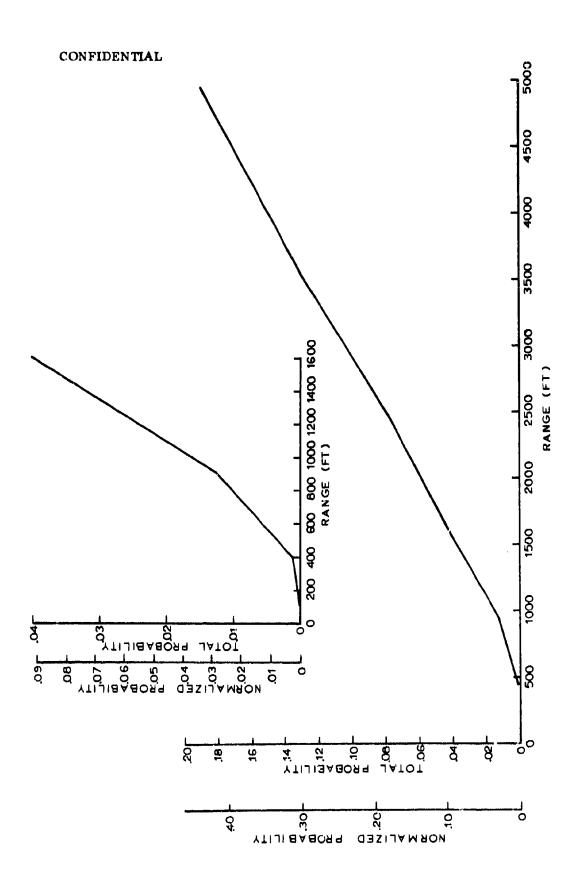
- (C) Figure B-34 is a plot of the range versus probability of occurrence for full sphere coverage. If a 0.95 probability of track is desired, 2.5% of the range data at the minimum and maximum ends of the distribution can be eliminated. Using this 2.5% criterion, the minimum range requirement is 765 ft. for a full coverage tracker.
- (C) Figure B-35 is a plot of the range versus probability of occurrence for AI radar coverage. Using the same criterion as for the full coverage case, the minimum range requirement is 1200 ft.
  - b. Aircraft "g" loading.
- (C) Figure B-36 is a cumulative probability that the "g" loading was greater than a certain value. As an example, 5% of the time the aircraft was pulling 6 or more "g's".

### c. Glint Interaction (Fig. 43)

- (C) The parameters interacted in order to give a preliminary look at glint were range versus target rate of rotation for various target aspects for AI radar coverage. Target aspect in this case is referenced to the nose of the target aircraft. The data for the 162° to 180° target aspect case represents a small amount of data. The effect of the small data base can be seen in Fig. 43 as widely varying noise on the average target rate of rotation.
- (C) Referring to Fig. B-37, it can be seen that, as the range to the target decreases, the rotational rate of the target increases. This rate increase increases the frequency of the glint, thus lessening the effect on the tracking circuits at close range. This indicates that it is possible to increase the tracking loop's bandwidth at short ranges without worsening the glint problems. A notable exception to this is the head-on case where the target is nonmaneuvering prior to a flyby. In this case, an increase in bandwidth will probably cause an earlier break lock.

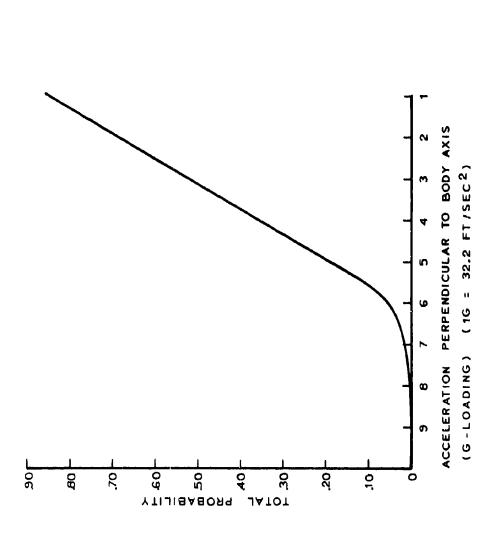


CUMULATIVE PROBABILITY DISTRIBUTION OF RANGE FOR FULL SPHERE COVERAGE FIG. B-34-



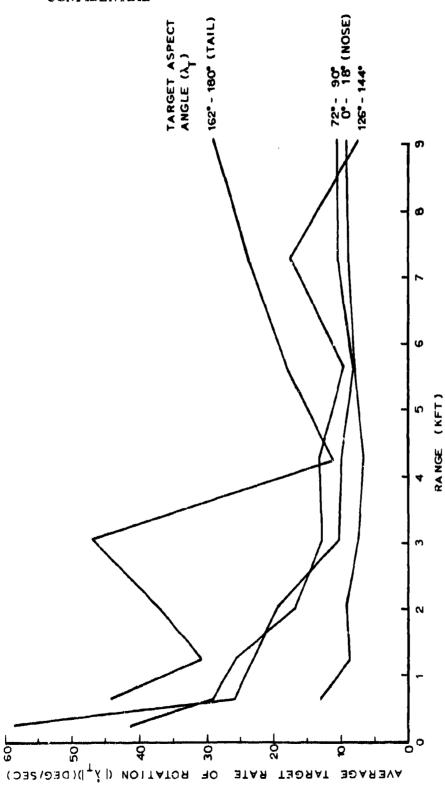
CUMULATIVE PROBABILITY DISTRIBUTION OF RANGE FOR AI RADAR COVERAGE

FIG. B-35



CUMULATIVE PROBABILITY DISTRIBUTION OF ACCELERATION PERPENDICULAR TO BODY AXIS FOR FULL SPHERE COVERAGE AND MINIMUM RANGE = 225 FT FIG. B-36 -





AVERAGE TARGET RATE OF ROTATION AS A FUNCTION OF RANGE AND TARGET ASPECT ANGLE FOR AI RADAR COVERAGE FIG. B-37-

### 7. Data

Tables for Miscellaneous Interactions

- a, Minimum Range
  - i. Nose sector (AI radar coverage) Table B-46
  - ii. Tail sector Table 47
  - iii. Full sphere Table B-48
- b. Fighter G's

Full sphere - Table B-49

- c. Glint
  - i. Nose sector (AI radar coverage)
    - (a) Target aspect angle 0 to 180 - Table B-50 (LAMB-T) 18 to 36° - Table B-51 (b) 36 to 540 - Table B-52 (c) 54 to 72° - Table B-53 (d) 72 to 90° - Table B-54 (e) 90 to 108° - Table B-55 (f) 108 to 1260 - Table B-56 (g) 126 to 144° - Table B-57 (h) 144 to 162° - Table B-58 (i) 162 to 180° - Table B-59 (j)

## ii. Tail sector

(a)	Target aspect	angle					
•	(LAMB-T)	0	to			Table	
(b)		18	to	36 <sup>0</sup>	-	Table	B-61
(c)		36	to	540	-	Table	B-62
(d)		54	to	72°	-	Table	B-63
(e)		72	to	900	•	Table	B-64
(f)		90	to	108°	-	Table	B-65
(g)		108	to	126°	-	Table	B-66
(h)		126	to	1440	-	Table	B-67
(1)		144	to	162°	-	Table	B-68
ĊŧΣ		162	to	150°	-	Table	B-69

Market Service and Service Control of the Control

# iii. Full sphere

(a)	Target aspect	angle					
	(LAMB-T)		) -	180	-	Table	B-70
(b)		18	} -			Table	
(c)		30	5 -	540	~	Table	B-72
(d)		54	<b>-</b>	72°	-	Table	B-73
(e)		7:	2 -	9() <sup>O</sup>	-	Table	B-74
(£)						Table	
(g)		10	3 ~	1260	-	Table	B-76
(h)		120	5 -	1440	•	Table	B-77
(i)		14	4 -	162°	-	Table	B-78
(1)		16	2 -	1800	-	Table	B-79

	GFF NBSE
TABLE B-46	PARAMETER INTERACTION

							9				2	5				9.				ş	9				JA:				:	9				94.				9 .				9				5				) V. G	
PARAMETER PANCE		LIMIT	37	0.31	1.05	0.23	10908,74	2 45			1 18 54611	555	12.38	2.79	3,20	9488,93 4	725	23,75	4.10	4.80	717	A CE	5.67	5.54	7922,47 A	965	37.40	7.05	6.33	1049.11	39.55	7,95	6.73	7485,95 A	566	10.14	7.10	7376.06 A	561	41. V 2	95.7	7344.02 A	543	42.52	10.	7315.23 A	445	43.79	9.71	7273.01 A	11.64
X PARAME		10000,00	52	0,21	1.04	0.20	100	172	4.4		1001	459	6,75	2,39	1,97		625	15,13	20.5	3,11	635	36.46	4.96	3.84	•	505	29,24	6,12	1.4	573	31.13	6.81	4.87	i i	וכנ	57.42	5.20		524	33,22	F. 4.	•	200	5.3.70 a 20	. · ·	•	434	34.75	 		17,13
		8100,00	2	0,19	1,04	0.20	120	, e	4.4	9		419	7.73	2,31	1.92	i	580	15,89	? (	24.08	501	24.03	4.65	3.64		574	25,52	5,57	4,10	9	27.27	6,16	4,62	ř	920	20.02	76.		515	24.21	2.5		550	7.00		•	435 -	30,70	7 1	l •	12.44
00*09		6400,00	20	0,17	1,05	0,22	140		4 4	0	•	349	6,20	2,23	1,85		492	15.41	0,10	21/0	520	17.41	4.19	3,31		531	20.50	* 1	90.9	44.8	22.04	5.33	4.24	3	116	2.50	4.42		495	D	6.63	•		70.4	47.7	•	431	25.12	2 m	,	12.52
O LAMBAR		4900,00	10	0.00	1,10	0,30	70.		1.32	7.	•	273	4.06	1,86	1,33		707	9 (	00.7	2,14	457	12.28	3.35	2,53	į	485	14,84	, es	2.78	483	16,23	4,22	3,25	,	97.	17.24	N. 4.3	•	465	20.4	3.61		457	10.14	3,73		415	108	4.24	•	13,82
ē.0	H	3600,00	· ·	+0.0	20.1	00.0	85	200	1.12		•	172	2,10	1,53	0,92	!	287	•		1,21	360	7,33	2,55	1,86		404	9.46	2,90	17.2	433	10.68	3,16	2,50	ć	524	11.70	2.72		413	12.10	5.6		409	17.12	100	; •	379	12.99	3,56	. !	56'51
BNS RAIK	TAPE NO.	2500,00	, ,	20.0	7 no	00.0	00	2 2 2	10.05	22		90	9,78	1,23	0,57	!	163	C 4	1,00	0.40	250	3.53	1.77	1.05	•	308	5.07	2,06	1,55	222	6.03	2,27	1,72	ÿ	160	20.0	1.87	•	349	0.0	96.	;	350		200		338	7,92	2,23		170 180 180 181
18 CBNUITI		1609,00	<b>3</b>	3 0	30.0	00.0	•	. 5	1.00	00.0		23	0,19	A 0.04	0,20	,	60	60°0	1	6,30	124	1.21	1,22	65.0		185	2,04	4.4	10.0	210	2,75	1.57	0,97		7.7	7.74	1.17	•	245	***	1.30	;	246	1 92	132	-	251	<b>*</b> (	1,34		22,76
SUBJECT		00,000	96	30.0	0000	0000	•		00.0	90.0	• •	•	7, A3	1,00	00.0	•	7) (F	200	1,00		23	0.19	104	0,20		5	940	1 E E	75.1	7.	99'0	1,12	D**U	q	n c	200	5.53	•	166	100	19.65	- :	111	1,14	, r.	•	120	1,27	1 4 5 ° 1		27,27
		400,00	9			2	C		00.0	00.0	•	0	00,0	00,0	00.0	,	- 6	200	200	1911	0	0.00	0.00	00.0		-4	10.0	1,00	2012	٠	10.0	1.00	0000	ú	٠.		0.40	•	no f	) ·	0.33		# C	× 0 + 0	07.0	•	16	0.14	70.0	. !	φε
		103,00	0.0	9 6	2 0	מה לה	G	0.00	00.0	93.0	•	0	0010	00.50	00.0	,	<b>-</b>	200	2 0	2012	0	3.00	00.0	000	ı	<b></b>	00 0	3 C	) )	•	00.0	0 10	99 10	•	<b>3</b>	90	00.0	•	<b>53</b> (	3 G	20.0		(3) (C)	3 (2)	2 5	•	0	ຄວ້າ	00.0	,	ت د د
AAMETER JT-DET		,	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		; ;	21.6	2.00 %6.	PC.		STE	•	4,50 NE	7	<b>.</b>	Sıtı		6.00 AE,	֝֞֞֞֝֞֞֞֝֞֝֞֜֞֝֞֞֜֞֝֞֞֜֞֞֜֞֞֞֞֞֞֜֞֞֞֞֜		31.6	12.5¢ NE.	בים	1	STE		18,00 AE;	្ត្រី	1	ה ה	24 50 AF	100	EY.	STE		54.00 AC.		STE		40,50 NE.	• • • •	STE		50,00 he,	֓֞֞֞֞֞֞֞֞֞֝֓֞֞֞֞֞֓֞֓֞֞֞֞֞֝֓֞֞֞֞֞֞֞֝֓֓֞֞֞֞֝֞֡ ֞	2.5		LITT RE.	р- р (Д .	2 4 C	•	• 0.4 <b>4</b>

						:	7				AVG				AVB				AVA	}			2					448				7				AVE			2				AVG	! :			<b>7</b>	
	PALE STREET		LINIT	À .	1.12		9464,90	**************************************		2.45		205	6.28	7 20		154	12,64	, , ,			17.68	4.63		157	20.26	3.63				6.82	•		452	6.27			25.42	6.7			23,94	<b>6.9</b>	4754.47	-4	25.57		21	,,,,,,
	7		19090.00	::	9		,		77.4			569	4.79	22.2	•	787	10.12	2.2		424	14,17	4.14	7.1	49.	16.47	7	4,33	-	627	5.21	4.47		424		4.63		19.91	3, 16	4.76	*0*	20,02	25.4	•	374	21,62	5.37	16.00	• • • • • •
			8100,00			0010	1			7		254	4137			366	<b>7016</b>		,	***	12.61	60'0	2461	467	14.74	7637	4114				4.24		422	5.82	4,32	•	17169	5142	4146	481	10,18	216		376	19,75	215	17.66	
	09'09		4400.88		9	0.00	8	26	704	7		214	16. in	7. E		312	7,21	68 2	9119	367	20.10	d, 45	7.4	378	12.81	76 7	3,73		245	***	3,01	•	262	4.62	2,90	:	24.76	4.77	4.09	282	15,24	8,0	11:	151	2:3		40.48	•
111	0:00 LANDA =		4960,00	`		90.0	:	72		**		151	2,24	47.1	}	243	90.4	2,47	K123	311	96.9	2,61	2,71	130		3,17	7. O.	į		10.77	20.7	ı	892	50.0	3,12	į	11.66	3,86	3,31	155	11,52	4 1	99.	622	12,95	3,52	26.96	
		-	3696,00	* *		0.00	;	## ## ## ## ## ## ## ## ## ## ## ## ##		- C	,	92	1,17		•	164	2,53	7	71.4	225	8,89	2,17	1,94	265	5.07	2,49	2,16			25.5	2,26		316	2.62	2,19	;	7.21	2.50	2,33	326	7,61	2,92	£ 5 3	322	9,96	2,56	27.40	. 44
TABLE B-47	CONDITIONS ARIN &	TAPE MG.	2500,36	•		80.0	•	•		111		35	72.0	1001	1.1	72	9,81	1,42	1010	110	1.40	1.59	1.80	÷ 55	2.04	1,7	1,21	i	176	1.86	£,26	•	268	4.92	1,27		2.59	2,03	1,37	238	\$6.8	2,08	7.	279	5.24	1,52	17. 63	1, 2, 3
TA	TE CONDITI		1600,00	9			•	G 6				•	6	) 1	3	78	0,17	1,17	1010	36	0,36	1,23	95.0	•	0.51	1,42	98 0	•	9		0.0	ı	67	4.4	0	, ,	1 2 2 2	1,50	0.91	117	***	1,55	<b>\\\</b> .	141	7.	# 6 6 6 6 6 7	54.07	-
	SUBJECT TE		00,000	9 6		00.0	•	e e	2 0		•	•	0.0		•	**	10'0	1,00	00.00	ю	50.03	1,33	0,47	•	0.06	1,17	6,37	•	70 0	4.4	6,35	•	<b>*</b> 7	7 6 6	0,35		0.10	121	0,41	28	0,27	1,21	1 4 5	•	0,61	937	As 42	4 1 1 1 2
			400.00	<b>=</b> 5		00.0	•	<b>a</b>	9 6			•	00,0	90.0	•	•	00,0	00.0	9	0	00.0	0°0	0.00	. •	0.0	0.0	00.0		9 6		00 0	•	<b>0</b>		00.0		00-0	00.0	00.0		10,0	1,00	B 4 0	**	1110	90.0	•	
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	PARAMETER HANGE	LIMIT	71	0.61	1.07	16	512	7.57	1.65	2.09	11184.87	25.57	2.96	3,75		1551	20.00	- F	3275,56	1209	69.31	7.18		9101	29.08	9.91			\$6.50	12,39			731	15.50	17.04		609	10.14	19,58		497	94.04	24 13		=	100.00	12550.00	6945,92	14,10
	X PARAME	10000.00	4	62.0	20.1		400	4.86	1,52	1.27	000	18.65	2,54	2,54		1165		1 TO 1	•	1125	53,65	20 T	10	266	63,24	7,95	8,18	0	66.39	6	10,35	į	766	11.76	13,46	ı	661	14.07	15.59		266	75.74	10.77	14.1	173	79.94	55.00	•	14,64
		8100.00		0,37	1,02	6119	362	4,33	1,50	1,24	777	16.47	2,44	2,40	•	1084	2000	10 m		1058	46,98	2,56	0,12	971	55,68	7:19	7,52	979	60,55	19.4	9.62	•	768	10.43	12,54		674	12,29	14,50		582	19.70		17:30	214	71.63	41,44		15.15
06,04		6400.00	4	0.34	1,02	0,13	200	3,55	1.47	1,22	708	13.08	2,31	2,19	,	0 t	77 M	3.76		186	36,71	4.69	21,5	954	44,30	5.82	6,24	***	48.71	6,87	7,88	į	792	21.00	10,23		717	9.40	11.51		634	75.00	7	20.01	294	58.49	28.46		16.20
360 DEGS 0,00 LAMDA =		4964.00	22	0,18	1,07	1240	203	2,08	1,29	6,66	£2.	96.0	1,91	1,53	ì	96,	70 C	2.87	•	998	24,89	9.0	70.7	668	31,21	4,35	4.59	864	35.12	5,09	5,72		793	00.0	7.00		724	6.58	8,01	l	651	10.1	20.0	200	345	D 9 " 9 9	10114		18,30
	,	3620.00	70	00.0	1,00		106	66 0	1,12	9,41	228	4.00	1.57	1,03	, i	224	, .	1.82	•	692	14,22	2,61	10.5	763	10,01	3,13	2,93	.22	22,38	3,64	3,79	1	733	200	4,42	,	691	4.80	5.33		635	27.00	, , ,	0.00	343	ed to	10.00 0.00		22,32
TABLE B-48 PARAMETER INTERACTION CONDITIONS RMIN =	9	7AFE NG. 2580.60		0,02	1,00	•	34	0,30	1,09	0,37	72.	77	1.24	0,67		2/2	20.0	6.0	:	427	6.10	1,79	1,41	538	9,33	2,17	1,80	53.	11.85	2,60	2,31	,	787	13.00	2,69	. !	572	3,30	3,15		545	16.00	0 W	100	359	10,43	, o	, !	27,65
TA PARAMETE TP CONDITI		1600.00		00.0	20.0		•	20.07	1,00	00.0	72	0.33	11,11	96.0	ě	2	0.00	6.63	•	179	1,05	1,35	24.0	258	3,32	1911	1,33	111	4.70	1,77	1,51	,	369	200	1,76	. !	15 A	22.73	16	•	372	4, 0	94.0	61.5	317	o .	200	•	36.21
SUBJECT		900.00	0	00.5	20,00	3	0	0.00	00.0	•	ur	6	1.00	00 "	ų		71.	20.0	•	58	0.27	:117	W - 2	65	9.59	2,14	0. 4.0	e n	n 86	1,20	1,64	į	123	a. C.	64		140	7 4 4 4 4 1 4 4 1 4 4	9. F.		45	Y) 6 2 U	7 0	•	17	8	,	•	57.73
		400.50		00.0	20.0	2	Ø	00.0	0.03	00.00	•	0.0	00.0	0.00	,	9 6		20.0	) 	-	0.01	1.00	00 · 11	2	0.02	1.00	00.0		20.0	25.41	0.47	,	, ,	000	6.45		er P	7 - T	3		D5 17	71.	-1 -	?	9,		0 Y 1		12.4
		100.00	(3)	00.0	900	<b>3</b>	9	0,0	00,0	00.0	c	ם ב	000	00.0	,	e e	2 0	0 2 2		O	5,00	D. 0	3	73	00.0	00*0	0,0	c	יי ני	50.0	3,0	,	<b>c&gt;</b> ;	300	00.0		ra t	900	(2) (3) (4)			() ( -! 	) r	•	Ą	7.4.	1 L.	•	124.01
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	Ļ					AVE							AVA				AYG				AVB				AVB				AVB				AVB				7			974				AVG	
	PER LANer	_	- Tui 1	13.6	7.4	9	7	12.4	7	12:2/	4	20.27	72.19	7	3		7.0	E .	2.3	77.16	72.96	141		407.70	74.33	<b>5</b>	7.24	286.36	75.00	22		390.07	73.57	11	1138.10	796,41	62.64	11 96,98	1138.16	796.47	=======================================		1136.12	15.29	7.14
	X PARAMETER	44.7		13,66	7.5		197	76.	11.46	920	48,18	5,5	14.61	438	9.79	16,74		325	76.01	77.10	****	141		107.70		16		286.36	•	22	267.50	800 BA	;	11	1138.14	798.41	;	11	1130,10	798.42	41	20.05	1135,18		
		•	328	13,19	5,13 6,13		<b>;</b> ;		1111	262	47,06	86 °07	11.41	167	64,24	75.00		405	76.37	?		292	72.87			173	70.07	72.33	•	147	17.11	12.50	į	121	17.74	14.3	,	47.70	87.76			47,36			2116
			502	11.74		•	77	7.6	10.78	966	48,94	2.0	12.33	522	56.62	14.07	•	478	72.03		66.73	966	55.15	No. 95		252	16.79	79.65	•	271		43,82	;	202	42.58	44.54	-	90°0	42.58	44,54	265	90.04	2.24 2.42		9°18
360 DESS	a remaj e		263	10,01		. !	451		10.31	243	28,47	11. • ;	78 1 12	920	52,98	12,77		169	62.23		0	104	76.29	22.23		264	79,27	29.92	<b>1</b>	449	90,10	27,13	•		29.08	27,32	::	90.00	29.08	27,32	346	00.00	27.52		3,16
		~ ·	255	8,56	N 5		£	10.0		513	34,94		***	495	44,01	P		497	57.94	77.62		413	9.00	17.55		383	22 45	18.21	•	376	28.30	18,81	į	78.87	23.41	18,62		70.67	25 41	18,82	375	76,07	18, 82		er ic
TABLE B-49	414	TAPE NO.	232	7,21	5, 84 4,74		787		9,24	767	29,46	*. *.		767	40,10	11011	<u>:</u>	471	19.61	12.50		421	97,00	13,95	•	660	90	14,01	•	200		12,21	į	56.50	18.97	15,21	***	29.90	18,97	15,21	303	59,50	15,21		2115
TABLE B-49		•	213	5.99	2,32 4,38		335	1 4 5 K	9.25	425	23,79	Z:	**	439	32,66	7 7	•	462	19,04	111271	); i	451	0 ° 0 ° 0	10.95	•	439	47,43	11111	•	435	000	11,27		10 to	13.94	11,27	•	48.40	13.94	11,27	435	48,40	13,94		111
d G	Supples	9	100	4.73	3.87		505	80.7	9,91	10 H7	19.07	6,21		401	26,14	/1.0	•	395	32,55	70	,	415	04.02	9.04	•	404	37.69	90.6	•	404	37.76	41°6	į	*D * 4.5	11.76	41.0		40 4 57 . 64	11,76	9,14	<b>*0</b> *	37,93	11,0 41,0		60°5
		46 90	175	3,01 1,01	3.50	. ;	242	4	60.0	333	14,69	2,65	07.0	345	20,26	97	3	361	24,62	4	-	380	27.18	-	•	378	27.79	8 46	•	375	24.0	64.8	ļ	27.97	9 33	8 49		27.92	9,33	6	375	27,92	ρ. Β. Β. Β.		24.7
			\n\d	2,84	3.27	. ;	221	900	11.0	267	10,73	n i	7.	277	10,000 10,000	0.06	•	562	16,29			314	17.40	7.93	•	317	17,68 100 17	7,98	•	316	7, 70		;	010 47.76	7.04	000	***	310	7,84	8.03	316	17,76	4,00	4	C917
	PASAMETER GEESOP		1.0C NE	13	- 63 - 63 - 64 - 64		2,00 he,	- ·	STD,	3.00			316	4.00 AB,	<u>.</u>			5,6C he,	ដូរ	- 5	2	194 JO 9	֖֭֓֞֞֝֞֝֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֡֓֓֓֡֓֡֓֓֓֡֓֡֓֡֓֡֓֡֓			7.00 NB.	֖֖֖֖֖֖֖֖֖֖֖֖֖֖֖֖֖֖֖֖֖֖֖֖֖֖֖֖֓֞֞֞֞֞֞֞֞֞֞֞	245		194 30.8		245		A DE NE		STE		10.01	, Li	245	LIKIT AB.		1 Light (5)		* 5 A

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X PARAME		10066,00	20.0	1.00		23	0,31	1.78	1,23	9	# G	2.23		123	2,56	.2,02	194	3,77	1.9	244	96.4	2,31	96.1	257	2.26	1.03	267	1.73	2.2		278	22.2	1,79	271	4.86	2,25	1.79	274	10° 4	
		6100,40	70.0	1,90	0.00	25	0,31	1.70	1,93	ř	0.17	2.18		2.19	2 20	1,30	145	3.70	2	67.5	3.64	2,38	•	211	2.5	1.43	221	7.7	2,2	:	224	2	1.79	225	4.13	2,36	1.7	228	4,18	
<b>9</b> 0.0 <b>9</b>		6400.00	, G	1.00	0.0	22	0.27	1.55	1.23	7	A.82	2.55		24	2.33	1.80	142	2.3	10.	7	2.92	2.16	1.0	188	2.12	1.63	199	3.32	\$0.5 \$0.5	•	203	0.0	1.59	284	3.41	9 · 2	1.58	205	3,45	
9,30 LAMDA:		4900,00	0.02	1,00	0.0	18	0,22	1.50	1,01	;	0.63	1.84		76	2.03	1,57	121	1.86	7 7 7	**	2,18	1.88	1,50	164	7.5	1,35	175	2.54	1,82		179	4.57	1,30	180	2.62	1,92	1.30	151	2,65	
5		3600,00	20,0	1,0	0 ° '	•	7,14	1,29	ů.	30	50 °	D 0		2 4	1.76	1,12	96	1,16	40.	# C	1,43	1,66	7,41	130	1 H	, o	139	1.0	10.1 10.1	•	143	96	•	177	1,30	1.57	.93	145		,
A LEAST TO COUNTY AND TO SELECT	2	2507,90	9.01	1.00	0.0	19	9.92	1.00	3.30	13	D.1.0	1.23	} ;	2 2 2	4.2	9.50	11	19.6	0.50 5.00	7.8	0,31	1.29	0 0	2		9,54	113	1.74	9.56	•	901	1.26	9.54	96.	1.39	1.26	3.55	139	00 to 1	•
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		ter E	. D. E. E.	2 (P. E.)		. <i>u</i>		.,	ű e	,	() ()	သော လ မ ဧ ဧ ဧ	•	- : c	C.	ن د	a	Ē.			: : :	ć i	<u>.</u>	(	7 C	<u>.</u>	c		i n	•	" ć	e.			' t.'		٠,٠	٠	e (	
		į.	.3:	e i	•	٠	÷.		۲.		Ė	υŁ	:	÷		÷.		ņė	٠,٠		c.	i, i	•		·i				· ·	•	٠,	• '	.'.		′.		· .		e;i	
ARAMFIFA LT-13T		ر م	PCT.	. Tu		2.5. 18.	PCT.	. בי	הוש	4.5. 18.				. E. C. 30.0		513.	12.5. 19.	PCT.	יינבי. בייני	, t				24.5 .4B.		<b>4</b> 19,	32.3 .6.		י בידי הידי		40.5	• • • • • • • •	413.	5.05	P C 4	<b>,</b>	t	LIMIT 19.	D :	

	350% ade	2.10 LAMBAE	
TABLE B-52	Political salarses	CAULTY TO TOTALITIBAS ANINE	F 22.

00.09

					7				AVG				AVE				AVE				AVG				AVG				7 1				7				446				7				4	<u>}</u>
PARAMETER RANGE	LIMIT	•	0.65	2.6	6529.72	45	0.61	7	6736.38	:	1.97	7.74	6495.46	145	N.67	5.17	6638.49	286	2.12	2.53	6637.76	259	i di	2.5	6542.01	285		2.45	6584,11	297	?	2.63	6447.83	909		2.41	6415.91	900			6416.03	907	3:		4450.02	68.6
Y PARAME	10000.00		0.64	1.00 00.00		90	0.53	1.7	7	<b>3</b> 5	1.74	9.0	7117	127	3.20	3,16	-	173	2.7	2.42	•	582	***	2,5	•	225		2.44		238	7710	2.41	• •	247	200	2,38						244	v	21.5		3.6
	8100,00		\$u*3	# E	•	<b>4</b>	0.48	1.76	•	76	1,53	2,53	1.61	109	2.71	3,12		147	6	2.45	•	177	# C	2.41	•	117		2,36	•	543		2.33		216	26.6	2,30				20.0		218	<b>9</b>	200		3.3
	6400.00		Ę.	F. 6		٨	60.	ه و	•	69	Ņ	2.35		•	7	2.36		122	7.01	2.17	•	150	3.26	2.18	•	168	N	2,32	•	181	0.4	00.7	•	2 T	6.4	2.07		191	3.67	?		190	9 n		9.00	9.34
	4002,00	-	Ti G	# C	• •	19	9,20	1.32		53	0.73	1.72	0	76	40.4	2.21		204 (0)	1,72	10.1	•	128	2,31	1.50	•	146	٠ د د	1.54		156		1.51	•	191	60.0	1.50		191	9 ° °		7.1	162	2.67	70.7	7.1	10.30
,	3657,10	•	D: "c	ວິເ ເີເ	•	10	80 C	D C	•	2 <b>6</b>		7 .	? •	•	Ŧ,	۲. د د د		73	1		•	60 i	200	4.45	•	114	46.	1 11	•	123		1.10	•	178	1.1	0.00		921	)			129	ed 9	• · ·	D	17.12
1	2500,10	•	6:3	0 0 0 0 0 0	•	<b>M</b>	72	9 6	•	10	<b>6</b>	25	•	52	N I	1, 20 1, 3, 4, 5, 5, 5, 5, 5, 5, 5, 5, 5, 5, 5, 5, 5,	•	7 :		0.72		<b>5</b>		F. 73	,	2		0.0		- c	# # # # # # # # # # # # # # # # # # #	65.0	•	<b>7</b> 0	20.	2.58		* ;			<b>n</b>	\$	4,07	0 4		14.54
			J.F3	900		יט י	00°0			<b>:</b> -1	e e	ව ර සු ර ef t	•	'n	م. 05 د د د	to tu	•	n ,	٦,	0 <b>4</b> . c	' '	W (	25.	90	•	42	H 7	7 W		C 4		7 .79 4 P7 4 E -	•	<b>*</b>	Paris de la compansión de	92.0		* .	* *	1		24	() ()	C: - C	97.	17.46
	טר יוינ	n	u e t	3 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	•	· • ·	. ja . E. i E. i	9 A	•	3	<u>د</u> .			<b>~</b> ;	2.1	ا د ا د ا د		ن و و	<b>y</b> (	, r		ے دا ہ	0 12 6 6	) (2) (2) (3) (4) (7)	•	7 . • · · ·	u i e e m	) () () ()		۵ + + ا		1 12	•	<b>≯</b>	46	, n		Pi d	n c ri c e e		•	5 T	Λ.,	) : 	•	27.60
	٠,٠			 	•	,	<b>.</b> (		•	v	C. (	ι . 	<b>:</b>		<u>.</u>	_' <u>.</u>	•		 		•			د د د د د د	•	,	. E	. e.	•	i	i t	1 .5 • U	•			)	•	-1 (	-1 C		•	-1	٠,	? 	•	37.40
	٠.	٠	nt i		•			•		•				. ,	t'. 1	.'	•	,	. i	. r.			ų ė		•			·		٠ د									- · ·	٠.				· , e,	•	U
F (		٠٠٠ د. ٥	,,	ייי יייי ער		, , , , , , , , , , , , , , , , , , ,	, , , ,	ייני ייני		4. V. 4.9.		֓֞֝֞֝֝֞֜֝֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֡֓֞֓֓֓֡֓֞֝֓֡֓֡֓֡֓֡		. C		, i.i.		12.5. 40.	, , , , , , , , , , , , , , , , , , ,	, E13,			13 1	, c.		24.3.	L			32.5	, )	, 1 ! V		40.5, 3P.	,	٠ ١ ١		,	n.	a E		LIMI1 49.			•	*

B-53	ICTIFY OFF YOSE	IN S D.OO LAMDA=	72 62
TABLE B-53	PERAMETER INTERACTION	SUBJECT TH CONDITIONS RAIN &	F 077

PARAMETER L	LT-D9T				J	- 184	ma*7/				Y PARLME	Y PARLMETER RANGE
						TAPE NO	1.1					
	<u>.</u>		.0.00	3 1 1 CO 6	30,3991	2501.90	3667,76	4900,00	6401.50	8101.0	10001	.1 <b>.</b> 1.7
		į	5 ; 6	3 ¢	ع د. د	<b>-</b>	۲ ; د	4 5	2	<b>.</b>	2	٠ <u>٠</u>
		 	: °					200	7			
7		· ·	ع د د د	_ (	5		•	D	1.70	9 6		
, ,		=	30°4	•	_	3	•	00.0	00,0			34 90 BAY
	•		•		•		•	•	36	38	96	
79.7		Ė	ء د	- C	1 5			900		. X.		9.42
					100.1	100.1		9	100 m	7	1.41	1.51
			00.0			200		M. C.	97.6	1, 32	6.91	0.87
•			•		_	•		•	•	•	•	9016.88 AVG
A. U.		٠,	Ļ	0	•	14	中的	45	99	7	9	2
104			•	0.0	£0.0	0,14	39	99.0	۰.	1,21	1,36	1.65
			30°	30.0	1,00	1,21	1,4	1,64	2.14	7,14	2,13	2.23
T2			۳.	•	<b>0</b> 0.0	6.36	84.0	1,38	٠.	1,72	1,76	
•			•	•	•	i	;		•	•	•	1214. Bd AVE
2 t		٠ ,	•	•	•	7 6	•	?;		177	110	707
		F	0 0 0		2 4 6			1,00	1.0		2.40	
7 .				·		1.70	7.01	3.4		96 4		
<u>ጉ</u>		3	٠.		•	7.00		2017	) (	•		7322.86 AVB
12.5L ×			a	0	14	NA NA	69	102	128	156	187	
	PCT.			96.0	6,12	ñ.46	1,13	1,67	Ė	3,22	3,76	÷.7
<b>a</b>		5	00.0	90.0	1,07	1,53	95.5	2,29	9.59	2,55	2,52	2.62
S		۰.	ď.	Ē.	r.26	۲.	1,70	1,51	1.01	1.30	1.06	
				,	,	ì	•	•	į	,	;	PAV 18'262/
10.01				o :	25.	7	: :	126		261	£ 7	767
	_			1 G	1263	70.0		2,00	- W			2,42
7 5				٠.	1 6	. 7			-	F . C	7.0	2.20
'n					,		:	3	•	:	•	7895.17 AVB
24.5. 4		٠.	0	1	32	72	112	144	170	242	234	<b>505</b>
	PCT.	6	Ö	90.0	0.30	0.51	1,60	2:47	3.34	40.4	4,65	5.84
		5	0 0	1.30	1,16	9	1.79	2,15	2.46	2.40	2.49	2.54
15		5	•	30.0	0.44	B. 19		1,53	•	<b>*</b> • • • • • • • • • • • • • • • • • • •	2.07	2.17 4054.11 AVE
	٠		c	o	4	9.6			46.	446	240	
36.36	_		, E	, C - C	6.32	2.50	1.70	2,58	1.47	4.17	4.90	
		5	20.0	1,90	1.14	1.38	1.76	2,11	2.44	2,51	2,51	2,57
S		-	•	٠.	٠.	6.75	1,15	1,51	1,91	2.03	2,07	
	•		,	:	;	•	:	•	9	223	28.2	6911,97 AVE
	_	 e	' ē	7 -		-		20.0			4.65	4.21
•				0.		1.37	. 22		9.36	2.43	2.46	2,52
8.	STD.	=	000	0, 0	0.42	6.76	10 F	1	4.1	2.01	2,05	2.17
		)	•	•	•	ı	•	•			. ;	6855.58 AVB
				7.	;	16	133	106	192	273	52	213
	PCT.	6	9,01	0,11	. 30 . 30 . 30 . 30 . 30 . 30 . 30 . 30	C6.0	1	2,1	3.62	98.4	Du . C	9.5
**				36.4		1,37	7.	20.0	2.30	<b>.</b>	7.67	2.51
Ā	_		•	•	<b>7</b>	•	7.1	1,30	1.0	1:1	6012	6852.86 AVG
LIMIT			N	16	£.	66	136	170	197	230	262	323
			~	9,15	0.39	16°0	1.4	2,76	3.70	٠.	5,15	6.45
	DT.	0	1.60	1.90	1,14	1.37	1.70	2.04	2.36	2.44	2,46	2,50
S			ь .	J. 10	1,41	6.70	1,12	1.49	1.68	~	2,03	2,14
•		÷	17 93		** 6.	**	13 51		:		•	9852,14 AVB
ī			7:1.4	1100	9	4 0 1 2 4	•	42.24		3	4	, D

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TABLE B-54	PARAMETER INTERACTION OFF 40SE SUBJECT TO CONTITIONS ANTW # 0.00 LANDA:	

PARAMETEN LT-TOT	•			•		9.				2	
•					TAPE WE	 				A A A A	TER FAUL
4	6	40°.00°	00° 000	1600,00	2500.90	3600,70	4900,00	6400.00	8100,00	10000,00	LIMIT
	r t	· •		•	9 6	- ;	- :	7	~	~ ;	٠,
		) (C		2 6		0 6 0 6	0 0	0.02	25.0	0.02	7
STD.		ם, פני						96		- C	D (
	•		•		•	•					18122. AVR
2.6( 149.		9	ت	н	NI NI	•	16	54	26	35	
D	6		9.00	0.01	0,02	50.0	0,15	0.27	0.31	0,37	0.4
TO .	<b>1</b>	3	0	1,00	1.00	1.00	1,19	1.42	1.39	1,31	1.38
51D•	Ė	00.	30.0	0.00	00.0	9.0	0,39	1.04	1,14	1.04	1,25
4	•	•	•	•	•	ţ	i	;	;	1	7786.33 AVB
	۱ <u>ن</u>	3 é	4 5	N (	•	2	39	9	2	2	#
			100	70.0	90	91	25.0		1,75	7.	2.07
	5 E		) (F	100	3 E	7.52	1,67	2.63	2,08	2.03	2°.
20.5		3 •	3		7	20.0	26'0	1.45	1,70	1,63	2,06
6.01 86.	•	C	+	^	22	Ţ	11	*	***	64.	8278,50 AVE
	0	-	9.01	, D.	5,25	1 12			֚֚֓֞֜֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	77.	•
, La	Ė	- C	0		17.1		1167	,			
510.			30.0		6.55	1 . A.	7.42			20.0	
		•	•	•		•	•			7	7008 72 AVE
12.5. NP.			CI	12	37	95	*	119	144	161	204
PCT.	9	0,0	50.0	0,10	6.43		1,61	2.51	3,23	3,59	<b>*</b>
. 10	63	ກ <b>ປ</b> ິດ	1,00	1,08	1.40	1,77	2,15	2.65	2,41	2,80	2.97
STD.		ے	0.00	82°0	45.5	1,11	1,56	2.04	2,39	2,48	2.00
											7688.44 AVG
10.01	٠٠,	C	<b>+</b>	72	25	78	114	191	167	134	526
		- -	9 to 1	0,18	96.0	1,10	1,92	2.90	3,66	4	5.43
	3 17		-10	100		1.7	7:11	2.57	2.73	2,2	70.7
	•	•		73.0	9	1.10	1.00	7.7		/6.7	21.0
24.5. NB.	,		4	30	F. 6	•	124	1.6.4	1 70	•	244
PCT.		u	6.35	0.25	0.73	1.26	2.10	3,10	27.52		9,70
.10	5	ာ ရ (	1,30	1,03	1.44	1.76	2.10	2.54	2,75	2.76	2.0
410.	0	30.0	00.0	0.18	0.51	1.14	1.63	2.17	2,61	2,68	3.13
		•				•	•		•		7415.61 AVE
32.0. 49.		:	10	ij	11	193	138	167	1.1	211	526
PCT.	63	, e	85.6	, 34	9".0	1,49	2,27	3.29	7	7,60	4.07
ia (	<b>D</b>	2	3 4 6	1,05	1.40	1,71	2.00	2.47	2.72	2,73	2.97
.01S	<b>:</b>	, L	1.50	7.22	66.3	1.11	1.60	2.12	2.56	2.64	3.11
40.5. NR.		٠	2,	57	-	107	173	17.4	3	240	247
PCT.	ů,	3,02	9.10	0.38	36.0	*	2.31	3,37	***	4.70	6.23
٠٢٠		30°L	1.0	1.07	1.40	1.69	2.04	5.44	2.15	2.69	2.05
510.		, D. C	11.2b	3,75	9.78	1,10	1,58	2.P9	2,54	2,61	
	•	•		;	:	•	;	,		900	7343.94 AVG
		•	1 5	•	7 K	717	•		7 7	66,	
i i			10: E	1.06	1.10	1.47	2.0.2			2.6	2.00
STD.	6	ລີ ເ	0.26	9.54	0.58	1.33	1.56	2.07	2,3	2,58	3.06
		•	,	,		•		,	• I		7334.61 AVG
LIMIT MG.		;	eri (	51		117	153	282	210	232	281
; ;			7.16		25.4	0.	2,31	36.5	7.4.	•	9.57
יובי ביי		- C	1.20	2.0	75.0	7,67	C0.2	2.0	, ee		2 4 5
		•			•	:	***	•		:	7279.39 AVB
AVG.	6	54.72	29.45	24.66	21.53	17.55	14.88	12.94	12.49	12.33	Z,

	X PARAMETER RANGE	LINİT	20.0	1.00	0.0	16577,35	\$1 *	1.42	0.82	10711.85	1.17	2.09	1.65	116	2.47	2.63	7689.69	161	3.42	Z. 60	7651.39	182	3.82	. e.	7453.51	193	4,13	. 62	7241.71	205	4.18	8.70 	7138.30	212		2.18	7076.97	218		2.17	7026.45	4.36	2.46	2.16	13.24
	X PARAM	10000,00	9.6	1,00	0.0	;	2 5	1.31	0,61		0.85	1,36	1.34	•	1,96	66.5	96.5	132	2.74	20.0	01.7	149	90.0	2.58	) ii .	140	3,26	2,56		172	3,41		•	179	5. C	2.04	ì	L L	2.41	2,0	101	3.73	2,37	2,61	13.76
		616".10		1,10	0.0	;	1 .	1.36	6.54	ž	0.76	1,36	1,37	2	1,77	2,72	51.2	121	2.49	2		137	2.79			148	2. 18	2,5		140	M C	5,5		147	, r	2.3	,	173	7	£	44.	M 4 M	2,32	2,71	14.08
90.09		6401.00	# E	00.1	00.0	•			P. 66	;	29.0	1.05	1.50	67	1.36		9	90	1.04	20.0		112	2.25	V. (	•	172	2.40	7.47		133	2.53	50°C		140	7.61	1.97		146	200	4.05		24.7	5.23	<b>7</b>	15.05
XBSE .00 LAMBA:		4986,00	7 6	100.1	00.0	•	6	0 M	n. 47		9 7 6	1,45	56.0	•	6.85	2.18	1.3/	77	1,79	2.10	7 * * *	6	1.55	6 ( C (	40°E	104	1,71	2.76	900	116	2 , A 3	1.97	7 1	123	• • •	100	•	129		1.31		8°,	95.	1.13	16.71
956	5	3.407,70	9 6	, C	0	,	- 6		3,30	•	11.0	1 2 5	<b>*</b> 5 ° C	31	. 45	<b>7</b>	1 • 1 •	\$	.,71		1,	4∑	200			9,	۲, ۲	*.		47	1.17	9		*6	. 2.	• • •		110 13÷			•	υ <b>τ</b>	14.	<b>1</b>	*c*
TABLE B-55 ER INTERACTIEN 1645 RHIN #	F 844	74PE 48	<b>0</b> 0.0	90.0	0.00	٠	4 0	70.0	0.99	,	10 C	5 , 4 5	7.73	16	3.95		1.0	30	31	7.4	4	7,	9.50	3.0		53	3.54	ાના હ (૧ <b>૦</b> જૂન ઇ		4,	6.74		? -	70	. 79	4 0	i	9.6	P 12	10	ì	, i	7	, J.	<b>5</b> 0.00
TABLE B-55 PARAMETER INTERACTION SUBJECT TO CONDITIONS AMIN #	.i	1430,63	ء _ ق	00.0	7.00	,	7 C	9 (C		•	1 6.0	1.00	<b>8</b> 6.60	**	90.6		•	1.	9.10	1-2.	•	۲. د	.73	15		∌£	7 * 3T	1.13	60.	45	, <b>, 4</b> , °	¥7) ( v · l v · l		7.7	24,	3 4 4	,	2 4		, ,	u	í	ł J	5 3 .	25.73
THORDS		01,4006	න යා දෙ	2			3 .: 6	9 (*) * (*)		r	o in		3	н	1,7	(*) 	,	٧	(V)   	ri f	•	٥	ŗ,	, ' I	,	•	,		•	U	`	,,,,	9	•,		• •			• .	•	:	/ N	• •	•	,
		0.15	, i.	Ē			•				· (	tu F	ر. • د.	,			; •		£ (	L, r	•			·.·	•		٠.	٠,	•			` <b>.</b> '	•			• }•			•'.	.'.		ı	• _ •	r . •	2.
	<b>b</b> .		•	i.		٠	į	ï	• •		ïė,		٠.			c.			u, s	e t	•		٠.,۱	' <b>.</b> '			٠.	•••			٠.	• • "	•						٠'						
	ARANETER LT-18:		0.5. 49. PCT.		c13.			,	000		100				P.T.	) ()		12.5 VB.			;		, 0 1			24.5			•	11.0			•	4(.) F.		• • • • • •			· ·	. ;			•		2

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では、10mmの大型の大型を行うという。 できるというにはある。 10mmの できる

	STE KRAE
TABLE B-56	Particular particular of library

					AVG				Q.Y	•			AVG				# A A				BAY				AVA	•			9				97				g A				9.4	•			914	
AMETER RANGE	LINIT		0.112	9. d	18226.53	20	0.26	1.63	17401.38	9	16.0	2.03	13727.76	•	2.07	7.64	11573.65	130	2.71	N. 6	10343.02	151	3.14	2.61	4.65. 4.65.	142	d. 00	2.5	2.36		3,50	2.59	2.62	177	3.62	2.96	2.58	179	3.70	2.59	2.59	198	3.98	2.55	2,53	15.93
A PAPANE	10,00,00	~	0.02	2.0		13	0.17	N 1	74.0	43	_	4.86		71	4	2,52				2,33			2,35				2,52	2,51	0212	***	2,62	2,43	2.16	143	2.72	2,38	2.13	145	2,79	2,41	2.15	164	3,45	2,33	2.19	16.75
	810",40	-	10'0			10	6,12	1.50	<b>7.</b> 5.	37	67.0	1.68	1.4	62	1,21	, c	212	į	1,67	7.49	6113	1,43	2.42	2,46	V.10	114	2,21	2,43	2.13	161	2,31	2,35	1.39	131	2.40	2,30	1. 36	133	2,47	2,32	Br • 1	152	2.12	2.24	1.14	47.42
	6404.00	#	5.0	6.6		^	90.6	P		30	62.6	1.47	10.	97	D . C		• • •	99	1.32	, c		76	1.64	7.	7.77	45	1.81	9.00	2.10		1,96	5.79	2,65	112	00.4	2.23	24.5	114	7.64	2.25	2.05	132	2.27	2,15	1.98	18.39
	4990,00	<b>+</b> 1	10.0	4.0	•	2	90.0	2 C	0.0	20	£2°5	4.5	0	31	09.0	7°.42	10.	90	١	95.0	3	99	1,22	2.25	7	76	1,36	2,10	2.11	:	1.44	2,08	1.93	Š	1,53	2,02	1.90	96	1,56	2.00	1.01	113	1,73	1,92	1,81	18.54
	. 1 340°, PG	<b>5</b>	P. 1	בייני נייני	•	•	٠, د .	P 6	•	11	1,15	. 7.3	<u>.</u>	12	W 1	,,,	•	39	6 : . (	2 4	•	\$5	204	D d		45	4.55	27.5	\c.	77	#1	1,01	1.60	2	1,71	# . E .	1.56	115	1,24	2	1,16	, <b>A</b>	1,40	1,77	35,	37.75
	74PE 13. 2580.00	•	3 C	30°C	•	~7	ان در د	) C	) )	•	7.57	5.75	00.1	10	7.16	5 5		12	P70	10.1		36	0.47	e H	F	;	0.57	1.51	36.1	ř	6,55	1.53	36.7	59	0,71	1,51	S :	51	6.73	<b>6</b> 1	1.92	72	59.0	1.64	9:0	23.41
	26.7.49	:o	() f	 			r! (	7 6	•	۳ł	E .	e c		**,	) ! E. !	1	•		2	7 7	,	16	5.17	H 6	36.	\$2	2.24		76.3	۲,	9 H	1.16	9 7	8) (1)	3.3	1.16	5.4.5	3.6	1.36	11.15	5 Y .	4	24.0	1,13	62.	37.75
	5.00	3 (	:1. i : i: r - i:	3 ; • •	•		ن د. ۲۰۰۱	٠.		Ü	3		•	ر.	i i	is my	•	-	دا ر د و	3 2 ( )	•	н		: د د د		¥	3.73	3 	•	•	,		2	7	, 3 , 4 , 6	(a) (		15	73	.3 .	ب • د د	•	9.0	ن ا د ان		\$4.42
	· · · · · · · · · · · · · · · · · · ·	•	. <u>.</u>	•,'	•		L (		•		ن ر		;		č. (		, •		e (	i.	•		: (		•		ç.	د د	<u>:</u>	•	( e .			`	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \			•	ر د		•	,	٠,	ć. ,	•	76. 32
	٠,	٠.	٠,٠			,	L r		•	•			•	,	i <u>.</u> .	l.	•	1	۱ <u>۰</u> ۱		•		i.,		:		e.		:		ï,	::	ί,		<b>;</b> .	·.·	•			• •			ί,	Ė,	٠.	٠.
		, t		1		c		ייני נייט			   			10				12.5. ag.		 . L 3 !-		16.6. 32.			.1	24.5		► (. (.) • 4	in Ž		901	, ,	ر ا ب د ا ب	44.5. YE.		(2)	e1	50.0		• • • • • • • • • • • • • • • • • • •	in the	This co.		۲,	i.	*5A2*

	Y PARAMETER RANGE	LIMIT	ب ا			24278.65 AVE	0.34	2,47	2.69 20502.83 AVG		1.13		17190.70 AVG	1.72	3,16		14150.91 AVG	2.17	3,06		151//.1/ AVE	2.60	2.79	5.00	11/26.4/ AVG	2.77	2,78		11CV1.51 AVB	2.96	2.75	10756.63 AVG		3.07	2.92	10676.74 AVG	151	2,4	2.77	10428.58 AVG	143	2.5	2,71	10223,31 AVG	
	Y PARAME	10000,00	0 0	00.0	0.0		0.08	1.67			200			. E.	2,24		3	1.13	2,20		5	•	2°0			1.66	2,78	١.	111	1.74	9.0	0	118	1.03	*		175	20.0	1.62		1.17	1.06	1.57		
		8100,00	<b>6</b> 6		0.0	•		2.40	0.71	13		2,42	;	) (C	W + 6	1.76		10 °C	2.05		ă	1.31	20 e e e	9.	*	1.46	£.	•	1.5	4	1.36	) · ·	112	24.	7		ο . • • • • • • • • • • • • • • • • • • •				121		. 42	96.91	-
60.ng		6401.00	e e		9.00	r	20°±	2.00	1.00	***	 	2.32		15,0	2,13	1.96	ĭ	2 4	2.0	1.65	2	1.09	1.89	4.35	ă	1.73	1.90		Y O	1.40	. R.O.	1.40	1,1	80 P.	1.42		1,0	0 d	et.		110	7.7	W, .	. 61	
F 485E 6.06 LANDA=		4900,00	4 6		00.0	•	1,6	2.00	00.0	•	20.0	2,22	ç	9.50	2.06	1,95		9.56	1.84	1.60	ç	13 E	1,77	1.51		1.02	# ·	1,43	, A	1.19	1,42	1.42	Ū¢.	1.76	1 30		,	1 6	, p		176	7 0	\$2.2	20.43	
g 6		3600,0	<b>0</b> 6		00.0	•	90.	00°	o r	• ;		1	•	7.21	2.17	7,17	;	3.5	24.	**.	77		24.0	6,	5.5	.72	4.1		7.5	9,4	<b>3</b> (	67.	25	1 o	25		C) (1	,	, n	i	ď.	) v	•	17.71	
TABLE B-57  CENTITIENS THIS TABLE  LAMB T 144	10 10	2500.00	000	9	0.00	c	90.0	00.0	30.0	++ <u>{</u>	90.0	0,00	q	60.0	1,72	C.45		6.16	1.33	6.50	7	0.37	1,35	27.5	7	£.47	1.40	5.0	40	14.0	1.45	•	5.5	(h (r) (r) (r) (r)	2.73	,	0 / 0 / 0 /		7.7		9 29	9 40 - H	4.	4 6.	•
TABLE PARAMETER INTERES 14 AMB T	•	1650,00	6) 6		0.00	c	٠	00.0	<u>.</u>	•	) () () (	c	•	<b>\$</b> 0.0	1,25	0.43	•	ü	1,43	۲.	2.0	0,22	1.23		Ħ	, 13 , 19 , 19	1.27		4.0	245	51.1		47	ණ යා අ දැ ය ද	0 • • • • • • • • • • • • • • • • • • •	,	() () () ()		4		or , ur) ,	4 (P)	4	,	
Subject te		967,696	ים פיים ר	9 60	9 u * G	ц	ب د د	<u>ت</u> . د	<b>3</b>	'3) (C)	) (1) (1) (1)		r	2.5	1,70	9	,	\ e .	(3) (-) (-)	ع د •	•	5.00	3 ( [" [	o r r	•	3,14	Ţ.;	?	11	0 11 0	€	 	~	(A. 14) 11: 11: 11: 11:	(3.		<b>4</b> 1	1	7 4 7		T) ()		75.	5	•
		5 <b>6.03</b>	9 E	, D	Ē.		: 3 E1	ָרָ בּי	, ,	'.	 6.	c c	,	ن ت د	0.00	3 <b>6</b> ° °	r:	`		د. د. د		10.	ن • • •	•		,, L.,	12 c		•	ני כי	i i		<b>\</b>	ų 1 ⊾ 6,	 		9	۷ • •	• ְ •		* (				· •
			ķ	E.	i.		ij.	E (	j	• • •	a et	•		•		ů.	•			t.		5	LY A				٠. ذ	•			i <u>,</u> i	•	• •				·	• '	•'•				٠.	٠,	
	PARAMETER LT-13T		0.0 PCT.		STD.	67. C		.Ta	\$10.	4.5. 48.		STD.	9	7. T.	er.	sto.				či.		PCT.	ra f	.016	74.3 .A.		, c	• (11)	32.6. 1.9.		i	5	48.5. 16.	1 1 1 1	ELV.		50.0° .88.	• •			L1817 26.	• • • • • • • • •	, c. r.	3	•

					974	•			AVG	!			Ave				AVG			9				AVG				AVG			AVE	:			AVG			1	7 A			
90000	E FAXALLIEF XANGE	LINIT	0.52	1.00	00.0	20	0.34	2.10	73618,57	77	9.00	69.	16193.42	D 00	4		16813,35	6 F	4.13		11.50561	1.53	3.25		3	1,62	3.70	12931,68	1.74	2.91		~	1.77	3.45		2 :	2.83	3.40		1.96	P0 . N	1
2	H VAXA1	10000.00		0.00		7		1, 00 00, 00			0 × 0	2.64		12	No. 10	2,87		7 70	2,70		-	0.67	202			0 76 7 E7		6	0.88	1,03			16.0	1,93		62		1,65	46		1.60	
		8100,00	9 6	0.00	04.0	7	92.0	1 ° 1		•	. K	2.64	,	2	13. N. S.	2,47		10	2, 79	7,48	5	9,46	2°	7	45	, c	1.95	š	7,47	1, 15	<b>.</b>	38	2 .	6	;	44	1.32	1.46	47	80.	•	
•		6400,00	2	00.0		m	9.05	1.00		<b>.</b>	. F.	30.00	;	10	20.0	2.08	!	47	7.47	2,38	Š	. S.	1.94	***	ç	7,63	1,75	E.	0.73	1.82	1.61	25	9.70	26.	;	7 24	10.1	1.58	20	5.42	62.	
		4900,00	9.00	0,0	00.	2	20.0			ر م	N 6	2,10	,	** ***	2,75	2,49		14	2,36	5,09	1	0.45	1,7		36	7, 54 5,66	1,53	45	9.62	1,73	1.40	11	٠ ر	4 4	: !	0 4 7 7	1.73	1,38	53	0.71		
162,09	٦,	3600,00	. 30 	06.0	06.	0	D	3 E	•	2	70.	06.0	•	• 50.	1.50	n #7	1	Ф М Т	1 78	1,13	MC.	125	4. F	-	28	1,57	, c	<b>19</b>	n 4.0	1,50		38	9 2	96.	. :	0 4	1,52		;	1,52		
Lawp T	TAPE N3	2530,00 360",30	00.0	9	3	0	00.00	90.0		<b>-</b> ;	10.0	0.00	,	20-0	1.00	0.00	,	60-0	1,57	1,05	48	32 0	1,39		23	1,52	£6.0	40	0,35	1,47	£6.5	32	0.36	F . 0	:	0 PE	1,48	66.0	92	0.42	94.6	
LAMP T 162,09		1600,00	00.0	96.0	30.7	0	000		•	++ ;	100	0.00	•	10.0	1.90	0.00	•	0 0 0	1.60	1.20	12	0.14	1,42	•	16	1,44	96.0	23	3,25	1,43	00.0	**	1.23	16.0		0 0 0 U	1.44	0 <b>.0</b> 0	27	5,30	C.	
		00°636	3.00	20.00		n		90.0	•	7	1001	96.5	•	16.6	50.1	30.0	•	2 00	1.00	0 °	٨	11,14	1,90		•	0 0 0 0 0 0	06.4	•	£1.	1,22	7.4.	<b>3</b>	us de la se	0.42		2.10	1.70	3 * C	12	9.11	7.37	
		434, ftc	, J.	្រំ	•	ε	<u>.</u>		•			ם.	:	o o		3,60		. 6		0.0°	#	n. C.		2	¬ ,	200	Ē,	н	7,02	2,00	3	7	N C	3 D		70.0	2.5	e e e	¥	70°L		,
Ļ		5							•	t		5	•	: i	5		•	ີ ຜູ້	10	: B	,				•	E .	<u>.</u>	•	ij	5		٠٠.	<b>3</b> 6				Đ		.,	en e	e i	
TER-TI REI				:		, A.B.	֭֓֞֞֜֞֜֜֝֓֓֓֓֓֓֓֓֓֓֓֞֜֜֓֓֓֓֓֡֓֞֜֜֓֓֓֓֡֓֡֝֡֡֡֓֡֡֡֡֝֡֡֓֡֡֡֡֡֡֡֡֓֡֡֡֡֡֡֡֝֡֡֡֡֡֡	110.				STD.	9		-	STD.		י אפר הידי	ıT.	rtō.	01. 39.		570.		28.		510.	, 0, 20		701		ار مرق. مرود		STO.	9		- - -	ato.	ee.≉	PCT.	210.	

	0.09	
	N OFF YOSE 0.00 LANDAE	
TABLE B-59	PARAMETER INTERACTION SUBJECT TO CONDITIONS SMIN B LAND T LIMIT	TAPE N9. 1

**						AVG									AVE									7 46					7				AVE				3					<b>7</b>				AVE	•				<b>9</b>
PADANCTED PANDE		LIMIT	-			14387.48	•	90.0	2.50	1.12	23621.72	•	7		18669.01	•	0.22	3,00	2.45	15992.71	1 K	2.44	2.45	15479.95	13	0.26	5. •	2.21	14976.10	9 0	7.0	, ,	13741.75	=	0.30	2.11	10.1	130.1001	0.35	2.00	1.81	15290.91	6 W F		M.A.	11623.42	29	0,41	1.76	1.63	11071,77
MYDYG A		10000,00	6	•		•	•	00.0	٩.	9	•	4 6				•	90.0	1,75	1,30	U		1.60	1.20		•	0.08	1,67	1,11	•	•	7.54	96		11	0,13	1,45	68.0	15	0,17	1.40	0.80	;	00		27.0		22	0,22	1,27	69.0	26.67
		8160.00	9 6				0	0.0	0,0	0.0	•	- 5	7			•	9u u	1,75	1,30	•	7	1.60	1.20	•	•	90 0	1.47	1,11	•	•	71.	44.		11	5,13	1,45	66.30	ŝ	6.17	1,46	0.40	•	5 G	# P	56.0		1,	2643	1,29	0 / ° d	25.14
		6400.00	9			•	0	00.5	9.00	0.00	•		4			~	<b>*</b>	2.50	1.50	•	ء ج	2.00	1,41	•	•	92.0	2.30	1.22	•	• •	# F		•	•	01.0	1,63	0°0	12	41.0	1.42	9.86		6		2.2		18	0.18	1.28	5/ ° E	24.97
		4900,00	9 6			•	0	00°	00 °	00.0	•	7 5	10,1			24	0,02	1.06	<b>0</b> - 0	,	20.0	1.00	0.00	•	m	20.0	10 m	0.47	•	۸ <u>د</u>		9		^	90.0	1,14	6,35	10	0.00	1.10	0.30	•			6.23		15	6.13	1,67	62.3	30.32
:		3650,9	-		06.50			06.0	•	•	•	- C				-	0°0	Ç	Ε,	•	1	10011	. ຕ		-	, 02	2,50	06".	•	? <u>.</u>			•	Δ	٠, د	C2.1	0 •		76.0	1,13		;	1 0	7	20		<del>+1</del>	1,1	1,36		53.76
	TAPE NO.	2500,00	2 6	20.0	0,00	•	ت	0.00	00.0	90.0	•	9 6	30.0	00.0	•	-	0,01	1,00	56°1	•	6.31	1.00	0,30		1	20,0	2.00	00.5	•	3 H	1.33	6.47	; ;	v	6.35	1.25		۵	6.57	1.13	0.33	;	101	0	· tv		15	0.10	90.4	37 °	32.41
,		1660,00	2 6		0.00	•	(3	0.00			•	3 C	00.0	00.0		-	0,01	300	00.0	•	10.0	1,00	۰.			20°E	٠,	•	•	200			١	•	- C	1,25	G. 4.3	v	90.0	1,17	0,37	•		4	٠,	•		9.67	떳!	1	39,21
		00.006	) C	90	90.0	•	J	3,00	00.6	30.0	6	9 0	- C	20.0	•	•	0.00	00.6	3,00	٠	0000	0.0	•		.3	30.6	30.40	3° 5	•	4 6 6	00.1	0.00	•	N	3.52	7	3 5 5	7	76.0	14 2 1	 0		3,02	, c	3	•	ירי	7.72	) H	<b>3</b> 0 • 0	29.93
		462,00	, c	•	200	•	o	ກ <b>ວ</b> ີ	ສຄະບ	, 00°		- c	2	6	•	r.	30°2		•	:	3 6	0.00	000	•	ס	က (၂)	2 E (	, ,	7	t c	00,0	, <b>6</b>			៊ុំ	2 	,	ō	<b>છ</b> .	7 C	(a.t.	:	70,0			•		0	5		ř.
		10. 10.	٠.		S	•	, ,	 0 1	0	 D•	ı	· (c		-	•		÷	C I	10°.	•	وي	0	0	•	• •	E I	5	9	•	i ti	5		•		D.	LD 6	5	٠.	<u>د</u>		•	•	(3	ė	<b>.</b>			L y	 	•	
PARAMETER I T-DAT		4			STD.		2.6. 38.	PCT.	.10	STD.	9	D 4.4	10	STD.		B. U. NB.	PCT.		STD.		DCT.	Ta .	STD		16.0. NB.	PCT.	, id.	Si D.		PC-1		519.	,	32.648.	PCT.			40.5. 48.	PCT.	. 10	1015	0 05	1116	, Ta	, or p		-IMIT	, L		2	, 9 v G.

TABLE B-60
PARAMETER INTERACTIFY OFF TAIL
SUBJECT IS CERLITTENS THIN = 18.00

ANGE	LINIT	ń	•00	9.	90	118 AVB	¥	. 56	.45		.46 AVB	47	.59	23	.62	.47 AVE	200	25.	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	OF AVE		.51	5	38	26	ii.	50	0.05 AVB	35	<u></u>		BAY L9	90	7.		1.27 AVB		.27	7,4		50.	12.1	1.80 AVG		00.	.65	
ETER R	=	r	•	-	0	15556		-	~	m	17333		<b>»</b> ( (	• 1	5	14041	•		•	13074	*6	~	n (	434.4		~	-	11866		W 4	- •	11552	•	~ 4	•	11448	•	•	99'6		e4 (		11366	•	. 4	.6	
Y PARAMETER RANGE	1000,00	~	C. 02	1.90	0,00	•	\$2	0,25	1,25	19.0		35	69.0	2,72	2,36	*	10				9	1,44	4,53	6		.61		5		77	51.6	2			56.5									<b>:</b>		2	
	3100,00	~	2.0	1.40	0, 0	•	23	5,72	1,72	0.51		32	96.	5 2	2.10	-	è •	7 A A	7, 7		37	1,32	4.49	5,61	33	1.48	5.93	9 c	39	1,50			1	200	5.7	:	1.56	2	ş	;	1.66	5.45	•	<b>.</b>	1.56	69.5	
	5407.90	~	3,02	1.00	00.0		17	71."	4.24	1,55		26	5 I	2,35	1.75	;	70		20.5	?:	20	1.04	4.48	4.97	000	1.17	5.07	2.66	32	1,26	70.4	7.38	ŦĎ.	1.28	5.51	! !	ĥ.	4.40	5.38	37	1.31	4. A		80 P	1.32	5.42	•
	4900,00	~	0.02	1.00	0.00	•	13	0.14	1,31	9,51		2	6,37	2,19	1,71	76	9 5	B 6	70.7	•	25	6,82	4,12	4.49	<b>5</b> 0	0.9	4,72	5,44	28	1,03	19.	1816	30	1.05	20.5		? ?	4.16	5,16	32	1.06	4,16		33	90.4		
16,03	365r . ng	~		1.30	20.0	•	٥	, 16	13.	76		=	22	#) • • • • • • • • • • • • • • • • • • •	155	ć	2 4				61	95.	99.	22.4	90		ę,	*.*	22	1,00	, e e	è.	52	W	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		9 5 2 4	. S. S. B.	4,43	56	5.74 1.0	0 M	;	75.	0,4	4.52	
rg.	2566.00	U	5.0	. DG	0.00		.\.	53.6	c,	۳,		173	9.0	2.67	2.36	4	÷		) d	06.1	4	0.14	2,25	1.56	7.	0.22	2.25	1.74	13	5.26	2,54	7.1	<b>4</b>	0.27	1.75	:	, 100 000	2.25	1,71	16	0.29	2.25	:	17	200		
	1600,30	Ç.	<b>3</b> 0.0	36.0	30.0		63	30°0	0.00	90°u		-1•		9 d	30° E	٠	· ·	200	- C	- ·	•	50.0	1,50	C.87	•	90.0	1,83	1,21	`	0,11	2 .	1, 67	70	0.12	0 6	}	о <u>г</u>	1.78	1,03	~	0,13	1.78	3	10	40,14	200	
:	36,636			00.0	00.0	•	0	90.6	36.5	9,00		<b>.</b>	ے د	ය ව ද	90°0	c	3 6	3			н	10.0	1,64	90.0	*1	3,02	1.06	90.0	7	20.0	900	0 0	•	200	3000	•	<b>n</b> 5	1.36	0.10	٨	* O * C	00.1		•		10° 1	
	a <b>6"</b> "3*	1.	ני ני	30,	90,0	•	״	90°L	90,	) 10 10		đ	ນ ເ.	7) E) L	٠ ئ	ε				•	7	n <b>p*</b> :	00.		-	າວ.	່ເ		כ	٠ ن ن	(2) (6) (2) (6)	3 • •	3		3 £	<u>.</u>	ع د د د		0 <b>0°</b> 0	د.	J. G.	٠ •	•	J	e 6	2 6	
	5	٠	•			•		£)		_		٠٠,			2	ι	'n		ė.			.0	0	ָבָּי. פּ	•		£.	ຼີ 0 -		5	e e	•	.,	b	) e	•	٠ ,		6		.0.	<b>b</b> 6			0	. 6	
Y PARAMETER LT-DOT		0.5. 49.		. T.C.	STD.		.0	PCT.	DT.	sto.		œ.	PC1.	-	21D	q	P (	֓֞֞֜֜֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֓֓֓֡֓֡֓֡֓֡		• - -	12,5t ve.	PCT.		STD.	18. D. A.P.		PT.	<b>S</b> 10.	24.5. ×9.		<u>.</u>	SID.	32,00 AB,		. ב ב		40.5c x8.		STD.	50.0. NO.		70.		₩.	į.	יובי	

	SFF TAIL	T N. DO LAMDA B
TABLE B-61	PAREMETER INTERACTION SEF TAIL	SUBJUST TO CONDITIONS RAIN A

						7				920	•				AVG				AVB					9 4				AVG				P V				4				424				98				9.4	
	LIMIT	0	9.0	0.0	9.00	9.00 AV6	1		7	400A		0.57	1.97	1.26	6636.38	7			4926.84	3	1.49	7.7		25.56V		2.75	1.01	6765.35	2		7.4	6621.84	5	1,72	, y	4407.47	5	1.75	2.3	1,07	10	1.77	2,35	10.1	,	1.80	2.6		10.47
	10666.00	_	_	00.0		•		91.0					1,97	1,29	;	?	P . C	20.	:	20	1,12	2,80	2.07	7	. 2	2,86	2.05		70	1,57	2.98	•	3	1,40	2,55		69	1,43	2,59	1,40	Z	1,45	2,56	1,94	7.	1,68	2,62	2,12	10.46
		•	٤.	0.0	٠.	1	<b>o</b> ;	0.0	1.55		32	3.50	1, 37	1,39	į	?	P . C	1 24	:	20	1,11	2,78	2.06	4	76.	2, 97	2,15			1.33			99	1,39	5.56	1.1	99	1,41	2° 40	1, 10	70	1.44	2.57	1.34	70	1.47	2,63	2.12	10.48
	6400.00	•	90°£	00.	00.4	,	•	60.0	1.00	•	22	4.	60	1,35	į	,	77		•	•	٠,	2.90	۳.	44	2	2.08	2.14		<b>.</b>	1.1. 2.1.0		•	96	ř.	7.0 7.0	•	96	Ň	2.70	•	3.6	1.23	2.66	2.02	28	1.26	2.72	2.22	11.37
	4900,00		90	00.0	9		en ;	90.0	7.0		90		2,10	•	;	72		01.0	?	33		2.76	2	;		2.82	2,23	•	43	16.0	71.6	:	67	0.97	2.47	90.7	•	66.0	2,53	9g • 7	51	10.1	2,49	2.02	51	1.04	2,55	2.27	12.00
7	3600,90	•	90.0	00.	96.0				•	•	5		1.64			-	67.	ē,		24	0.42	2,17	1,41	ć	0 C	2.32	1,96	,	<b>S</b>	70.0			36	7,62	2,05	`.	61	49,1	10 to	1,11	7	29.0	2,05	1.74	+	69.0	2,12	2.06	14.96
TAPE NA.	-	3	0	0.00	0	,	•	9. E	? •	•	ur.	•	1.30	0	!	۲,	2.15	, ,	_	18	0,21	1.4	0.0	,		1.75	۰.		74	20.00	1,17		53	0.36	1.52	ŗ	62	0.39	1,59	•	31	9.42	1.50	•	31	0,43	1.74	1.14	17.22
		>	9	00.0	9			3 C	٦	2	•	•	1.03	c.	,	•	<b>6</b>	ų 4		٠	e.	1.33	4		-	1.56			11	<b>→</b> ()	100	,	13	7.13	1,46	c/ ° 0	1.3	9,17	1.62	7		0.18		o .	*1	-1	1.50		29.12
	300.006	<b>.</b>	D	3 E 7	, c			3 : E :	. •		3	c	30	٠.				- c	,	-1	٠.	1.98	_	r	•	10.1			7	N A	300	• •	•	3,33	e . E .		•	7.04	1.25	7	0	0.0	1.1/	~	Ð	3,30	1.17	3.	63.78
	4 to 1 co		֓֞֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓		Ē		יַ	r. (	<u>.</u> د د	: :			: m	11 <b>6.</b>		<u> </u>	., - c	າ : ເີດ			e.	۳ <b>.۵.</b>			٠	) :: ::	Ü	•		£ 4	•	•	-	وُ			Þ	٤.	ن • • • • • • • • • • • • • • • • • • •		FI	יים"ר	3 2 1	<u>.</u>	-	٠ د د	) (1)	, ,	47.90
			Ė		•					•	,			¢.				ء ذ	•			3			٠.				٠.,			•		ċ.				ij		: :-			<u>ئ</u> :	r.		ė.	ij		•
		6	PCT.		c10.		(0.2.	הנד.	- c		g	- 110	, , , ,	or.		0 (		, , , ,	•	ė,	PCT.		ים.	5		 	STD		× 6	֓֞֞֜֝֞֜֞֜֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֡֓֜֜֜֓֓֓֡֓֡֓֡֓֡	ער		. 6.2	PÇT.	E (	;	ė,	PC1.	7 1	ים:	er 2	PCT.	· 1	٠ <u>۱</u> ۵.	60	FCT.	٠ د ا	ero.	(j) >
		0.5					Z. ü.									2				12.5.									24,5				32.00				40.5				50.05				IHI				

B-117

TABLE B-62
PARAMETER INTERACTION OFF TAIL
SUBJECT TO CONDITIONS PHIN # 0.00 LANDA # 60.

					AVA								AVA	•			AVA	•				Ş				7				¥				2			7	t							
PARAMETER BAMBE	LINÎT		10.0	9	7 60 0972	92	0.24		1.12	5	0.97	2,37	2.53		4.6	3.16	2,81		2.13	3.25		410.75	8.5	4	2.01	8167.06			2.9.	7969.48	217	2.2	2.5	21. 21. 21.	2.74	10.0	78.5	121	2.01	2.91	2.82	127	2.6	2,42	2.7
Y PARAME	-	-4	0.01	ě	Ē	19	0.19	1,26		\$	0.62	2,11			1,39	X, 05	2,14	3	1,69	3,21	2,56	•	3 3	2.07	2,64	,	200	2.95	2,67	;	2.13	2,96	2,65	*	2,22	2,93	2.43	102	2.29	2,81	2,58	100	2,34	2,71	2124
	8100.40		•	•	•	17	-	•	•	7	05.0			54	1.33	60°N	7	4	1,60	3,33	2.64	:		11.0		;	2 4	3.12			2 2	ac.n			2,07	3.95	2.73	77	2.14	2, 11	2.68	*	2,19	2,40	
	6409.00		0.0		•	16	n.16	1.25	0.43	88	0.64	2,03	1.58	97	1.05		Ņ	T.	1.26	3.28	۲.	,	•	20.0	٠.	;	9 0	2.98	2.86		1.66	2.69	₩,	7.7	1.73	2.97	•	7	1.00	2.85	2.75	2	1.84	2.72	
	4900.00				•	12	0,10	1.08	0.28	33	0,42	1,56	1.00	9	0.76	2,38	1,58	42	0,95	2,83	2,19	:		2.63		į	6	2.70		,	62.7	2,61	2,32	XY	1,36	2,70	2,32	99	1,41	2,60	2,27	7.	1,46	2,47	
•	3600.00	•	10*0	Ď.	•	٠	50.0	٠.	٠.	19	. 22	•	•	92	4,36	1,73	•	2	5,54	2,13	1,45	;	• •	2	•	,		2,21		•		-	۴.	9		2,27	•	24	٠.	2,19	•	9	66 "	2,47	
	TAPE NO. 2500.00		0.00	Ġ.	2		0.0	0	_	М	0.03	<b>,</b>	•	•	0.10	1,33	C	16	0.50	1.56	96.0		\	1.52	6.33	1	25 35 37	1.66	0,92	;	6.45	1,53	0.93	23	1.51	1.73	6.98	42	9,57	1.59	6.36	ţ	0.39	1.54	
,	1660.00	•	00.0	6	5	•	C .	Ē,	<u> </u>	r)	0.90	9	=	+1	0.01	1,00	•	₩7	0,02	1.00	٠	•	` 6	1.29	0.70	•	0 0	1,36		;	111	1,36	•		6.17	1,50	24.0	12	0,22	1.3	9.71	54	9,25	1,29	00.
	06.200		80.0	٠,	() #	ø	3.00	Ć,	Ē	9	00.0			-1	0,31	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3 t	н		1.30	•	•	•	90	۳.	•	4 94 6	1.0	ם ב	•	H 24 - C	7.36	•	N	7.5	, L	) (1)	•	e i	1.25	24.6	`	9,0	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	``
	407.03	•	10°0	ල ( ල (	: a : a : a : a : a : a : a : a : a : a	¢3			5 C	r	. B.	9	L3	7	ກຄືບ	בי בי	10°	i4	0.0°	70 °C	u.	,-	c	5 5 6	. =			i di	•		2 G	5 L	. a.	٤	ا ا	95.	F.3 •		ر. ان	i.	.i <b>c.*</b>	ε.	. P.	<u>ئ</u> د .	
			• • •	- 1 d				· ·	•				; •	٠	c	r į c	er.		6		r		· c.	, c	15.		· t	 	è,		Ė	ü	is ;	٠	e,	٠, ۱	•	ı			•		e.	ໍ່ເ	•
TOUT I N		69.	PC1.				PCT.	r.	. O. I.S.	9€	OCT.				٦.		419	, eg.	PCT.	r (	2:3	0		 	STn.			; ;	510.		, L.	n,	510.	ď	PCT.	, i	;	, E4.	ocī.	• • • • • • • • • • • • • • • • • • • •	, ii	ė,	P.T.	, ,	
ARANFTEN		.6,0				2.0,				4.5				10.10				12.5				 3	5			4			-		34.6			40.5				50.0				11811			

TABLE B-63
PARAMETER INTERACTIEN SF TAIL
SUBJECT TE CRUDITIONS SPIN \* 0.00 LANDA \*

DAMETER	TOWNETTED 1 T. DOT										Y PARAME	PARAMETER PANCE
140C1EN						TAPE NO	H .		,			
	5	D	30°.	20 ° 004	1600,00	2500,00	00 0000	4900,00	6407.05 50.00	0160010	00.0001	- Twill
, Z		. 0	Ľ	2 2 6	-	30,0	-	-	۳	6.0	•	
				00.0		90.0			1.00	1	1.90	1.00
	STD.		00.0	90.0	00.0	0.00	90 0	<b>0</b> 0 <b>.</b> D		0.0		0.0
	•	•	٥	•	•	4	•	•	ř	4	*	MAY 17.87
3	, L	Ė		9 0			Y 0	90,0			0	13
			•			ē	-	4.17	1.46	17	Ś	1.50
	AID.	-				90.0	00.0	73.0	1.34	200	1.46	1.46
	;	-	_		2			•	•	•	•	5641.02 AVE
4.5.	.04	.,	ຍ	•	•	-	•	11	33	7	<b>F</b>	\$
	Į,			•	99.6	0.02	n.10	0,26	n.78	0.32	181	-
	- L	0	. 5	ō	30.0	8	7,17	1.94	2.67	2.58	2,53	2,47
	STD.	5	3 <b>0.</b> 6	Ç.	ŗ	0	1.77	1,35	2.10	2,21	2,17	
				•		•	٠ ;	i	1	;	1	5568.49 AVE
0.0	0				• !	- 7	12	<b>6</b> 5	55	ž į	<b>?</b> ;	R.
	PCT.		ย <b>ต</b> ็ง	90.0	0.03	0.0	9 n	99.0	1.32	1,51	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.77
	.10		•	Ċ,	3.00	1.57	1.76	2,13	2.0		2,93	18°2
	STD.		€	E.	00.0	96.0	1,19	1,36	2,30	7.41	Z. 34	2.2 2.2
		•		•	•		3	S	ŗ	7	2	
16,20		Ė	÷	15	6	51.0	2	200	19-1	1.46	2.63	2,35
			) C			1.46		2.13	68.6		2.85	2.72
	610		•		0.37	0.75	-		2.26	2.40	2.31	2,14
	5	; •		<u>;</u>	•	•			•	•		6288,95 AVE
10.01	.02	.,	כנ	-		22	•	62	8	<b></b>	*	119
	PCT.	B.	00 0	10°6	0.07	92.0	a, 65	1,13	1.4	2,16	2,34	2.6
	.10	6	30.	1,66	1,29	1.45	٩,	2,29	2.9	2.30	2.96	2.03
	510.	6.	ē	e.	0.45	0.56	~	1.58	2.52	2,61	2,52	2.33
,		•		•	•	•	•	•	•	;	36.	
24.5.	2	¢	ے د	7;	D (	6	2 .	2 :	2 :	,	COT .	
	ij	5		4 C				11.1	10.0	7.0		
		, è			•		# T	200				
	310.	, 3	90.		•		1,63	11.11	16.5	<b>C</b> • 24	2.5	5054.22 AVE
2		•	c	0		2		2	3	4	113	
	ט פ		2	56.0	1 E	0.42	. 85	1.17	7.11	2.46	2.63	2.0
		c			1.33	1.50	7.14	2.39	26.6	2, 33	2.92	2.81
	510.		0	30.00			1.27	1.71	2.46	2,55	2.46	2.30
	;	•			•		•	•	•	•		5748.95 AVB
40.5		,			17	S.	24	75		1 40 T	116	136
	PCT.		3 c	3.42	6.17	9.47	6	7.4	2.2	2.55	2.72	9.70 0
	101		<b>e</b> : 4		1,24		6. (	2.41	2.92		2.94	2.67
	519.		0	•	0.42	•	1,24	1.71	2.49	75.3	7.49	3.7
5	7	٠	2	•	•	9	\$		Ē	111	110	
	PCT.	.0	90.0	40,0	0.21	0.51	£ .	1.52	2, 35	2.62	2.79	3,18
		0	200	1.00	1.37	1.50	2,13	2.4	2,92	2.5	2,94	2.86
	STD.				0.56	0.24	1.23		2.47	2.56	2.48	2.34
	; ;				•	,	•		•	•	•	5610.44 AVB
LIHIT	\$			45	27	\$	47	14	113	125	133	153
	PCT.	0	•	7,13	0.31	54.0	•	1.68	2.53	2.31	2°	3.37
	, ,		5 F	1.37	1.44	15.5 16.5	56°0	2,31	7.61	2.42	2.61	2.7
		•	•	2.53	90.5	***		1 . 00		7 · J	2	242 5 20 AVE
	4	ć	7	44 +7	44 94	12	74 41	40 01	15 75	15.14	14.64	
	,	;	31.	•	`A • ? •	7		34.4	*****		,	: ; ;

	9FF TAIL 9.00 LAHDA =	
TABLE B-64	SUBJECT TO CONDITIONS AND A SECONDITIONS	

	PARAMEYER RAINGE	LINÏT	• (			1. 01 AW	2	6.13	1.23	25. ·	274 . 36 AW	17.	2.17	1.67	7386.38 AW	2 ;	7.	20.1	7255.84 AW	124	2.78	2.41	90.7	117	3.17	2.90	2.90		2.5	2.06	8.1	944.53 AVE	25	2.86	7.9	6461.25 AVE	797		1.9	6318.49 AVE	167		7.7	6203.17 AVE	179	3. 2.	2.78	1.05	43.45 AVE
	X PARAME	10000,00	• ;				12	111	1,47	65.0	*	9.6		1,29	;			1.7	•	1	2,27	2.74		114		2.87		126		2,42			130	2.82	1.89	į	135		1,30		142	3,10	7.7	A D 3 1	153	3,27	2.68	1.87	14.14
		8100,00	• (	D (			•	8 ° °	1.25	9.0	98	0.50	1,75	1.09	;	•	1.1	1.53		2	F.	7.67	7637	182	2,13	2.42	1,42	7.1	2.34	2.5	1,62	;	2.44	2.49	1,62	ì	176	7.70	1,65		130	2.0	2	•	1-1	2,73	7.4	1.44	15.44
		6400,00	•	2		•	•	9a.r	F. 34	a, 75	X	92.0	1. E	1.10	•			1.41		•	1. UB	2.30	1.36	=	1.50	2,44	1.53		1.78	2.40	1.54	ï	` *	2.42	1.54		בר ה		1.58		t i	5.5	2.		119	2,28	2.12	1.56	17 .7
		4900,50	0		9 6	•	•	0.03	1.03	0.00		0,21	1.4	0.83	1	10 H		1114		57	0.97	2,12	1.00	5.9	1.20	2,31	1,35	**	1.36	2,31	1,37	;	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	2.30	1,39	;	6	2.27	1.4		2 ;	10.0	2.21	;	•	1.75	2,21	1.44	14.53
90.09		3500,10	9 (		) (i)	•	-	٦,	1.00	00.	•6	30,1	1.25	. 43	8	2 2		75	•	35	9,	6 t	,	7	99 6	1.79	1.10	7	<b>D</b>	£ 4.	e e	5	r e		<b>5</b>	;	<b>0 0</b>		1		79 (	<b>E</b> .	•	•	36	1,13	1.42	٠.	21,13
7 647	TAPE WE	2509,70	D 6		000		-	Ē,			**	10.0	3. J	ac.9	•	0 <u>(</u>		6.33		13				19	0,25	1.53	C. 31	96	98.0	1.52	46 °C	Ē	1 1 1 1 E	1.56	9.79	;	B 7	10.	16.0		11	J			52	25.0	1.50		31.14
		1640,60		7 C	3.03		<b>e</b> r	7.00	50	0.00	0	0.03	0.00	0	•		, E	50.5		2	N 0		3 3 1	,	90.0	1.14 1.14	2.35	11	1 .7 1 H : 12	1.18	фр. U	;	110	1,12	C. 32	;	7 5		'n		21	7.0	7 . 1 .		5.2	1.76	1.7	Ç	34.15
		ວຍຄູາປ	ء ء د		1.70		0 (	) : F (			(3)		(2) (2)	30.0	E,	ָ פּיָּ		5.1		ن دن ا	3 F	) (	•	3	e e	() () ()	1 13 4 10	н	# # F	J. 1	() ( )	J	, ,	1.	ja P	•	n #				^;			•	t3 ♥	31,	<u>,</u>	,	34.35
							<b>3</b>	: · ·		•	~3	ر • •	, C	c)	:	 		į.		3 (			•	د	ë •				י ביני	t c	· .	-	•	e P	t. r		1	• (	·.					•	`	· ·	· •	•	£4, €1
		E.			."		''(	,	5 e	•			En (	•							įė	. i	•	, ,	<u>.</u> .	en e	•			er i	,			,			r	.';	. ' ;			• '	٠,			٠,	<b>'</b> ,'	•	1
TOTAL . WILLIAM C				, <u>, , , , , , , , , , , , , , , , , , </u>	STD.		, e			•	4.5. 48.	POT.		S13.	6		 . i.	٩٢٥.		12.5. 49.	; <b>;</b>	. E		14.6.	PCT.	, F	• ii ·	24.5. 48.	act.	2.1 2.1	, ci	42		; <b>,</b>	415.		n F		,C19,		, i. j.	; ,	1 t		.e. Likii	,	; ;	:	()

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	BFF TAIL	8.00 LAMBA #	
TABLE B-65	PARAMETER INTERACTION	SUBJECT TO CONDITIONS ANIA .	

Aire		LIMIT	, , ,	7.0		74 AVE	•		:			1.7	i,	÷:	27	ı	*	14. 17. Ave			5	.52 AVB		<b>.</b>		. 86 A78	3			W 2.		7	10.		2:	3:	.34 AV6		4	3 25	. A A A	.20	.27		25 AVE
TER R		3		•	4 4	3005		•	-	-			-	7	200	. 🕶	~	7		•	<b>~</b> ·	1818		e i	N =	1630	•	* **		77	~	₩.	75		N	N •	6123	(	n .	• ++	4023.63	n	~~	**	1480
Y PARAMETER RAM		16640.00	*				•	**	7			0.41	1.76	1,92	7.3	1,16	1.3	. u	107	1,77	2,17	79.1	717	2,12	7.7		126		1.4	:	2,46 2,46	2,32	1,51	191	2,56		7	977	2.07	1,53	871	2,81	2,28	1.50	.,
	;	6186.50	ri (	# C			•	B. R.	1,00	04.0	ř		1,68	1,17	*	. S.	2.05	1,2	\$	7.7	21.2		*	1.76	2		191		1,42	•	2.5	2,30	7.7	116	2,21	65.5		122	2.2	1.51		2,42	2,26	1.49	•
		6490.00	4				•	80°E	1.00	9.0	ř		1.78	1,58	•	0.77	2.02	<b>1.</b> 2	2	1.13	70.7	1.5	22	1.4	26.2	}	. 67	2.53	7.		1.71	2.26	1.47	101	1.61		;	105	1.69	1.1	•	2.02	2.16	1.46	•
		4980,50	7		D ( )		<b>1</b> 0	0.04	1,98	0.0	*	22.0	1.69	0.77	2	0.45	1.97	1,63	*7	0.0	7.07	£0.1	55	0.00	20.2	•	. 67	7 17	1,06	ř	1,19	1.99		83	1.29	1.93		87	1.00	1.13	•	1.49	1.89	1,10	
	**	3600.90	9 6				7	0.01	1,00	0.00	•	6	4,58	6,43	17	n.22	1.65	9,4	30	NO.	1 30	•	88	98.0	7.6		<b>6</b> ;	16.	0.76	•	76	¥.	9.10	;	582	1001	•	76	7	200	=		1,58	7.	40
-	TAPE NB.	2500,00	* c	į			-1	10.0	9. T	0.00	M	0.03	1,33	6.47	•	90.0	1.40	\$ * C	12	21.0	1,53	,	77	0.17	1.67	•	27	1.22	0,42	ş	e e	1,29		7	ij.	9		5	17.	0.55	9	B. 59	1.25	9,51	***
1		1500.00	3 6		2 6		S	00.0	0.00	09.0	•	0.01	1,90	0.00	•	0,01	1.00	5 5 5	2	20.0	900		2	2.62	90.1		<b>4</b>	1.90	0.0	o	0.08	#:	16.0	12	91.0	9 6		16	1.1	0.33	10	0.24	10.	0,20	5
	9	nc*086	3 C				<b>a</b>	3.10	02.9	30.0		90.0	36.	9 <b>0</b> °	ف	00.0	36.5	3.50	و	9 6	9 6		•	0 c	) C	•	ت د د د	90.0	90.6	٠	96.96	e .	<b>1</b> • 0	+1	e e		•	ې ۱۰	7.75	3.0	1	9.40	3,00	3°.	4
		10° LD	3 E				,	0,10	20°C	70°	c		3 <b>0</b> °	ŋ <b>, c</b>	9	99.0	7,00		. د	3	ສ : ອີຍ	•	c)	e c	. c	•	7 G	0.00	<b>.</b>	6	, j	۳: د د	9	·5 ;			•	¹ «	. C		Ψ,	5	9		137 64
B.	•		•		•	•	•	9		6		6	0.	204	. 1	0	i 2 6		٠ ;	r, è		•	. (			•	ċ	6	0	٠	6		3	•			•		0	e I		ic.		ָּט	
RAMFTER LT-191		<b>6</b>	P. 7.			•	2.01 46.	PCT.		STD.	4.5. NB.	100		STB.	8.6. 38.		i e		2.5. 18.	֖֭֡֝֝֞֝֞֜֝֓֓֓֓֞֝֝֓֓֓֞֝֞֝֓֓֓֓֞֝֓֡֝֞֝֓֓֓֞֝֡֡֝		;	. d d.	PCT.	. d15		24.5t AB.	, a	5TD.	32.6	POCT.	- 1 C		40.5. 48.				9		stb.	111		⊢ ( 4 (	513	4

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	aff tail	C.00 LAMBA .	60
TABLE B-66	PARAMETER INTERACTION	SUBJECT TO CONDITIONS AND E	126.

*		•			74	•	ю	•		¥	• •		. ~	7 AVE	<b>.</b>	•		4 AY		•	•	7 Y Y			_		4 AVB		,		8 AY6	<b>.</b> •		. 141	944	~	<b>.</b>	• •	JAF 6		•	<b>.</b>	A 46		•	~ .		200
PARAKETER RANGE	LINI		ě	•		•	•	÷			•	4		6389.77	•		ě č	6687,5	11	1.3	i i	7.6747		100	-		6617.1	17		6	6391,2	<b>21</b>	7	1 6	6162.2	14	ri i		6081.4	7	2.2	<b>•</b> •	5041.18	17	2.6	<del>-</del>		۱
X PARAK	15800.00		ě	0.00	ě	•	6.03	1,00	•	;	1	1.24	6.55	. 1	96	27.0			:	1,36	1,73	6.79	110	1.60	1,63	0.77	•	118		0	•	126	7.			131	2.00	1.		136	2.04	<b>1</b>	1.0	168	2,37	1.77	14.0	
	8180.00		0.0	9,40	9.0	•	56.0	1.40	0.0	•	-	-	96.0	, !	47	i e i	7 0 1	•	**	1,13	7.4	<b>9.</b> 0	7	1.83	1.78	94.5		103	. 42	7	•	111			•	116	1,72	1.57	1	121	1,78	**	:	152	2,48	1,71	2.2	
	6400.08		ē	0.0	Ē	•	50.0	1.00	٩.	,		1.20	30.0		<b>6</b> 0	6.60	4 F	:	69	9.0	1.57	37.5	11	10.1	1.68	6.73	ļ		MA	47.6	•	) • (	1.01		•	•	3.00			163	1.4	1.76		134	1.73	1.62	0	
	4960.00			0.00	6	4	•	0	ë	•	? F	10.1	96.0			.,	9 4	•	<b>:</b>	ń	1.50 1.50	•	9	0.72	1,53	6,67	,		7		•	۲,		•	•	22	10.1	8 1	Ď	2	1.06	1.69	0.63	189	1,35	1,55	29.0	
•	3609.00			06.0	e.	^	0,92	1,60	٠.	•	•	100	0.67		15	3		-	27	9,33	1,52		32	100	1,50	1,71	•	0 0 0 0			•	<b>9</b>	10.0	1	•	25	ě	1,00	<b>3</b> 4.	<b>58</b>	1.	4 93		7	1.96	14 e (		
	TAPE MB. 2500.00	0		9.00	•	8	0,02	1,60	6	4	۰ د د	1.20	0 40		<b>-</b> :	90.9	77.0	•	13	0.14	60 t	0.52	16		1.31			2 2	1.45	0.57	•	23	7.	17.0		<b>5</b> 6	36.0	1,00		35	0.36	1.29		25	0.50	16:1		
	1600.00			•	<b>-</b>	•	00.0	0.00	6	c	<b>&gt;</b>		0.00		•	9	10	:		٠,	90.	5	•	9	1.00	•	,	ی م د د		0.0		<b>49</b> ?	, D	) M	}	•	0.07	21.0	•	10	9.09	1,10	0.0	35	0.30	90.1		
	900.30		0.00	0.0	n	0	00.0	£.00	0.0	6			00.0		5	9 6			>	0 0	0	9.0	•	0.00	9.00	0.00	•	= F	00-0	3.50	•	-	4 6	90.6	•	••	6.0		•	~7	9.0	20.1		13	01.0			
	40.00		9.60	0.0	ຍຸ	0	7 <b>0 0</b>	0°0	٠.	•	3 C		0.0	,	ن د د	3 c	0 C	•			2 . F	•	J	•	3,00	٦.	,	ن د و	00.0	00.6	•		. c		•		2 6	•		0	90.	20.0	•	N	7.0%	ë ë		
<b>-</b>	0		:0°-	0		1	5		2		'Ł	6	0	,		è		•	•	0	p c	•	•	0,	b		,	· • •		63					•	υ,		) C	•	•	•	<b>E</b> ) 6	•	••	0			
ARANETER LT-DBT		0.5. NB.	PCT.		\$10.	2.0€ 48.	PCT.	pT.	STD.	•	:	0	510.			֝֞֞֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֓֓֡֓֡֓֡	STD.		12.5t NB.		E	.n.s	18.0. 88.		DT.	STD.		24, 3. AB.	Tr	STD.		32.01 MB.		STD.		40.5. NO.				50.00 40.		J.		LIMIT 48.	<b>P</b> CT.		;	

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_	AFF FAIL	1.00 LANDA =	00.
TABLE B-67	PARAMETER INTERACTIRY RFF FAIL	SUBJECT TO CONDITIONS ANIA #	LAMB 7 244_DD

RAMETER	LT-987				•						WARAN Y	PABAMETER BANCE
						TAPE NO	**					
i	q		404 204	0	1600.60	2500.96	Seun no	4900,00	6400.00	6100,00	10000,00	LIMIT
í		.0	10°E	-	_	9 6		- E	- 2	ri E	7 5	2 0
	7.	0	0.0	C		00.0						
··	.TD.		0.00	90.0	00,00		0.00	00.0		E		3
									•	•	•	7667.41 AVE
2.01.	9	•		9	9	<b>CV</b>	•		•	•	7	<b>*</b>
4		2	300	3000	ביים	20.0	20 E	60.0	90.0	94.	40.0	<b>3</b> '
•		<b>3</b> (	3,63	30.0	0	6	100	1,20	1.33	1,33	1.29	 
n	•	•	0.00	9.0	D .	Ē	69.	0,40	8,75	0.73	0.70	***
3	4	•	•	d	r	•	•	**	•	;	\$	
:		, c	•	•	3 6		3 ;	9 9		?	"	2:
•					70.	•			7.4	***		
•		; è					D	21.0	1,52	1,50	# C	
л	•	96.	a :	90.0	~	Tc 'a	17.0	55.0	0.0	1,00	1,00	20.5
.0.8	<b>E</b>		<	ی	•	22	72	*	7	*	×	
	ú	0	00.0	9	٠.	27.	0.27		, M.		2	2 2
	uT.	Ġ	200	200	1.00	1.25	1.42	1.68				
•	TD.		90.6		-	0.63	4				4.42	
						•	•	,	•	•	-	6147.54 AVB
12.51	9		3	•	•	15	39	55	*	*	9	*
	PÇT.	;0*·	0 <b>0°</b> u	0.00	<b>90.0</b>	0.16	3,42	0,73	1.11	1,35	4,4	1.57
	7.	0	0.00	00.0	1.00	1,33	1,36	1,65	1.88	2,04	2,83	2,05
S)	.15	6	ם, פ	e	۹.	G5.5	9.70	•	1.04	1,22	1,28	1.29
												5978,37 AVE
19.61 19.61	ŗ	1 - 1	<b>3</b>	ا د. ا		10	*	65	98	17	101	110
	֖֡֞֜֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	b c	3) E: (	00.0	0,04	0.16	6 . S.	0 50.0	1.28	1.58	3	200
•		2 6	, on	200	٥,	1,28	9 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1,65	1.67	7.0	2.03	2.2
,	<u>.</u>	1	9.00	3.40	-	8 . D	9.67	0.79	1.62	1.72	1.27	
24 3.	Œ	٠	=	u		•	24	7.6	3			
	Ų			9-6	2		3	•				
•			000	•	1.00	1.29	1 2				70.0	R,2
•	.0.	U	2	0.00	00.0	6.61	9	M C	7		1.24	2
		•	•	•		•	•		•	1	:	5737.46 AVB
32.01	æ.		3	<b>(3)</b>	10	30	99	85	115	117	124	
	PCT.	0.	3 <b>0.</b> c	J. 40	0.0	6,30		1.03	1.52	1.44	1.1	2.08
	-		30°0	9.90	1.06	1.27	1,33	1,61	1.82	1, 17	1,96	2,01
<b>v</b> 7			ם בּ פ	*	0.00	0.57	99".	0,61	1.65	1,23	1.27	
5 07	q		t,	-	÷	2	;	6	•	į	•	5577.81 AVG
		, r	e •		2 2 2	\$ 5	7.0	24.	*11.	77.	201	139
	Į.	٥	70,	00.0	00.1			64.				
ائ	.10.	0	ກຸດ	۲.	00.0	76	7.73	76.0	60		1.32	
		•	•			•	•		•	) ; •		5433.57 AVB
50.0	9	٠.,		•	-	37	*	7	117	129	136	
•			50.	00.0	0,13	9.39	6.81	1,21		2.00	2,11	2.2
•		2	_	٥	٠,	1,32	1,56	1,62	1.79	1,4	1.94	2.00
,7			, .	Ó		74.0	1,73	99.0	1.98	1,20	1,33	
11811	9	•	-	2	17	9	4			17.	97.	5425,49 AVE
•	Ç	0	-	٠.	9.29	0.52				20.0	42.0	
	or.	0	1,00	1,00	1.09	1.36	1.30	1.69	1.5	1.17	-	2.03
•	,TD,	0	0,00	e.	6,29	0,51	16.	0,95	1.15	1.35	1,39	1.45
•	2	ė	414	11. 97	6.4		1	,	;	3	;	5032,97 AVG
•				14.41	) · O	90.0	3	27.81	23.47	21.40	21.33	26.92

は、これでは、これできるとはなるというできると

						Ž			3				Ĭ			5				Ĭ				Ž			1				Ž			7				A			3	\$
	Y PARAMETER RANGE	LINIT	<b>-</b> 1,3			<b>416.</b> 43	11.0	2	2007	£	o d	1 2	7865.45	3	2.2	2.5	*	21	5.5	5065.54	3	2	1.32	9574.12		2.0	56.4		2.1	12	5421.84	7		1.32	2	<b>3</b> 5	7	5078.12	Ĭ.	1.1	1.34	38.16
	Y PARAME	10000,00	٠٠; د	100.1	0.0	•	0,11	1,33	•	*	0.28	0.71	:	. 2	1.84	<b>.</b>	*	7.0			3 !		1.05	ř	1,07	1.0	1.1	£	1,14	1.42	3	1.25	1.86	1,14	=	1,32	9.	•	Ξ;	1.18	1.12	34.73
		6100,00	***	9	0.0	•	70.0	1,13	0010	2	3,74	1,57	:	0.52	1.76	۲. ۲	2	7,73	,		. 53	7.75	7. 24	:	1.02	F	£. 24	*	1.0			1.1	1,42		2	1,27	7 2	•		1	1.45	39.41
90.00		6498.69	<b>-</b>	9 6	De	•	, e	2.0	9	2	A.21	0.0	:	1,67	1.59	ē.	25	6.67			2		2.02	•	*	7.		2	10.1	1. N.		1 1	1.72	P.	2	1.18	10.6	•	107	1.79	1.11	33.81
PFF TAIL 2,00 LAMDA E		00.0061	0 (	0.0	00.0	M	0,02	8 6	96.0	13	9,13	1,23		22.0	1,39	0.67	5.4	07°D	1.4		22	66.	0,74	•	0,73	1,53	0,72	67	16.0	1.71		, e	15.1	2.74	7.9	0.97	1.0	•	<b>.</b>	1.65	0.87	37.48
68 Ion 167 7/ = 7,01			<b>-</b>	÷.	5.	•	26	F 6	9	=	0	, E	, ;	0 T T	1,38	<b>9</b>	50	22.	,	•	<b>5</b>		9.	5	27.	7	6	3	67	1,59	ř	15	92	66.	٧0	. 55		•	£ ;	64.	27.	46.54
TABLE B-68 PARMETER INTERCTION SOCIET TO CONDITIONS ANY A 142 DR		2500,00		0.00	30.5	-	16.0	30.1	3 6 6	n	9.05	90.5	•	0.35	E . H	02.5	11	6.0	5 C		, c	1.90	900	CC		00.4	02.0	27	22.0	900	ž	0.27	M I	0.17	<b>;</b>	B. 34	10		e.	17.	0.40	96.10
TE CONDITE	•	1695,00	e e	00.	00.0	æ	00.0	ر. وي		o	<u>ئ</u>	200	c	0.0	9.0	e e	( <b>3</b>	9.00		•	rd ;	100.5	9. C	,	3.62	1.63	<u>ت</u> د	7	9.0	H 0	•	n . E.7	1,96	0°0	12	9,16	3 23 - E. + E		J 1	5	22.	E * . ve
SJH JEGT		967.19	ن د. ۲	100°E	0 E E	.a	5.5	30 E		c.	(3) (6) (6) (6) (6) (6) (6) (6) (6) (6) (6	9.30	ď	0 0 0	0.5	: :	5		3 L.		 ?	a ja Sign	, e	c.			)  -		.) (1)	3 m 1 c 1 c	-	بر. ع		J. • C	н	*1 .	) ; ; ; ;	•	ξ. C.	1 (1) (1) (1)		124.55
		.a. ru≯	" č	, e.	າຍໍ້			2 E		7	မ စီး စီး	្រី	•	າ ເກ ຍ ເ		<u>.</u> .	٠.	i e		•	~ c	2 to 10 to 1			i, ij	e (		••		) #3 L- [ *   (		, L				ا د د د د	1 • 1	•				· .
				, r	ė;			٠, د	•		i t			E)					<b>.</b> • .			, <del>.</del>			•		•			•		٠,	٠. ۱	•		Ç	•		٠ ،	.'.	٠.	•
	+11-1 Titua		6.30. FCT		419.	2.6. 43.			•	4.5. x9.		STD.	1	PCT.	5	້ ເມື	2.5. 49.	ن د د	- E-	,	F. F. S.	 	E .	, <b>,</b>		- 1	יי ניי	72.5. va.	PCT.	 	e e		-1	٠٢٦).	54.6. 59.	PCT.	 		6 P L L L L L L L L L L L L L L L L L L	, •,		;;;

B-124

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TABLE B-69	PARAMÉTER INTERACTION	SUBJECT TO CONDITIONS ANIM .	LAMR T LIMIT

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ETER RANGE	LIMÉT	₩,	8.12	2. 2.			2.	r:	_		<b>6</b> 1.	2.18	9602.5	2	<b>2</b> .		20.99	21			-	2					2.23		-	1.1	, i	£413.22	2		2.27	6389.47 A		17	2.22		7.	P. P.		20.62
M PARAM	10000,00	•	2	2	2		29	4		_	_							11									7				2						C7 -	2.79	1,45	37	9,52	7.7	}	32.86
	8180,88	-	E .			+	0,01			•	= 1	( ·	:	13	9,17	7		#1	77.	1		75	9	1,14	ř	. 33	1.78	1.39	23	1,34	25.		52	90.0	1,30			1.74	1.26	Š	E. 47	1.74	•	34,65
	64.88,00	•	0.0			•	90.0			•		2.1		11	0.13	1.67	•	3		6,72	. 1		1.4	2.4	;	1.28	1.30	1.83	22	1.29		70.1	22		1.00		CN.	1.6	8,98	i i	14°6		;	37.38
	4980,80	-	9.0	0 0	9.0	•	•			•	5	C2*1	;	•	9,18	7.0		13		0.62	;	12		99.0	•	•	1.58	•	10	0.25	1,64	?	56	92.0	16.0		8-28	1.59	6.69	<b>58</b>	0.57	, e	-	40.49
•	3600,90	•	00.00		0 F.		6	9.0		N	0,02 0,02	<b>3</b> 6	,	<b>5</b>	96.0			<b>a</b>		9	•		12.1	0,41	¥	15.0	**************************************	1.	16	0.18	8 4 4 6 4 6 4 6 4 6 4 6 4 6 4 6 6 6 6 6		11	7.19	9.5	•	12.5	1,37	1.58	22	0°"u	1.40 0.40 0.40	•	48.43
4400	2500,00		ė		•	•	04.0			<b>N</b>	6.62	7 6	:	<b>+</b>	40.0	1,63	;	<b>*</b> 5		0.43	•	9	1,17	0,37	đ	0.09	1,22	7	0.	60.0	1.22	1	91	1-20	9.40	40	6.31	1,17	0.37	<b>52</b>	9.20	1.23	! •	64.34
	1600,00		٠,	9.00	2	0	30.0	0 C	•	9	c (	9 6	3		<b>~</b> (	3 C	١.	~ 6	100		•	0.0	1.00	•	•	50.0	1,00	9	•	0.03		•	• ;	1 000	0.0	•	-	1,00	•	13	41.0	1,00		94.74
	30.000	-	00.0	9-0	20.5	0	e.	5	•-	_	9			_	Ģ.			e> 0	30.0	E.	c	90	9	ē	ى	٠,	0.0		a	5	0 C		<u>.</u> ا	00.0	36.6	,-	0.31	1.00	3.36	ى	9 0	3. E		134.95
	46,04	<b>3</b>	J. 0.	2 C C		9	90.0	# C	: :		2 6			<b>3</b>	2 . D (	7 A	•	7 E	0.00	00 .	ė	_	00.0	•	=	3 E E	C C C	60°.	3	0°0	0 0 0 C	•	- <u>;</u>		e e	c	, aa,	F .	ດລີ້	~	٠ و و	3 6	•	163,45
		. ,	ا •				ė,	s e	•	•	0		•	٠.,	b e		•	ć		0		٠,	2	5	•	<u>.</u>	t i			0,0	ų ė	•		3 C	13	•	9	u.	•		c. c	, E1	,	E.
KAMETER LIFTBT		6.5. ca.	PCT.			2.6. 38.		. E. S.	• 0 • 6	4.5. 148.				3.6. XB.	בי י	. TO.		12.5, 48.	, i	STD.		100 100	, ta	STD.	24. 546.		Ę.		32.048.	PCT.	, e. r		40.5. 48.		STD.	50.0.	PcT.	٠٢.	sro.		, c.	ATD.	,	
E Y	•	3				~				*				10			1	15				9			4				32			,	3			r.				LIMIT				

		60.00	
	369 JESS	n.00 LAMDA =	C C
TABLE B-70	PARAMETER INTERACTIAN 360 JESS	SUBJECT TE CONDITIONS PRIN =	2

						*				•	2				2				3	}			9					7				2				921				974	•			97.	# *				Ave
DABANCOCO BAMOS	TEN NAMED	LIMÍT	9 (		76.0	10799.18	6	ri (	Z. 8Z	2.2	720.0021		2.73	4.73	10094.96	215			77.0	220		4.36		72.4114		1	7.46	7859.95	21.4	9.32		7704.11	220	<b>9.</b> 3	5.42	76.4	232	9.62	5.19	7.2	235	9.0	5.15	7.24	1767.78		5.13	7.23	7558.05
- DAMAGE		18600.00	7		6.0		2,	7.1	1,28	N	142		2,94	1,07					30.18	284	6.19	DE . N	3,81	,	7 1 1	4.52	4.42	1	248	7.43	4.00	•	<b>586</b>	7,59	4,62	4,53	218	7.71	4,43	4.5	162	7,76	4.40	4,48	266	25.	4.38	67.7	
		8180,00	21		0.30	•	<b>Z</b> :	64.0	121	20.00	0.1	2.18	1, 39	1,75	,	<b>9</b>	3.5	2.7	2.00	1.13	5.43	3.66	3,71	;	d 5	7.7	92.7	•	1.3	6,72	2	;	202	9 . v	4,27	4,13	214	7.80	4.10	4.1	216	7.04	<b>8.</b> .7	e. ,	***	7.5	96.4	4	<b>.</b>
		648h.88	<u>ه</u> د			•	200	9.50	7.	8.32	•	7,	1.86	1.40		166	9	2.52	۲.03 د.03	178	1.51	3.32	1.62	į	171		3, 36	)	176	50.0	3.41 4.52	1	. 143		3.75	3,48	195	5.59	3.59	3.44	197	5.43	3.58	3.42	007	44	- M	3.44	}
		4960,00	•	, d			38	0,37	1.1	0,52	ě	1.28	1.76	1,27		139	5,49	2.24	<b>7.1</b> 2	149	3,31	2.79	2,63	,	124		2,96	•	159	4.01	3,16 1,16	1	166	4.12	3.11	3,07	176	4,21	2.2	3,62	178	4.24	2,98	3,01	•		2.97	3.04	
10.61	+	360".00	* !	20° u	9 C	•	58	92°u	1,14	2,43	**	7.79	4.46	9 ° 6		110	, , ,	1.70	1.44	121	2,10	2.17	2,10	ţ	129		2.30	•	135	2,43	7.0	•	141	2,72	7,42	2,36	151	2, A.D	2,32	2,51	151	2.83	2,32	7,38	73.	יין ניין ניין	2.12	35	) ; •
CAND :	TAPE NO.	2500.00	H 2	100	9.0		•	90.0	1.23	99.5	9	3 P.	1.23	6.92	1	21	76.0	, s	74.	72	9.38	1,53	0.47	;	r c	1.65	1.00	•	86	1.25	1.1		92	1,31	1.78	1.12	100	1.37	1.72		161	1.40	1.73	1.10	55.	761	1.74	4.1	! }
3			۰,		90.0	•	~	20.0	00.1	00.0	•	٠,	30.1	•		23	12.0	5 T • C	6	35	6,32	1.14	64.0	;	7	1.27	09.3	1	*	6.49	1.39		47	1.54	. 45	0.74	53	0.59	1.40	0,71	53	0.66	1.42	0.74	2	* *	1.4.1	9.73	)
		900.00	<u>د</u> د	9.0	90.0	•	9	30.00	B (	3,00	•	20.6	1.30	00.0		٠,	C		90.5	ه	9.08	1.25	0.46	,	;;	1.17	6.5	•	13	0.12			10	0.14	1.13	9.48	3,	9.10	1.10	3,44	36	0.16	1,16	7,4		7.	1.10	9,43	•
		467,00	C 6	200	90.0	•	0	80.	60°	50.6	c	, <u>.</u>	9	00"		٦,			( f. • 1.	a	ຄູນ " ເ	. <del>.</del>	, G.	•	ء د			•	5	ଅ : ଅ :			د		ງລູ•ລ	3 C	-	10.	1.00	າ <b>ມ</b> ີ ເ	-	, 01.	1.00		11	4 6	00	) E.	•
		10.11	· · ·	2 6	C		. (	ه د	2	. 0 .			i.	20.				2		• •	9		: :		ć	ė	13	•			a e			<b>.</b>	, i	. D .	,		. 0	:: ::		σ.	6	: :	•	c	, ė.		•
F. 6. 7 . 0.7	Ĵ		9 1		. TD.		4 (4 ) (4 )	ָבָּי. בּיי		SID.			1	STD.		, 269.		÷	•		PCT.	DT.	sta.		ار 10 ع		STD.			•cT.		• •		PCT.	Tal.	<b>.</b>		PCT.	. 07.	sto.		PCT.	ut.	\$10.			. I.	STD.	
227 284 04			ų. V.				2.0									9				12.5				9	10.0				24.5				32.05				40.50				56.0	; ;			1181	3			

TABLE B-71
PARAMETER INTERACTION 360 DESS
SUBJECT TO CONDITIONS THIN TO 0.00 LANDA TO 15.00

A Anna			1.65		2	1.96 AVB	2	29.		Ŗ.	124		67.	10.5			3	2.57 4.67 AVE	-	11	10°		162	01	98-	6367.87 AVB	7.75		.27	1, 96 AVB	33	76	124			75	.27 AVB	476		- C	. B4 AVB	29		
4 4000		j			_	1231	•		•			**	74	7	2	•	-	7		•	77 (	5473.42		-	re 44	636		7 P	-	6134		-	2.2		-	TV (	5997.27	•	- 1	74 P	5074	•	P 174	
V BARANCTER BANK			6.05	1,00	•	i	<b>D</b> (	1619	69.	1,62	100	2.04	2,36	1,84	102	4,24	2.79	<b>92 2</b>	279	6.03	2.71	Z. 33	338	7,08	2.27	<u>;</u>	687 1	2.48	2,19	,		2,45	2,17	416	8,19	2.5	9447	422	8.5	2, 4 2, 4 3, 4	} ;	125		,
	80.00.8	2	0,95	1,68	96.0	i		76.0	1,57	10.40	707	1. 21	2,38	1.70	1.76	3.40	2.74	2,25	248	5.39	2,72	C 7	210	9219	2.31		988	2.53	2,22		71.7	2,49	2.19	368	7.33	2,50	• 1	372	7.42	2 C	1		2.53	
	4074	4	9,65	1.00	6.9	i	90	26.0	10.1	1.0	79	1.53	2.29	1.87	145	2.98	2.57	2.12	211	4.22	2,51	<b>7.13</b>	252	2	7.01	:	299	20.0	1.97	ļ	920 15.90	2.31	1.95	330	60.9	2.31	1.1	334	6.46 146	2.52	:	257	90.0	
	60.00		6,02	1.03	90.0	į	12	25.0		24.0	73	1.12	1.92	1.38	121	2,12	2,20	1.71	181	3,16	2,15	1,80	220	7.2	1.60	3	265	2.03	1,52	į	4.57	1,99	1.49	297	4.75	2,00	1.0	200	4.63	20'2		700	2.00	
k.	3660.30		6,92	1,00	90"	i	2	77.0	7		48	0.59	1,54	16.8	86	1,27	1,01	I. UV	135	1,95	7	1,164	168	2,47	1,25		214	1,72	1,15	i	3.16	1,71	1,15	241	3,32	2 d d	011	544	N .	1,15		C . 7	9	
	TAPE W3		10.0	1.80	0 ·	•	•			90.0	20	0.16	1,15	6,36	¥	94.0	1,26		68	66.0	H . C		114	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	70,0		152	1 m	0.76	•	1.90	1.42	0.77	174	2.62			179	2.00	0.63		700	1.50	
	1600,09		00 0	0.0	00.00	•	<b>*</b>		9 6	2	1	90 0	1,14	0,35	23	0,21	1,13	* ? • •	45	19.0	1.21		75	9,00	9.0	. 1	9 6	1,28	0.60	ć	96.0	1,26	19'0	96	66.0	6241	2	66	9 . 0 .	70.0		901	1.34	
	00.096	(3)	36.0	0.0	90.0	c	• 6				<b>~</b> 4	0,01	1,00	0.0	**	0.01	10.1	•	*	50.0	H C		ដ	60°0	0.0	. ;	9	1.00	0.00	c.	9.18	1.00	9.90	22	0.22	1,00		29	0°50	90.0	•		1,16	
	400,00		00.0		•	=		200	•	•	•	00°u	3 C	90.0	•	•	e e	2		000	ė c	2	1	= = = = = = = = = = = = = = = = = = =			=	0	٠.	3	٠,	0.0	•	٧	200	)  -  -	,			9 6		0 £	9 4	
	16.,0		6	D.		•				,	ü		:	.i 2	••	JO* J		) W.	LI,		) (c)		.,		3	(	9	0.0	<b>30.</b>			70		Laj			<u>:</u>	' ' <b>(</b>	3 (	, (, ) () ()	•	1 5	11	
KAMELEK LT-DBT		0.5c MB.	PCT.	E	9.0	2.0: km.	PCT.	-	510.		4.2: 18.	֭֭֭֭֭֭֭֭֭֭֭֭֭֭֭֭֡֝֝֝֝֓֞֝֡֓֓֓֓֓֓֡֓֡֓֓֓֓֡֓֡֓֡֓֡֓֡	'n		8.0c m6.	100	. בי	<b>;</b>	12.50 NB.	בינ פני	M.		18.00 MB.		\$19.			DT.	STD.	10 Gr.	100	10	210,	40.50 NO.	, to	STD.	č	30.0C	1	STD.			DI	

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TABLE B-72

# 25 E 5.5. 5.5. 5.5. 5.5. 36.00 3.20 3.10 3.10 60.69 PARAMETER INTERACTION 360 DEES SUBJECT 19 CBNDITIONS PHIN = 0.00 LAMDA LAMB T 54.00 0.40 1.28 1.58 0.93 1.22 0.56 90.00 2000 9000 12 6 12 6 16 6 9 0 0 455 2259 PARAMETER LT-BET PCT. 701. STD. 67. 27. 570. 86. 21. 51. 7 17 E ST. F. 4.7. 8.00 18.C. 32.6 24.5 50.6 LIMIT

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TABLE B-73
PARAMETER INTERACTION 360 DEGS
SUBJECT TO CONDITIONS RAIN & 0.00 LANDA \*

1000		r ,	1		ķ		3	3	ş.				Ž.		2			14	2	117	2	24.2 AVE		***				2		.7. AVE	*	1	70 71 Ave				NV II	15.00 15.00	<b>#</b> {	ĽĖ	110.47 AVE			
TER B	•	7	•	-i			•	· <del>vě</del>	-1		**	ei.	2		•	Ħ	N C		7	n	ei,	7201		'n	3		13,15	N	N C		23	ai (	N W		3	N A	18.750	7	į.	N O	3	. 3	~	
X PARAMETER RAN		18600.00	0.10	60 17	6,29	15	14.0	1,36	1,18	75	3,10	2,49	2,14	261	6,22	2,78		334	**	3,13	2,78	101		2.50	2,79	430	10,36	9	2,75	454	10.05	2.0	2,72	472	11,14	Z: 7	•	<b>;</b>	25.22	2.70		226	2.1	
	•	6180.08		1.99	0,2		0.69	1,96	1.40	140	2,78	2, 49	2,16	224	5,45	3, 86	2,54	244	7.34	3.16	2,74	XX	45.4	5.23	2,94	300	9.23	90.0	2,73	549	9.70	00°0	2.74	424		2. 5		433	10.15	2,72			2.52	
	***************************************		0.10	1.09	0.29	95	19.0	1.92	1.50	113	2.27	2.43	1.07	187	4.85	2.92	2.47	246	5.9	3.84	2.5	28.5	7-0	0.00	2,75	144	7.67	2.9	2.78	150	6.43	2,05	2.04	376	8	2.79				2.60	;	124	2.67	
	***	<b>90'086+</b>	0.04	1,25	0,43	20	0.31	1.34	0,71	*	113	1,88	1,32	135	2,55	2,36	1,62	180	3,78	2,45	1.84	28.0	19-7	2,51	1,00	23.	5.12	2.37	1.87	207	5.51	2,33	1.84	314	5,72	Z*Z		925	<b>1</b> 010	1.61		40.4	2.10	
	4 2		0.02	1.00	90.0	ij	60 0	1,00	-	1	0.57	1,64	1,02	82	1,51	20.5	1,26	123	2,09	2,13	1,45	163	2.75	2,11	1,49	282	3,16	1.07	1.64	229	3,54	<b>3</b>	1,	246	3,71	1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 0 1 0 0 0 0 1 0		762	? .	1.50		, ,	4	•
	TAPE MB	2200.00		00.0	6	•	Ó	1,00	0.00	17	0,19	1,41	0,77	32	0.42	1,63		96	•	1.52	•	44	1.18	1,53	16.8	111	1,54	1,45	16.0	158	1, 51	¥ ;	u, 3y	173		1.42		2 d	2.4	90.0	. ?	9 T C	1.40	
•	000		٠	00.0	ē	8	0,02	1,00	o.	•	90"0	1,33	0.75	115	0,15	1.27	0.77	25	0.26	1,28	99.0	io Pr	0.40	1,43	0.93	35	0,57	1,31	0,61	99	9,69	1,28	0.0	82	19 0	1.21	• ;	10 6 10 4	A 0 .	0.72	<u>.</u> ;	1:-	1,25	
	000	2		•	0	9		C1	e.	•		0	•		-	9.90	ē	'n	-	1.00	•	٥	•	•	c	=======================================	60.0	1,00	•	16	۳.	90°	•	23	•	) (C	•		•	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	•	4	1,72	
	470	•	9,69	0000	0,0	7	Ü	00"0	٠.	0	00.0	00.	o.	•	٩.	30.0	e_	0		00.0	_		0.00	0.00	•	-		1,50	=	-	•	5	7.		9	. E		•	. c	1 . C		۰ <u>-</u>	1.00	
<b>L</b> -	<u>.</u>		_0	0	50.7	* 1	19*1		(.) 8 . !	(1	٠.	D	1	• •	0.1	9	; ; :3 -	٤,	04	0.1		•	0	0	. dC	•	.0		•	1 :				•••	D 6		•	_	<b>3</b> C			0	5	•
ER LT-09T		40.	PCT.	DT.	STD.	2	PĊT.	10	STD.		PCT.	ЭТ.	STD.		PCT.	ot.	20.5		7	DT.	STD.		7	Dr.	sto.		PCT	1	2.0	2	PCT.	Ė.	-	9	۲. د	STS.				510.			5	•
ARAMF TER		. 0	)			2.5				4.5				9.00				12.5				16.0				24.5.				32,01	•			40,7				20.00						

TABLE B-74

PARAMETER INTERACTION 360 DEGS

SUBJECT TO CONDITIONS 91.00

LAMB T 90.00

R RANGE	LIKİT	•	6.0		0752,17 AVE		7.07	16.0	1.74	-	4.	26.		163,23 AVB			3,23	716.91 AVB	3	10. V		7476,22 AVB		12,47	# ·	34.4 44 910		13.37	3.23	25.20		14,01	3.19	3.50		14,53	3,10		BAY BE DAGE		10.0		6973,63 AVB	Ž	70.0	200	6989.81 AVG	A.
X PARAMETER RANGE	10000,00	~	0,42	90	-								1,69				2,28			1 . L				66.4							7 117		3,01		47.	11,22	2,94		•	11.46	2,48	2.93				2.86		13.62
	6100,90	~	0,02	0.0		4		7	1,12	***	2.42	2.10	1,73		239		2,20		258		2.69	•	350	8,31	2,37	,,,	345	9,03	2.34	2.34	412	96.0	2,30	2.40	434	4.4	2.4	2,90	787	10.07	2.17	2,76		4.55		8		14.55
	6405.00	~	0.03	9.0		90	2.43	1.42	6		70	2.13	1.50	•			1.95		524	2.66	2.41	•	283	6.28	2.78		319	9.90	2.71	2.91	XAR	7.35	2.65	2.46	371	7.65	2.50	2.46	500	7.86	2.51	2.42	•		4	50.2		15.71
	4900,00	8	0.0			54	27.0	1:13	0.33	*	9,00	1.75	1,22	,	121	2.02	1,58		173	2 4 6	2.03	•	223	4,24	2, 58	6.10	254	4,76	2,35	2.03	241	5,15	2.30	2,03	200	5.40	2,25	2,07	13.	2.60	2.19	2.02	ļ	252		1.95		18.63
60.06	3600,00	0	Ö	90.0		<b>^</b>	90.0	1000	9.00	ž	40,0	1.39	26,0	į	* 6	4.63	1,10		Ξ.		1.29	•	153	2,29		1,00	185	2,72	1.84	1.29	213	3,04	1,81	7,26	<b>18</b> 2	£ 28	1.78	1,50	240	10 m	1.73	1,34	!	783	- 22	1.29	ì	22.42
	2500,00	0	9.0			P3 (		3 C	00.0	Ŧ	50°8	1.00	90.0	;		4 to 4.	05.0	ı	9 4	44.	0.58	•	06	60.	1.22	7.*0	117	1,43	1,53	6,73	143	1.58	1.40	0,72	162	1.98	1.46	0.0	178	2.05	1,42	0.45		212	7	0.0	,	28.06
ن	1600,00	0	06	38		~ ;	20.0	701	<b>6</b> 0 <b>.</b> 0	۳	0.05	1.00	0.00	•	2		0.0		<b>10</b> 6	2,10	0.42	•	35	40.0	1,24	•	52	0,50	1,21	0.45	70	99 0	1.19	67.0	*	0,81	1,20	0.67	3	60.0	1,19	0,64	į	122	61.	09.0		34.02
	900,00	0 ;	9	90	•	•		•	₽.	-	0.01	1.00	00.0	•	-1 č	100	9.00	1	N 0		0.50	•	<b>+</b>	40.0	1,52	•	1	90.0	1,14	42.0	13	0.12	1.15	38.0	4.6	0,10	1,16	•	22	0.20	1.14	0.42	;	7 F	70.1	٠.	;	45.09
	400,00	0	000			o ;			no o	c	u, 00	0,00		(			00.0		≓ <b>6</b>			,	н,	100	200		+	0,01	1,00	•		0.01	1,00	•	7	70.0	•		۸	0,02	1,00	•	•	90.0		90.0		54.49
<b>.</b>	101	.5	, , c	0			- è		<b>2</b>	٠.	.0.	0	30.5	•		) ()	0		us a, C		c	•	• •	e c				-		D	•	3,63	00.	0	,,	6		. D .	•	0	0	:0:	٠	. <b>.</b>	Ö	0.	į	. i b
PARAMETER LT-DOT		0.50 NB.	126	STD.		2.GU NB.		-	.0.5	4 56 149	PCT.	pr.	SID.				STD.		12.51 NB.		STD,		18.01. NB.			- - - -	24.5L NB.	PCT.		STD.	32.00 NB.	PCT.	DT.	stb.	40.50 MB.	PCT.	ָם. מַלָּייָ	STD.	50.0E NS.	POT.	11.	STD.		- 1013 604		STD.	• : :	
>																							1	R~	1 5	30													C	n	N	FΤ	D.	ΕN	งา	T/	١	

	369 BE&S	0.0G LANDA =
TABLE B-75	-	SUBLECT TO CORDITIONS ATTACK
		SUBJECT

RAMETER	LT-D8T					•				X PARAN	PARAMETER RANGE
	, E	£ 53		445.0	TAPE MB		2007	•			1 1 1
0.50			2	יים מיים	00.00		D9 * 90 A+	00"40+0	04.001 <b>8</b>	56 ° 0200 L	, TE 13
	PCT.	€.	•		00.0		0,62	•	20.0	è	60.0
- (		E (	00.0	0.00	0.00	00.0	1.00	1.00	1,00	1,00	1.00
0		D.		-	<b>15</b>	ě	09 0	•	0.00	ē	86.0
2.0%			0	a	8	^	F.	2	7.0	90	1174/672 AB
		e.	06.0	0.00	0.02	-	0,14	0.25	00.0	0.32	4
-;		e -	0.00	0.00	1,50	5		1.48	1,41	10 m	
S)		0.0	9,30		0.50	W.	0,61	6.8%	0.78	0.76	
70			<	•	Ç	į	;	i	į	,	9149,74 AVE
•	בני.	-		4 2	77	7		9 4		112	
. ~	, ,						D 4		7	7.1	);
v.	10			10	64.6		į	10.7	•		70.7
,	•	•			•		•	1.3	•	7.0	2747. 48 AVE
09.6			₩	•	*	26	26	139	176	205	248
<b>.</b> `	<b>9</b>	0.0	10.0		0.34	0,82	-	2.82	3,70	4.25	5.55
- 1	, na.	<b>•</b> •	904	1,25	1,75	1.78	2,23	2,54	2,64	2,60	2.63
n		5	90.0		/A.D	1,10	•	2,12	2,18	2,11	
12.50			٥	č	Ĕ	;	2	•		2	7470,72 AVE
:	.;	0	8.92	9.7	9,6	0 0 0	161	197 T	23.7 4.23		
	9	•	1.90	1.20	1.57	1.78	2.14		7	2.6	
í	7	0.0	٠,		96.0	1 30	1.55	2.10	2.22	2.16	2.2
			•	. (	. ;	•	•	•	•	•	7349.18 AVB
10.0t	•	•	1		79	130	186	247	214	345	417
ζ."		<b>-</b>		62.0	9,0		2,26		6.42	7.29	56.0
v	, .			•		100	2,17	2,51	2,69	2,65	Z.
1	•		•	•		77'1	1.01	12.2	\$212	2117	2,21
24.56			•	51	109	3.66	227	285	UTE	XAX	
	PCT. L.OC		00.0	-	1.28	2,31	3,76	5,93	7.05	7.05	3.
-;	<b>(3</b> )	0	1,00	1.14	1.47	1,75	2,07	2.43	2,60	2,57	2,43
•	•	0.0	P.	-	<b>96</b> . D	1.36	1,65	2.20	2,24	2,18	
100			;	:	92,	į	1	101		•	9AY 14 7069
	DCT.	c	10		129	7	100	317	372	614	200
	7		9	41.		7,17			2 .		20,17
60	0		~		60.0		.61		2.24	7.7	20.0
	•	•	•		•		:				4757.21 AVB
04.00	•		25	77	150	ž	276	332	757	435	203
Ē.	701. 201.	-	71.0	0.70	1.70	60.	4,41	9.20	7.78	8,70	#.07 97
	•	- 6		71.0	7.0	) (	20.7	2.34	7,51	16.2	Z • 20
	•	•			1	Ď7 I T	1.34	6113	212	71.7	12.2
50.00			23	16	167	230	292	340	405	493	256
₹` 	57. 2.00	0	17.0	0,83	1,88	8,09	09.*	6.42	8.00	20.8	10.73
~ (	. 5 .		6	•	1,1	1,66	1.98	2.30	2.48	2,47	2.56
	5	5	0,23	•	. a	1,27	ņ	2,13	2,21	2,15	2.19
LIMIT	_		42	123	253	271	333	NON	4	15 15 15	9082.39 AVE 577
		6	0.34	1,10	N	3.47	5.01	4.87	6.49	9.47	11.36
T	1,96	1,90	1.02	1,12	1,56	1,61	1,89	2,19	2,36	2.36	2.47
<b>S</b>	• •		0.15	6,35	₹.	1,20	1,53	2.07	2,15	2,10	2.15
7	AVE AT	•		97 61	**		;		;	•	6509,72 AVB
•	. 106.	5		07		90-47	19.06	17.30		19.67	19.24

••	360 DEGS 5.00 LAMDA =
TABLE B-76	PARAMETER INTEGACTION 360 DEGS SUBJECT TO CONDITIONS THIN E 5.00 LA

					AVB				AVB				9	•			9					9				AVG				AVG				AVE				9				9				9.0	<u>}</u>
X PARAMETER RANGE	LIHİT	<b>I</b>	0.0	9.00 T	12372.14	90	* :	1.00 1.00 1.00			1.75	2.01	1.70	7.	4.09	2.64	2.47		26.5	2.57	2.25	9531.13 A	248		6.5			7,85	2.56		404	6.24	2.53	6323.89 A		50	7 - C	8190.42 A	442	8.78	2.49 2.83	8104.35 A	224	9.74	2.33	7625.71	10
X PARAME	10000,00	•	-			52		1,06		80	1,14	_			2,91		2,11	246	4.49	2,40	1.98	;	2002	• 0 ° 0	00.0	4017	327	6,17	2.36		353	6,54	2.52	9017	376	6.15	8/17		10 E E	7.03	2.2		467	7.02	2.00		20.44
	6100.00		Ė.	5.0		22	0.22	77	5	2	0, 33	1.67	1,31	134	2,45	2.29	1, 33	746	3,74	2,30	٠.		526			1	235	5,78	2.24	<b>0</b>	8	4	2.20	•	344	5, 23	7.10	•	966	6,11	2.15	<u>.</u>	433	6.37	2 .		21.59
	6400,60	973	0.02	6.6		87	7.0	. c		2	0.74	1.58	1.78	104	1.04	2.21	2.04		2.85	2,25	2.02	,	9g2	ه د و د	77.7	1.	243	4.21	2.17	7	267	4.53	2.12	1.0	241	4.81	£.,		N-EM	86.4	2.0		377	5.77	1.02	1.1	02 FC
	4900.80		0.62	1.00		1.3	0.10			÷	0,53	1,50	P . D	9	1,17	2,13	2,04		1.92	2,13	2.04		160	200	* 0 * 7	1.01	193	3,08	2.0	0.1	216	3,35	7 6	7.1	239	3,62	1.00		252	3.77	1.87		372	4.47	1 . 7 e	1.00	25.48
,	3606.00		0,01	9.0		•	90.0			52			ĸ.	42	0,0	2,10	•.	-	1.21	2,07	1.82		110	D F		7	144	2,11	***		147	2,35		<b>1</b>	149	2,59	10	•	274	2.74	4.	• •	246	9	,		20.19
1	7APE NO. 2500,00	•	00.0	9.0	3	en ;	* C			10	0,13	1.60	1.02	18	0.25	1,72	1,28	2	6,49	1.59	1,03	;	65 C	16.0			Ş.	1,11	9 2	•	115	1.20	, e		129	<b>1</b>	C	3	143	1.56	. e	•	202	2.15	1.51		36.55
	1600,00	•		0,0		ਜ ; (	10.0	20.		-1	0,01	1.00	0.00	•	9,04	1,25	0,43	đ	0.10	1,53	0,67	ļ	24	3.5	1,21		4	D.	1,20			0.49	1,17	<b>Y</b>	63	3.56	1.16	•	70	0.65	7 . T	,	126	1.16		,	49.47
	90,006		ē		1	•		5.6	•	•	0.00	•	į.		•	90.0		<b>c</b>	•	0.00	٩.	,	•	70.0		•		٥,	- C	•	•	٦,	2 c	•	•	9 t t t		•	ď	÷		•	54	7.46		•	64.49
	400,00	•	9.00	5 C	3		5 6		•		30° G	) () ()	na i	•	00.0	1.00°	ນູ້ຄ	æ	9 <b>0</b> 0	00.0				5 6		•	0	ت	r. c	•	н	ن	e. c	, •	~	ນໍ້	a t L L M		٠.	76.0	ລ : ເີຍ ເ	•	•		( e	•	45,64
	10.001		0	 0 6	<u>;</u>		) (	2 0	· •	•	1610	<b>1</b>	70.		.04.7	0			, co					- - -			••	() ( () ()	5	• •		<b>6</b>	L 1 4	•	.,	 	: 1 to	• •	-	E .		• •	,		<u>.</u> '	•	۲,
ER LT-087		2	7		)			· E			PCT.		• 0 - 0		PCT.	ot.	sto.		PCT.	.10	sto.		r- 3	; ;			٠,	בן ב	er.	•	,	PCT.	- - -	•		1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	, e	•	Ci.	104	: : :	;		ا دا د	- £	•	Ç
ARAMETER		0.5			,	2.0.				4.2				8	•							- 1	E .				24.5				32,0				40.5				50.0				LIMIT				

	360 DEGS G.GG LAMBA #
TABLE B-77	PARAMETER INTERACTION 5 SUBLECT TO CONDITIONS ANIM W AMEN TO ARE DO

B-133

では、「「「「「」」という。「「「」」というできた。「「「」」というというできた。「「「」」というできた。「「」」というできた。「「」」というできた。「「」」というできた。「「」」というできた。「「」」というできた。「「」

	;	20.00
TABLE B-78	PARAMETER INTERACTION 060 DEGS	CONTROL
	ü	5

RAMETER	L T-DAT	<u>.</u>			<b>.</b>	LAME	162.09				7	TOWNS CASSING
						TAPE N	ġ					
	•	10.101	400,00	90,006	1690,00	2500,00	3600,00	4900,60	6400.00	8100,mg	10000,00	LIMÎT
J			= c	E) (	0 ;	9 6		•	•	<b>=1</b> (		<b>+</b> į
	;;	s è			200		9.0	0 · 0	B. C	10.0	20.0	20.0
			2 6	3 6				9.0		<b>P</b> (		
	,		•							•		15737.88 AVB
2.6	, 9,		0	0	7	N	•		15	22		
	<u>.</u>	0.0	7,03	9.36	0.01	0.02	0,05	60.0	6.12	0.18		9.50
	70	.00	9,00	00.0	1,00	1.00		1.00	1.00	1.05		1.92
	STD.		9.00	30.0	00.0	90°0	0 0	00.0	8.00	12,0	6,37	7.
,	•	•	•	,	,	•	ļ					17856.66 AVG
. 13		• •	မ <u>(</u>	-1 ;	2	•	ij	27	4	7	52	<b>7</b>
		3	700	100	20.0			65.0	76.5	Z:		î.
		•	) ) )	7	10 0 T	30	60.1	1,61	1.73	1, 45		2.64
	S 0.		n a	06.0	0.00	90.0	0 * °	1.76	1.81	1.93		3.51
•	•	•	•	٠	•	;	•		;	:		ISCUY, SO AVE
		· •	e e	9-93	2 2	10-0	7 6	27.	•	¥2.		17
	nT.		, c	0 +		5			100			
	STD.			00'0		0.00		10.1		1 · ·	7	12.5
			•		•	•		:	•			11185.74 AVB
12.5	P.	•	0	~	,	**	51	78	95	107		133
	PCT.	00.	0°0	0,02	90.0	0,23	19'8	1,13	1.57	1, 17	2,82	3,11
	П.	0	9,6	1,00	1,43	17.1	1.51	1.62	2.47	2.19		2.93
	STD.	13	ວລໍ້	0.00	1,05	0.54	04.0	1,59	1,71	1.46		3,38
							1	,	ı			18866,83 AVG
18,00	Ę.	.,	2	•	16	*	11	111	126	145	151	169
	<u>.</u>		0°0	7.3	0.18	6.45	0.95	1.61	2.12	2.48		2.5
	Ė	Ď	50°C	1.90	1,38	1.19	1,55	1,62	2.08	2.14		2.82
	STD.		ສ <b>ຸ</b> ຍ	0.10	0.78	6,53	9.18	1.64	1.62	1.48		5.10
	6	•	•	•	ž	4			•			344 44. VUV
	, i	Ė	- C	` .	200		7 3	77.	101		6	4.42
	; ; ;		3 : C		72.	28				, c		2.0
		, E		1	5.4			2.	11.2			
	: :		÷ •	0.40	0	P 1		1.65	20.			AVA TT 1978
10 02	q	•	•		2	**			27.	- 52		26.7
•			4 <b>C</b>	9.1.0	0 00	0.77	42.	2.11	2.67	3.87	3.26	4.42
	50	e:		1.17	1.29	1.76		1.A0	2,45	2,12		2.68
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- (U) The primary objective of this study is to define the dogfight environment in terms of a tracking system. The secondary objective is the apply this dogfight definition to present AI radars.
- (U) This study is divided into two efforts, a determination of the primary weapon control requirements and a parameter interaction study. The purpose of the primary weapon control requirements study is to define the dogfight environment and to investigate the relationship of aircraft, tactics, weapons, and the available data base. The purpose of the parameter interaction study is to define the dogfight environment more precisely in terms of tracking loop requirements, clutter problems, and glint.

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- -- OBJECTIVE IS TO APPLY THIS DOGFIGHT DEFINITION TO PRESENT AI RADARS.
- -- THIS STUDY IS DIVIDED INTO TWO EFFORTS, A DETERMINATION OF THE
- -- PRIMARY WEAPON CONTROL REQUIREMENTS AND A PARAMETER INTERACTION
- -- STUDY. THE PURPOSE OF THE PRIMARY WEAPON CONTROL REQUIREMENTS STUDY
- -- IS TO DEFINE THE DOGFIGHT ENVIRONMENT AND TO INVESTIGATE THE
- RELATIONSHIP OF AIRCRAFT, TACTICS, WEAPONS, AND THE AVAILABLE DATA
- -- BASE. THE PURPOSE OF THE PARAMETER INTERACTION STUDY IS TO DEFINE
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